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Extended optical theorem for scalar monochromatic acoustical beams of arbitrary wavefront in cylindrical coordinates

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ABSTRACT

One of the fundamental theorems in (optical, acoustical, quantum, gravitational) wave scattering is the optical theorem for plane waves, which relates the extinction cross-section to the forward scattering complex amplitude function. In this analysis, the optical theorem is extended for the case of 3D-beams of arbitrary character in a cylindrical coordinates system for any angle of incidence and any scattering angle. Generalized analytical expressions for the extinction, absorption, scattering cross-sections and efficiency factors are derived in the framework of the scalar resonance scattering theory for an object of arbitrary shape. The analysis reveals the presence of an interference scattering cross-section term, which describes interference between the diffracted or specularly reflected inelastic (Franz) waves with the resonance elastic waves. Moreover, an alternate expression for the extinction cross-section, which relates the resonance cross-section with the scattering cross-section for an impenetrable object, is obtained, suggesting an improved method for particle characterization. Cross-section expressions are also derived for known acoustical wavefronts centered on the object, defined as the on-axis case. The extended optical theorem in cylindrical coordinates can be applied to evaluate the extinction efficiency from any object of arbitrary geometry placed on or off the axis of the incident beam. Applications in acoustics, optics, and quantum mechanics should benefit from this analysis in the context of wave scattering theory and other phenomena closely connected to it, such as the multiple scattering by many particles, as well as the radiation force and torque.

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1. Introduction

Scattering and absorption are the two most significant mechanisms that affect wave propagation throughout a medium. Understanding the physical nature of these effects during wave transport allows adequate characterization of the medium of wave propagation by deconvolution of scattering and attenuation spectra.

The most rigorous description of these phenomena is interpreted by means of the so-called “optical theorem” (OT) [1–8], which constitutes a general law of wave scattering theory. It is otherwise known as the “extinction theorem” [7], which relates the extinction cross section of an object of arbitrary geometry placed in the field of monochromatic plane waves to its forward scattering amplitude, which is the scattered wave amplitude measured in the far field along the forward direction of wave propagation (p. 20 in [9]).

An analogous OT has been derived for the acoustical scattering by baffled membranes and plates in the direction of the specularly reflected waves [10], nonetheless, in scalar wave scattering

applications, there has been a need to account for the plane waves scattered at any angle, not only restricted to the forward or backwards directions. An integral relation for the angle-dependent scattering amplitude of plane waves has been therefore derived from the standpoint of quantum theory [11–13], which constitutes a “generalized optical theorem” (GOT). Subsequently, it has been applied in the context of electron diffraction theory [14], scalar optical [15] and evanescent waves [16], and acoustic backscattering by elastic targets (with no internal dissipation) having inversion symmetry [17]. Additional extensions for the GOT to study vectorial wave phenomena related to electromagnetic waves [18,19], elastic waves [20], surface waves [21] and layered media [22] have been formulated as well.

The relevance of the GOT relies in the quantitative and accurate evaluation of cross sections rather than numerical integration procedures [8]. In essence, the extinction, scattering, and absorption cross sections (or power) are meaningful measures of the object scattering and absorption properties. As such, most practical applications and experimental methods (with some specific applications discussed in [23]), tools and devices involving wave scattering phenomena (such as medical, non-destructive, sonar

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85 and underwater imaging, multiphase flow characterization, spec-
86 troscopy and particle sizing in dilute suspensions, near-field
87 diffraction X-ray and ultrasonic tomography, microscopy, and
88 inverse scattering, to name a few) would benefit from an *extended*
89 GOT formalism, which accounts for the character of the incident
90 wavefront, as opposed to plane (unbounded) waves. For conven-
91 ience, it is termed; extended optical theorem (EOT).

92 An EOT has been formulated for quantum beams [24], optical
93 Gaussian beams [25] (and others of arbitrary shape [26]) that pos-
94 sess some degree of amplitude roll-off in the transverse direction,
95 since the classical OT is no longer valid for shaped beams. Along
96 that line of research, an acoustical EOT has been established for
97 any scalar beam (not only limited to non-diffracting beams [27])
98 of arbitrary character incident upon an object of arbitrary shape,
99 and for any incidence and scattering angles [23], based on the
100 partial-wave series expansion (PWSE) method in spherical coordi-
101 nates. Though the formalism developed in Ref. [23] is applicable to
102 any object of arbitrary shape, computing the extinction, scattering,
103 and absorption cross sections (or their corresponding efficiencies)
104 of elongated cylindrical-like objects with the EOT in spherical coordi-
105 nates, may lead to numerical instabilities and inaccuracies [28].
106 These challenges arise from taking a large number of spherical
107 partial-waves to fit a non-spherical cylindrical-like object [29] in
108 order to ensure proper convergence of the series. Nevertheless,
109 these complications should not be interpreted as a lack of rigor
110 of the PWSE formalism [23], rather the method in spherical coordi-
111 nates may not be entirely suitable from a computational stand-
112 point for the analysis of cylindrical-like objects with arbitrary
113 shape. Therefore, it is of some importance to develop an analytical
114 formalism suitable for elongated objects in cylindrical coordinates.

115 Here, a generalized formulation in cylindrical coordinates applica-
116 ble to any acoustical beam of arbitrary character in 3D is devel-
117 oped for a scatterer of arbitrary geometry and size, located
118 arbitrarily in space. Note that a related work for *optical/electromag-*
119 *netic* beams has been recently considered [30]. The EOT in cylindri-
120 cal coordinates provides generalized PWSEs for the extinction,
121 absorption, and scattering cross sections in terms of the non-
122 dimensional beam-shape and scattering coefficients of the object.
123 Furthermore, resonance, background and interference cross-
124 sections are defined in the framework of the generalized resonance
125 scattering theory for arbitrary beams, and their corresponding
126 analytical expressions are derived. Efficiency factors are also
127 computed for a viscoelastic cylinder centered on the axis of a
128 zeroth-order quasi-Gaussian beam, chosen as an example to
129 illustrate the theory.

130 2. Theoretical analysis

131 Consider a scalar acoustical beam of angular frequency ω
132 incident along an arbitrary direction on a viscoelastic object of
133 arbitrary geometry immersed in a non-viscous fluid (Fig. 1). A
134 time-dependence in the form of $e^{-i\omega t}$ is assumed, but omitted from
135 the equations for convenience.

136 For a 3D arbitrary-shaped beam composed of monochromatic
137 waves, the incident pressure field in the frequency domain can
138 be expressed in a cylindrical coordinates system as [31],
139

$$140 p_i(r, \theta, z, \omega) = p_0 \sum_{n=-\infty}^{+\infty} \left[\int_{-\infty}^{+\infty} b_n(k_z) J_n(k_r r) e^{ik_z z} dk_z \right] e^{in\theta}, \quad (1)$$

142 where p_0 is the pressure amplitude in the absence of the object, $J_n(\cdot)$
143 is the cylindrical Bessel function of the first kind, k_r and k_z are
144 the radial and axial wave-numbers, respectively, defined as
145 $k^2 = k_r^2 + k_z^2$ [31], where k is the wavenumber of the incident radi-
146 ation (for a 2D beam, k_z is a discrete (real) number [32]). The param-
147 eters r and θ are the radial distance and polar angle in the (x, y)

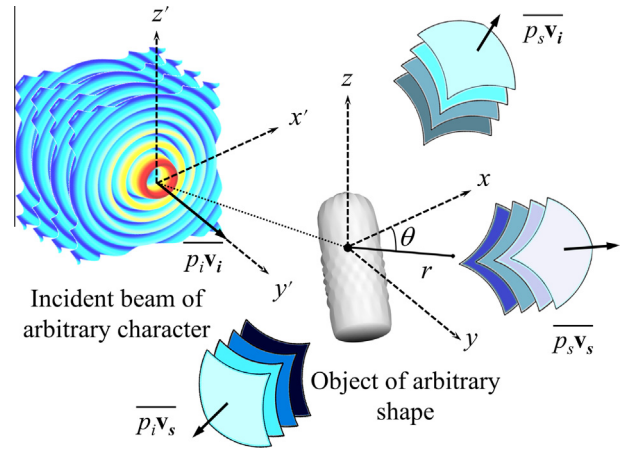


Fig. 1. An elongated object of arbitrary shape placed in the field of an incident acoustical beam of arbitrary wavefront in cylindrical coordinates (r, θ, z) . The primed coordinate system has its origin at the center of the beam, while the unprimed coordinate system is referenced to the object.

148 plane, respectively. In the generalized case of an object of arbitrary
149 shape in 3D, the radial distance $r = r(\theta, z)$. The factors $b_n(k_z)$ corre-
150 spond to the beam-shape coefficients (BSCs) that solely describe the
151 incident beam of arbitrary wavefront. They are determined as fol-
152 lows; first, the relationship of the two-dimensional Fourier trans-
153 form (in θ and z) of the incident pressure field $\mathcal{F}\{p_i\}$ is derived.
154 Then, its inverse function $\mathcal{F}^{-1}\{\mathcal{F}\{p_i\}\}$ is expressed in terms of a
155 Fourier series and a transform (p. 125 in [31]), and the result is
156 equated with Eq. (1), leading to the expression,
157

$$158 b_n(k_z) = \frac{1}{(2\pi)^2 p_0 J_n(k_r r)} \int_0^{2\pi} \left[\int_{-\infty}^{+\infty} p_i(r, \theta, z, \omega) e^{-ik_z z} dz \right] e^{-in\theta} d\theta. \quad (2)$$

160 If a given beam expression for the incident pressure is an exact solu-
161 tion of the Helmholtz's equation, the r dependence in Eq. (2) cancels
162 out, and the BSCs are functions of k_z and n alone.

163 The scattered wave can be represented by a scattered pressure
164 field expressed as,
165

$$166 p_s(r, \theta, z, \omega) = p_0 \sum_{n=-\infty}^{+\infty} \left[\int_{-\infty}^{+\infty} b_n(k_z) C_n H_n^{(1)}(k_r r) e^{ik_z z} dk_z \right] e^{in\theta}, \quad (3)$$

168 where $H_n^{(1)}(\cdot)$ is the cylindrical Hankel function of the first kind of
169 order n , and C_n are the non-dimensional scattering coefficients that
170 depend on the mechanical properties of the object of arbitrary
171 shape and the surrounding nonviscous fluid. When the object takes
172 the form of a circular cylinder, the radial distance r is constant
173 (independent of θ and z), and the scattering coefficients C_n can
174 be exactly described in terms of known cylindrical Bessel, Neumann
175 and Hankel functions and their derivatives, as well as the mechan-
176 ical properties of the cylindrical material [33].

177 It proves convenient to use the far-field expressions for the inci-
178 dent and scattered acoustic fields in a nonviscous fluid to evaluate
179 the cross-sections, by using the asymptotic limits for the cylindri-
180 cal Bessel and Hankel functions with large arguments. Thus, in the
181 far-field limit, Eqs. (1) and (3) become
182

$$183 p_i(r, \theta, z, \omega) \approx_{k_r r \rightarrow \infty} p_0 \sum_{n=-\infty}^{+\infty} \left[\int_{-\infty}^{+\infty} \sqrt{\frac{2}{\pi k_r r}} b_n \cos\left(k_r r - \frac{n\pi}{2} - \frac{\pi}{4}\right) e^{ik_z z} dk_z \right] e^{in\theta}, \quad (4)$$

$$184 p_s(r, \theta, z, \omega) \approx_{k_r r \rightarrow \infty} p_0 \sum_{n=-\infty}^{+\infty} \left[\int_{-\infty}^{+\infty} \sqrt{\frac{2}{i\pi k_r r}} b_n C_n e^{i(k_z z + k_r r)} dk_z \right] i^{-n} e^{in\theta}. \quad (5)$$

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