

#### **ORIGINAL ARTICLE**

# Nozzle geometry variations on the discharge coefficient



**Propulsion and** 

Power Research

## M.M.A. Alam<sup>a,\*</sup>, T. Setoguchi<sup>a</sup>, S. Matsuo<sup>b</sup>, H.D. Kim<sup>c</sup>

<sup>a</sup>Institute of Ocean Energy, Saga University (IOES), 1, Honjo, Saga-shi, Saga 840-8502, Japan <sup>b</sup>Department of Advanced Technology Fusion, Saga University, Japan <sup>c</sup>Department of Mechanical Engineering, Andong National University, Korea

http://ppr.buaa.edu.cn/

**Propulsion and Power Research** 

www.sciencedirect.com

Received 14 February 2014; accepted 16 November 2015 Available online 12 February 2016

#### **KEYWORDS**

Boundary layer; Compressible flow; Reynolds-averaged Navier–Stokes (RANS); Shear layer; Sonic lines; Supersonic core **Abstract** Numerical works have been conducted to investigate the effect of nozzle geometries on the discharge coefficient. Several contoured converging nozzles with finite radius of curvatures, conically converging nozzles and conical divergent orifices have been employed in this investigation. Each nozzle and orifice has a nominal exit diameter of  $12.7 \times 10^{-3}$  m. A 3rd order MUSCL finite volume method of ANSYS Fluent 13.0 was used to solve the Reynolds-averaged Navier–Stokes equations in simulating turbulent flows through various nozzle inlet geometries. The numerical model was validated through comparison between the numerical results and experimental data. The results obtained show that the nozzle geometry has pronounced effect on the sonic lines and discharge coefficients. The coefficient of discharge was found differ from unity due to the non-uniformity of flow parameters at the nozzle exit and the presence of boundary layer as well.

© 2016 National Laboratory for Aeronautics and Astronautics. Production and hosting by Elsevier B.V.

This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

#### 1. Introduction

Nozzles are found encountering in a wide variety of engineering applications, mainly to generate jets [1–4], flow metering [5–7], and sprays [8,9]. The accurate prediction of the compressible nozzle flows is still challenging for the aerodynamicist, and achieves increasing importance since

<sup>\*</sup>Corresponding author. Tel.: (880) 8043156244.

E-mail address: dralam@me.saga-u.ac.jp (M.M.A. Alam).

Peer review under responsibility of National Laboratory for Aeronautics and Astronautics, China.

<sup>2212-540</sup>X © 2016 National Laboratory for Aeronautics and Astronautics. Production and hosting by Elsevier B.V. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

### Nomenclature

а	sound speed (unit: m/s)	$u_i, u_j$	Cartesian me
$A_e$	area at nozzle exit (unit: m <sup>2</sup> )	$v_x, v_y, v_z$	Cartesian ve
$C_d$	discharge coefficient		tions (unit: 1
$C_p$	specific heat at constant pressure (unit: $J/(kg \cdot K)$ )		
$\hat{D_e}$	diameter at nozzle exit (unit: m)	Greek symbols	
$D_m$	diameter of Mach disk (unit: m)		-
Ε	total energy per unit mass (unit: J/kg)	β	conic diverg
F	inviscid flux vectors	δ	boundary la
G	viscous flux vectors	$\delta_{sh}$	shear layer t
H	total enthalpy per unit mass (unit: J/kg)	γ	ratio of spec
H	vector for source terms	μ	dynamic vis
i	unit vector in the <i>x</i> -direction	υ	kinematic vi
j	unit vector in the y-direction	$\theta$	conic conver
k	unit vector in the <i>z</i> -direction	$\rho$	density (unit
k	turbulent kinetic energy per unit mass (unit: J/kg)	R	gas constant
$l_0$	location of minimum jet section (unit: m)	τ	shear stress
$L_m$	location of Mach disk (unit: m)	ω	specific diss
$L_s$	length of supersonic core (unit: m)		
<i>m</i>	mass flow rate (unit: kg/s)	<i>Subscripts</i>	
M	Mach number		
p	pressure (unit: Pa)	0	stagnation p
q	heat flux (unit: W/m <sup>2</sup> )	b	ambient
q	dependent vector of primary variables	t	turbulent
r D	radius (unit: m)	x	x-coordinate
	radius of curvature (unit: m)	v	y-coordinate
	keynolds number	x	<i>z</i> -coordinate
	temperature (unit: K)		

electromagnetic energy density (unit: J/m<sup>3</sup>) w ian mean velocity components (unit: m/s) ian velocity components in x-, y- and z-direcunit: m/s) ls divergent angle (unit: degree) ary layer thickness (unit: m) layer thickness (unit: m) of specific heats nic viscosity (unit:  $Pa \cdot s$ )) atic viscosity (unit: m<sup>2</sup>/s) convergent angle (unit: degree) v (unit: kg/m<sup>3</sup>) onstant (unit: J/(kmol · K)) stress (unit: Pa) c dissipation rate (unit:  $s^{-1}$ ) tion point nt

reference velocity (unit: m/s)

 $U_r$ 

the nozzle performance is significantly influenced by its inlet geometry. The flow emanating from nozzle exit serves as the initial conditions for the downstream jet flows. Thus, the studies on nozzle geometric effect are becoming a major interest for compressible and incompressible nozzle flows.

Several works reported information on aerodynamic features of jets and flow with various inlet-boundary conditions and nozzle geometries. Matsuo et al. [10] performed numerical study to investigate the effect of nozzle geometry on the sonic line and characteristics of the supersonic air jets. Two contoured converging nozzles, two conically converging sharp-edged nozzles ( $45^{\circ}$  and 75°) and a sharp-edged orifice were employed in their study. Otobe et al. [11] investigated the near-field structure of highly underexpanded sonic jets using three nozzle geometries (cylindrical straight nozzle, 75° convergence conical nozzle and  $45^{\circ}$  divergent orifice), and they proposed an empirical relation of diameter of Mach disk in terms of the pressure ratio, regardless of the nozzle geometry. Menon and Skews [12] conducted a numerical study on underexpanded sonic jets issuing from nozzles with contoured inlet, 45° conical inlet and an orifice inlet under a range of pressure ratio between 2 and 10. Hatanaka and Saito [13] conducted experimental and numerical studies to investigate the effect of nozzle geometry on the structure of supersonic free jets for three simple nozzle geometries over a wide range of pressure ratios up to 90. However, most of the above research works concentrated mainly on the shock and Mach characteristics of jets. In another study, Yu et al. [14] performed numerical simulations to investigate the effects of geometry variations on flow through nozzles. Four nozzle configurations were considered in the study: a baseline nozzle and three modified (extended, grooved and ringed) nozzles. The turbulence characteristics of incompressible flow through nozzles at Reynolds number of approximately 50,000 were investigated in their study. Only very few studies have reported, till date, on the performance of nozzle in terms of discharge coefficients. Hebber et al. [15] conducted an analytical study to obtain a simple, explicit and analytical expression for the discharge coefficients of conical convergent nozzle operating under varying pressure ratios. Cruz-Maya et al. [16] performed study to characterize the discharge coefficients in the venturi sonic nozzle considering the viscous and multidimensional effects of the fluid flow as uncoupled phenomenon.

Since the main purpose of this research is to investigate the effect of nozzle geometries on the performance in terms of discharge coefficients, five cylindrical, four conical convergent nozzles and eight conical divergent orifices with varying radius of curvatures, convergent and divergent angles, respectively, have been used. Sonic lines and their inflections were analyzed to examine the effect of flow parameter at nozzle exit on the discharge coefficient. Based upon the computed results, the nozzle geometry has Download English Version:

# https://daneshyari.com/en/article/1719606

Download Persian Version:

https://daneshyari.com/article/1719606

Daneshyari.com