



Egyptian Petroleum Research Institute  
Egyptian Journal of Petroleum

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FULL LENGTH ARTICLE

# Process engineering optimization of nanofiltration unit for the treatment of textile plant effluent in view of solution diffusion model



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Received 11 December 2014; revised 25 February 2015; accepted 9 March 2015  
Available online 9 January 2016

## KEYWORDS

Nanofiltration;  
Spiral-wound membrane;  
Dye-house wastewater;  
Color and COD removal;  
Solution diffusion model

**Abstract** A nanofiltration (NF) based separation process is used to treat the effluent from a textile plant to allow for water reuse and fulfill environmental standards. The wastewater effluent contains reactive black (RB5)- and disperse (DR60) dyes. A NF-unit model E2 series with HL 2521 TF spiral wound module was used to carry out experiments. 90 & 93% color removal and COD reduction for RB5 and 98 & 95% for DR60 were achieved. A parametric study of the separation process is undertaken to characterize the effects of the operating variables, e.g., trans-membrane pressure, dye/salt concentration in the feed, temperature, and cross flow velocity. The solution diffusion model was used to develop power correlations to calculate the permeate side solute mass transfer coefficient as a function of effective cross-flow Reynolds number. In contrast to the commonly assumed constant hydraulic solvent permeability, a non-linear relationship was developed over the applied trans-membrane net driving pressure. The latter correlates exponentially with salt permeability for both dyes. The effects of feed salt-content on solute mass transfer coefficient, water and salt permeability, concentration polarization, dye hydrophobicity and ionic strength were studied. Results were used to assess engineering specifications of a commercial size NF-plant (500 m<sup>3</sup>/d capacity).

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Peer review under responsibility of Egyptian Petroleum Research Institute.

<http://dx.doi.org/10.1016/j.ejpe.2015.03.018>

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## 1. Introduction

Weaving, textile and dying industry represent one of the most important economic sectors in Egypt whose production exceeds \$5 billion in 2012. The latter constitutes 25% of the Egyptian gross domestic production. The textile fabrics – particularly

**Nomenclature**

$A$	membrane area ( $\text{m}^2$ )	$(P_f - P_p)$	pressure difference across the membrane (bar)
$A_{eff}$	effective area ( $\text{m}^2$ )	$Q_f$	feed flow rate (L/h)
$b$	leaf width (m)	$Q_c$	concentrate flow rate (L/h)
$c_{if}$	concentration of component $i$ in the feedstock (mg/L)	$Q_p$	permeate flow rate (L/h)
$c_{ip}$	concentration of component $i$ in the permeate (mg/L)	$R$	universal gas constant ( $\text{bar m}^3/\text{mol } ^\circ\text{C}$ )
$c_{sp}$	concentration of adsorbate on the membrane at equilibrium (mol/kg)	$Re_{eff}$	effective cross flow Reynolds number on permeate side (–)
$c_{dsp}$	total dissolved adsorbate concentration remaining in the solution at equilibrium ( $\text{mg}/\text{m}^3$ )	$Re_c$	effective cross flow Reynolds number on concentrate side (–)
$\bar{C}$	average salinity on the feed side (mg/L)	$R_m$	membrane hydraulic resistance ( $\text{m}^{-1}$ )
$C_f$	dye/salt feed concentration (mg/L)	$R_{non-rec}$	any non-recoverable resistance developed during filtration ( $\text{m}^{-1}$ )
$C_c$	concentrate concentration (mg/L)	$S_{fc}$	wetted surface of the flat channel ( $\text{m}^2$ )
$C_p$	permeate concentration (mg/L)	$S_{sp}$	wetted surface of the spacer ( $\text{m}^2$ )
$d_h$	hydraulic diameter ( $\text{m}^2$ )	$Sc$	Schmidt number (–)
$D$	solute diffusion coefficient in water ( $\text{m}^2/\text{s}$ )	$Sh$	Sherwood number (–)
$DR$	dye rejection (%)	$SR$	salt rejection (%)
$h$	channel height ( $\text{m}^2$ )	$T$	operating temperature ( $^\circ\text{C}$ )
$h_{sp}$	spacer thickness ( $\text{m}^2$ )	$U$	fluid linear velocity (m/s)
$J_p$	permeate flux ( $\text{L}/\text{m}^2 \text{ h}$ )	$u_{eff}$	effective cross flow fluid velocity (m/s)
$J_s$	salt flux ( $\text{kg}/\text{m}^2 \text{ sh}$ )	$V_{fc}$	volume of the flat channel ( $\text{m}^3$ )
$k$	mass transfer coefficient (m/s)	$V_{Tot}$	total volume ( $\text{m}^3$ )
$k_p$	permeate – side mass transfer coefficient (m/s)	$V_{sp}$	volume of the spacer ( $\text{m}^3$ )
$K_{sp}$	membrane sorption coefficient ( $\text{m}^3/\text{kg}$ )	<b>Greek symbols</b>	
$K_s$	salt permeability coefficient (m/s)	$\rho$	fluid density ( $\text{kg}/\text{m}^3$ )
$K_w$	water permeability coefficient ( $\text{m}^3/\text{m}^2 \text{ s bar}$ )	$\mu$	dynamic viscosity of the solution ( $\text{kg m}^{-1} \text{ s}^{-1}$ )
$l$	membrane thickness (m)	$\sigma$	osmotic reflection coefficient (–)
$L$	channel length (m)	$\vartheta_i$	molar volume of component $i$ ( $\text{m}^3/\text{mol}$ )
$M_s$	rate of solid flow through the membrane ( $\text{kg}/\text{s}$ )	$\Delta\pi$	net osmotic pressure differential across the membrane (bar)
$NDP$	net driving pressure (bar)	$\bar{\pi}$	average osmotic pressure on the feed side (bar)
$P$	operating pressure (bar)	$\pi_f$	osmotic pressure on the feed side (bar)
$\Delta P$	net hydraulic pressure differential across the membrane (bar)	$\pi_p$	osmotic pressure on the permeate side (bar)
$\bar{P}$	average hydraulic pressure side (bar) on the feed	$\pi_c$	osmotic pressure on the concentrate side (bar)
$P_f$	hydraulic pressure on the feed side (bar)	$\varepsilon$	porosity (–)
$P_p$	hydraulic pressure on the permeate side (bar)	$\tau$	payback period (year)
$P_c$	hydraulic pressure on the concentrate side (bar)		

dye houses – are frequently considered as one of the most hazardous water-polluting sources in Egypt.

Their wastewater usually contains residuals of dyestuffs, detergents, sulfide compounds, solvents, heavy metals and inorganic salts whose concentrations are beyond environmental allowances. Compliance with Egyptian environmental laws oblige such fabrics to practice treatment units to verify environmental standards [1,2].

The waste effluent contaminants are based on the type of the process being used [3,4] and cannot be directly discharged to receiving water bodies due to their dramatic harmful impact on the environment [5–10]. Dyestuff-effluents as the major toxic polluting source are usually subjected to conventional biological treatment by activated sludge. The latter does not meet great success as most of dyes resist aerobic biological treatment and chemical oxidation [3].

An advanced treatment technology is therefore necessary, especially if reuse of treated wastewater and de-colorization

are objectives [11]. Membrane filtration can be considered as an optimal solution to remove color, COD and salinity [12,13]. Nanofiltration (NF) has proved high reliability in many waste water purification purposes [14–17]. NF-process is an efficient color removing technology, reducing the volume of generated wastewater, recovering and recycling valuable constituents. It functions by both pore size flow and the solution diffusion mechanism [18,19].

The present work is concerned with the study of the performance of low pressure NF-membrane unit for treating dye-house effluents from El-Alamia Company for Textile and Dying (10th of Ramadan Industrial City) aiming to: (i) recycle water permeate for reuse, (ii) recovery of residual dyestuffs in concentrate stream, and (iii) reduction of pollution impacts to conform with environmental standards.

Wastewater effluents of dyed-cotton and polyester were thoroughly analyzed for pH, COD, TSS, and TDS according to standard analytical procedures, with HACH spectrophotometer

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