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## Blasting with Solid Carbon Dioxide – Investigation of Thermal and Mechanical Removal Mechanisms

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### Abstract

Cleaning technology is an important factor in the field of production technology as well as service and recycling. Blasting with solid carbon dioxide (dry ice blasting – dib) is generally based on compressed air, which is a flexible but energy consuming acceleration method. To improve the mechanical acceleration by rotational wheel blasting, the main removal mechanisms of dib, mechanical and thermal, have been investigated separately. Based on the developed methods both mechanisms can be characterized independently of the target type. The presented results show a promising approach to determine the size of the mechanical removal mechanism's impact force. Obviously it depends primarily on the blasting pressure, one of the main influencing process factors.

Cleaning applications – substrate and the adherence of the residues – show different resistance against thermal stress as well as against mechanical impact. Because of this, an overall benchmark independently of the application had to be defined in order to compare the blasting efficiency of both blasting technologies and the results.

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### 1. Introduction Main text

In the context of surface technology great importance is attached to the cleaning and maintenance of metalworking machines [1]. Cleaning is the removal of residual lubricants, process liquids as well as remaining substances from preceding processes. Total removal of cooling lubricant residuals and chips is usually done by an aqueous or organic rinsing medium. For the transfer of the contamination into this cleaning medium and the following lubricant regeneration as well as the lubrication process itself, a significant amount of energy is required, e.g. for the heating or vacuum generation [2]. The cleaning process can make a substantial part of specific manufacturing chains: For example, up to 25% of production time and of production costs are generated by purification processes within the manufacturing chains of representative automobile parts [3]. Flexibility in the design/application of cleaning technologies is important due to

the continuously changing requirements of different cleaning tasks [4].

### 2. Cleaning Applications

The suitability of dry ice blasting (dib) for cleaning and pre-treating was confirmed in detailed experiments [5, 6]. In the area of selective cleaning by means of dry ice blasting several applications had already been investigated: Examples are the combination of cleaning mechanisms, the decrease of noise emission, the increase of the material removal rate through hybrid combinations as well as energy efficient alternative acceleration concepts [7, 8].

Dry ice based cleaning technology can help to avoid downtimes regarding current carrying power plant installations. For the inline cleaning of wood machining tools blasting with solid carbon dioxide (CO<sub>2</sub>) offers a task oriented selective cleaning technology. The prerequisite for the process

integration of cleaning by compressed air driven dry ice blasting is a substantial decrease of the noise level of up to 120 dB(A). Therefore, approaches of noise reduction regarding various noise emergencies were studied to develop noise reducing nozzles. As an energy efficient alternative to compressed air driven processes the mechanical acceleration of the dry ice pellets was examined with the help of a centrifugal wheel blasting device.

### 3. Blasting with solid Carbon Dioxide

Dry ice blasting has been intensively investigated [9]. Solid carbon dioxide (CO<sub>2</sub>) is a one-way blasting medium. Due to sublimation, no additional solid residues of the blasting medium remain beside the removed contaminant. CO<sub>2</sub> is chemically inert. In solid state the hardness of dry ice pellets is comparable with gypsum and the temperature at ambient pressure is -78.5°C. Recent investigations of the hardness came to the result of a Mohs hardness of 1.5 [3]. The CO<sub>2</sub> used as blasting media does not contribute to global warming, since it is either a by-product of the chemical industry or derived from natural sources [7]. In any case the CO<sub>2</sub> – if used as blasting media or not – gets nevertheless into the atmosphere.

Two forms of blasting with solid CO<sub>2</sub> have to be distinguished: CO<sub>2</sub>-snow blasting and dry ice pellet blasting. Beyond this the acceleration method, either by compressed air or mechanical by rotational wheel blasting, influences the energy efficiency as well as the blasting foot print.

The CO<sub>2</sub>-pellets are made of CO<sub>2</sub>-snow, which is pressed through a matrix. The diameter of the matrix' holes as well as the environmental conditions determine the properties of the CO<sub>2</sub>-pellets, the so-called dry ice.

The cleaning effect of solid CO<sub>2</sub> blasting is based on a combination of a mechanic and a thermal mechanism (**Fehler! Verweisquelle konnte nicht gefunden werden.**), which is supported by the sublimation of the blasting media. While the contaminant is mechanically removed by the impact of the CO<sub>2</sub> particles (A), tensions at the interface of the contaminant and the surface to be cleaned are a result of the thermal mechanism (B). Due to the sublimation the surface is additionally cooled, which increases the thermal mechanism.

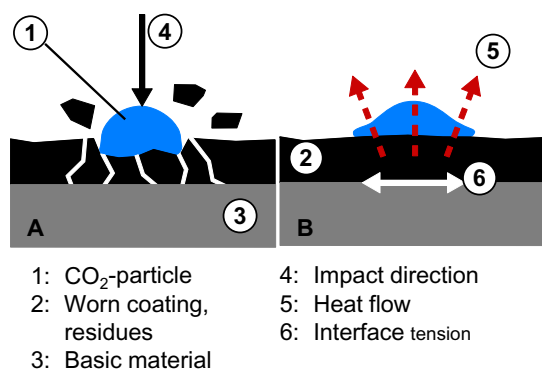


Fig. 1: Thermal (A) and mechanical (B) removal mechanisms

#### 3.1. Motivation

Nevertheless, essential questions still have to be answered for a significant better understanding and a potential improvement of the blasting process. In particular the direct energy consumption for the majority of the purification processes is to be reduced. The Identification of the relevant mechanisms for the cleaning, e. g. mechanical and/or thermal is needed for their detailed investigation. Can these be separated and recombined for a specific cleaning task more effectively?

To identify the primary removal mechanism of a specific cleaning task, the different mechanisms have to be varied. Up to now, various investigations were conducted, but a measurement of the effects proved to be difficult. Due to the sublimation of the dry ice pellets as well as of the blasted CO<sub>2</sub>-particles a measurement of their properties is not possible with conventional methods. But the solid CO<sub>2</sub>'s hardness, impact force and cooling effect is of interest with regard to the residue's removal and the cleaning process. The contact time of the particle's impact onto the workpiece (or any sensor) is of high significance for the measurement.

#### 3.2. State of the art

UHLMANN investigated the impact force of blasted CO<sub>2</sub>-pellets. Besides the indirect effects generated on the so-called blasting good the blasted particle's velocity was measured and the resulting kinetic energy calculated. The impact force was measured by piezo-electric load cell. He distinguished a static and a dynamic force component. The dynamic force of dib was measured to be approx. four times as high as compressed air blasting for specific parameter settings. In opposite the static component of dib was only 10% higher than compressed air blasting. The maximum impact force measured is of higher relevance for the particle's impact: Dry ice blasting resulted in 150 N, compressed air blasting in 75 N [10].

HABERLAND investigated the removal effects, too. By the application of thermocouples the cooling of the workpiece was documented. Due to the already cooled compressed air (down to approx. -70°C), which accelerated the pellets and the workpiece specific heat conduction the minimum temperature was already reached before an initial pellet impact. The impact was observed by a high speed camera (hsc). Because the pellet was entirely smashed he calculated a contact time by the particle's velocity and dimensions of approx. 22 μs. Additionally he supposed a possibly melting by the impact observation [11].

REDEKER formed a larger carbon dioxide cylinder and measured the properties with conventional but cooled equipment. By the help of the measured elastic modulus a contact time of approx. 1.5 μs to 50 μs for the elastic impact was calculated. The values depended only on the particles' diameter between 0.1 mm and 3 mm. Regarding the solid carbon dioxide's hardness and flow limit a total elastic impact is unlikely. In a plastically approach, REDEKER assumes a contact time of less than 15 μs to 500 μs. Though being much longer than it can be observed by many investigations by hsc

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