



# The influences of the engine design and operating parameters on the performance of a turbocharged and steam injected diesel engine running with the Miller cycle



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## ABSTRACT

This study reports the influences of the engine design and operating parameters on the performance of a turbocharged, steam injected and Miller cycle diesel engine by using a simulation model based on the finite-time thermodynamics. The model is validated with experimental data and the effects of various engine design and operating parameters such as cycle temperature ratio, cycle pressure ratio, friction coefficient, engine speed, mean piston speed, stroke length, inlet temperature, inlet pressure, equivalence ratio, compression ratio, steam ratio, retarding angle and bore-stroke length ratio on the effective power and effective efficiency are investigated. Furthermore, the energy losses originating from incomplete combustion, friction, heat transfer and exhaust output are demonstrated by using figures. The results show that the engine performance increases with increasing some parameters such as cycle temperature ratio, cycle pressure ratio, inlet pressure; with decreasing some parameters such as friction coefficient, inlet temperature, steam ratio, retarding angle of intake valve closing. However, the engine performance could increase or decrease with respect to different conditions for some parameters such as engine speed, mean piston speed, stroke length, equivalence ratio and compression ratio.

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## 1. Introduction

Nitrogen oxides (NO<sub>x</sub>) emissions have detrimental effects on the environment, therefore they must be decreased. It is known that formation of NO<sub>x</sub> is very sensitive to combustion temperatures in the internal combustion engines (ICEs) [1–28]. They can be abated by reducing combustion temperatures. Recently, so many searches have been performed on the steam injection method (SIM) to lower NO<sub>x</sub> emissions released from the ICEs. The SIM leads to a high decrease rate in the formation of NO<sub>x</sub> emissions. Because, the steam in the charge decreases combustion temperatures due to higher specific heat of steam and slower combustion process is carried out. [1–12]. Another NO<sub>x</sub> reduction method is the Miller cycle application. The Miller cycle is carried out by lowering the compression ratio according to the expansion ratio. It can be achieved by retarding intake valve closing during the compression process or earlier closing intake valve during suction process. Hereby, maximum combustion temperatures and NO<sub>x</sub> can be decreased [13–38]. Turbo charging systems are commonly used to increase specific power of the internal combustion engines (ICE) [39–50]. The combination of these three methods could be used in the diesel engines in order to acquire maximum NO<sub>x</sub> reduction rate with higher power output.

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**Nomenclature**

$A$	heat transfer area ( $\text{m}^2$ )
$C_v$	constant volume specific heat ( $\text{kJ/kg.K}$ )
$C_p$	constant pressure specific heat ( $\text{kJ/kg.K}$ )
$d$	bore (m)
$F$	fuel-air ratio
$FTTM$	finite-time thermodynamic model
$h_{tr}$	heat transfer coefficient ( $\text{W/ m}^2\text{K}$ )
$H_u$	lower heat value of the fuel ( $\text{kJ/kg}$ )
$ICE$	Internal combustion engines
$l$	loss
$L$	stroke length (m), energy loss percentage (%)
$m$	mass (kg)
$\dot{m}$	time- dependent mass rate ( $\text{kg/s}$ )
$N$	engine speed (rpm)
$P$	pressure (bar), power (kW)
$P_a$	turbo charging pressure
$r$	compression ratio
$r_M$	Miller cycle ratio
$R$	gas constant ( $\text{kJ/kg.K}$ )
$\bar{S}_p$	mean piston speed ( $\text{m/s}$ )
$\dot{Q}$	rate of heat transfer (kW)
$S$	stroke (m)
$SIM$	steam injection method
$T$	temperature (K)
$v$	specific volume ( $\text{m}^3/\text{kg}$ )
$V$	volume ( $\text{m}^3$ )
$x$	ratio of steam to fuel

*Greek letters*

$\alpha$	cycle temperature ratio
$\beta$	pressure ratio
$\delta$	expansion ratio
$\varepsilon$	stroke ratio
$\phi$	equivalence ratio
$\psi$	cut-off ratio
$\lambda$	cycle pressure ratio
$\mu$	friction coefficient ( $\text{Ns/m}$ )
$\rho$	density ( $\text{kg/m}^3$ )
$\eta_C$	Isentropic efficiency of compression
$\eta_E$	Isentropic efficiency of expansion

*Subscripts*

1	at the beginning of the compression process
$a$	air
$c$	combustion, clearance
$cyl$	cylinder
$ef$	effective
$ex$	exhaust
$f$	fuel
$fr$	friction
$ht$	heat transfer
$i$	initial condition
$ic$	incomplete combustion
$in$	input
$l$	loss
$max$	maximum
$me$	mean

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