



# An efficient strategy exploiting the waste heat in a solid oxide fuel cell system



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## ARTICLE INFO

### Article history:

Received 16 March 2015

Received in revised form

15 September 2015

Accepted 19 September 2015

Available online 22 October 2015

### Keywords:

Solid oxide fuel cell

Thermionic generator

Waste heat

Performance evaluation

Parametric optimization

## ABSTRACT

A novel model of the hybrid system consisting of a SOFC (solid oxide fuel cell) and a vacuum TIG (thermionic generator) is proposed so that the high temperature waste heat produced in the fuel cell can be efficiently exploited. Analytic expressions for the power outputs and efficiencies of the SOFC, TIG, and hybrid system are derived. The relation among the current density of the SOFC, the voltage output of the TIG, and the ratio of the areas of the SOFC and TIG is obtained by the energy balance equation. The influence of the current density of the SOFC on the power output density and efficiency is discussed for a given ratio of areas or voltage output. The maximum power output density and efficiency of the hybrid system are, respectively, equal to 0.560 W/cm<sup>2</sup> and 0.284 and the efficiency of the hybrid system at the maximum power output density is 0.240. The optimal regions of the power output and efficiency of the hybrid system are determined. The advantages of the hybrid system are expounded, compared with the single SOFC.

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## 1. Introduction

Electrochemical energy conversion has particularly attractive as the demand of secure, clean, and sustainable energy sources. Fuel cells can directly convert chemical energy into electricity without ignition combustion and have aroused much speculation about application in different endeavors and are considered to be one of the most efficient energy conversion devices [1,2].

Among the existing types of fuel cells, high temperature SOFCs offer great promise for making the most use of various readily available carbon-containing fuels. For stand-alone applications, the efficiency of SOFCs can reach 45–65% [3], which can compete with internal combustion engines [4], but the efficiency will quickly decrease with the increase of the electric current. On the other hand, the conventional SOFCs operate at relative high temperatures (973–1473 K), resulting in high quality exhaust heat [5]. Therefore, the hybrid systems of SOFCs, which can overcome some shortcomings appearing in SOFCs and enhance the power output, have attracted considerable attention in the last years. Kaneko et al. developed a solid oxide fuel cell and micro GT (gas turbine) hybrid

system [6]. Shirazi et al. analyzed an internal-reforming SOFC and GT hybrid system from the perspective of thermal, economic, and environment points [7]. Zhang and Chen established a hybrid system consisting of an SOFC and a heat engine and considered the influence of multi-irreversibilities on the performance of the system [8]. Facchinetti et al. optimized an SOFC-gas turbine (GT) hybrid cycle fueled with hydrothermally gasified waste biomass based on the first law of thermodynamics and exergy analysis [9]. Chen et al. put forward a fuel cell-thermoelectric generator hybrid system and determined the optimal operation condition [10].

TIGs (thermionic generators) are a kind of solid state generators. Renewed interests of TIGs are aroused due to the recent advances in device designs [11], electrode technology [12], and the desire to develop a high temperature topping cycle for thermal power systems [13,14]. Compared with traditional power plants, TIGs use electrons as the working substance without mechanically moving parts [15–17] and have advantages in aspect of small cubage and high power density. Moreover, a TIG has better performance at high temperatures (>1000 K) [18] and is more suitable for constituting a hybrid system together with an SOFC than a semiconductor thermoelectric generator [19,20].

In the present paper, we will establish a new model of the hybrid system composed of an SOFC as a topping cycle and a TIG as a bottom cycle, analyze the effects of main irreversibilities on the

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Nomenclature			
$a$	ratio of areas	$R_L$	ratio of heat leak to waste heat
$a_L$	convective and/or conductive heat-leak coefficient, [W/(cm <sup>2</sup> ·K)]	$T$	temperature of SOFC, [K]
$A_0$	Richardson–Dushman constant, [A/(cm <sup>2</sup> ·K <sup>2</sup> )]	$T_0$	environment temperature, [K]
$A$	area, [cm <sup>2</sup> ]	$T_2$	temperature of TIG anode, [K]
$e$	quantity of electric charge, [C]	$V$	voltage, [V]
$E$	reversible voltage of fuel cell, [V]	<b>Greek letters</b>	
$E_{el}$	activation energy, [J/mol]	$\gamma$	pre-factor for exchange current density, [A/cm <sup>2</sup> ]
$F$	Faraday constant, [C/mol]	$\epsilon_0$	thermal emissivity
$\Delta h^\circ$	standard molar enthalpy change, [J/mol]	$\epsilon_L$	thermal emissivity
$\Delta h^\circ$	standard molar Gibbs free energy change, [J/mol]	$\eta$	efficiency
$\Delta \dot{H}$	enthalpy change, [W]	$\eta_{s,a}$	efficiency for given $a$
$i$	current density, [A/cm <sup>2</sup> ]	$\eta_{s,a,max}$	maximum efficiency for given $a$
$i_0$	exchange current density, [A/cm <sup>2</sup> ]	$\eta_{s,a,P}$	efficiency at maximum power output for given $a$
$i_L$	limiting current, [A/cm <sup>2</sup> ]	$\eta_{s,max}$	maximum efficiency
$i_{V,c}$	cutting current density for given voltage, [A/cm <sup>2</sup> ]	$\eta_{s,P}$	efficiency at maximum power output
$i_{a,c}$	cutting current density for given ratio of areas, [A/cm <sup>2</sup> ]	$\eta_{s,V}$	efficiency for given $V$
$I$	electric current, [A]	$\eta_{s,V,max}$	maximum efficiency for given $V$
$k_B$	Boltzmann constant, [J/K]	$\sigma$	Stefan–Boltzmann constant, [W/(cm <sup>2</sup> ·K <sup>4</sup> )]
$L_{el}$	electrolyte thickness, [μm]	$\sigma_0$	reference ionic conductivity, [S/cm]
$n_e$	number of electrons	$\Phi_c$	work function of TIG anode, [eV]
$p$	composition pressure, [atm]	$\Phi_h$	work function of TIG cathode, [eV]
$p_0$	standard atmospheric pressure, [atm]	<b>Subscripts</b>	
$P$	power output, [W]	$a$	anode
$P_{s,a}$	power output for given $a$ , [W]	$act$	activation
$P_{s,a,max}$	maximum power output for given $a$ , [W]	$BV$	Butler–Volmer equation
$P_{s,max}$	maximum power output, [W]	$c$	cathode
$P_{s,V}$	power output for given $V$ , [W]	$conc$	concentration
$P_{s,V,max}$	maximum power output for given $V$ , [W]	$el$	electrolyte
$P_{s,V,\eta}$	power output at maximum efficiency for given $V$ , [W]	$f$	SOFC
$P_{s,\eta}$	power output at maximum efficiency, [W]	$h$	TIG cathode
$q$	heat flow, [W]	$ohm$	ohmic
$q_c$	heat flow through TIG anode, [W]	$P$	maximum power output
$q_L$	heat leak, [W]	$s$	hybrid system
$q_w$	waste heat of SOFC, [W]	$t$	TIG
$R$	universal gas constant, [J/(mol·K)]	$\eta$	maximum efficiency

performance of the system, and determine the optimal ranges of key parameters. It is expected that the results obtained are of interest for readers in the research fields of fuel cells.

## 2. An SOFC-TIG hybrid system

Fig. 1 shows the schematic diagram of a hybrid system composed of an SOFC, a TIG, and a regenerator. In the hybrid system, the SOFC can produce power as well as act as the hot reservoir of the TIG. By using hydrogen as fuel and oxygen as an oxidant, the fuel cell can generate electricity via an electrochemical reaction. The regenerator is used to preheat the incoming gas and air. By using effectively a part of the waste heat produced in the fuel cell, the TIG can export an additional power. As a result, the hybrid system can obtain better performance than any one subsystem. In the hybrid system, it is assumed that the temperatures of the SOFC and the cathode of the TIG are uniform because it was experimentally demonstrated that the cell voltage variation caused by non-uniform temperature distribution of the SOFC can be controlled to be smaller than 1% [21]. It is further assumed that the temperature of the anode of the TIG is also kept to be constant through the control of the heat-transfer area and the electrodes of

the TIG have the same inside area. It should be pointed out that it needs several hours for an SOFC to reach the working temperature from the room temperature [22,23]. Thus, the proposed model and

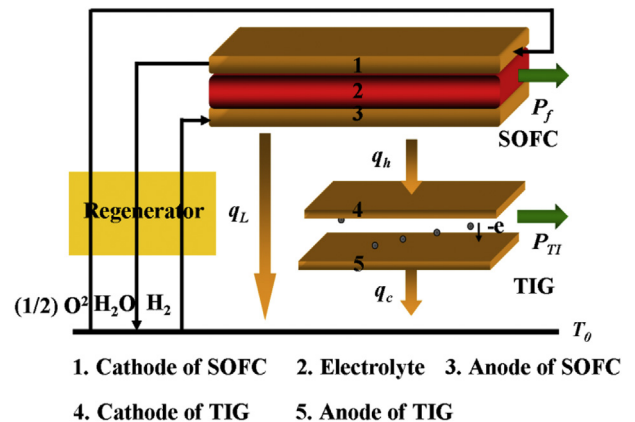


Fig. 1. The schematic diagram of an SOFC-TIG hybrid system.

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