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# The end-of-life disposal of satellites in libration-point orbits using solar radiation pressure

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### Abstract

This paper proposes an end-of-life propellant-free disposal strategy for libration-point orbits which uses solar radiation pressure to restrict the evolution of the spacecraft motion. The spacecraft is initially disposed into the unstable manifold leaving the libration-point orbit, before a reflective sun-pointing surface is deployed to enhance the effect of solar radiation pressure. Therefore, the consequent increase in energy prevents the spacecraft's return to Earth. Three European Space Agency missions are selected as test case scenarios: Herschel, SOHO and Gaia. Guidelines for the end-of-life disposal of future libration-point orbit missions are proposed and a preliminary study on the effect of the Earth's orbital eccentricity on the disposal strategy is shown for the Gaia mission. © 2015 COSPAR. Published by Elsevier Ltd. All rights reserved.

Keywords: End-of-life disposal; Solar radiation pressure; Circular restricted-three body problem; Elliptic restricted-three body problem; Zero-velocity curves

## 1. Introduction

Libration-point orbit (LPO) missions are often selected for studying the Sun and the Universe. Orbits around the Libration points  $L_1$  and  $L_2$  of the Sun–Earth system are advantageous as they can be reached from the Earth and, since a constant sky field of view is ensured with respect to the Sun and the Earth, they are frequently used for space observation. There are also further advantages regarding the ease of Earth communication and in the thermal system design. However, they lie in highly perturbed regions; therefore, an uncontrolled spacecraft would naturally follow the unstable manifold and after several years could cross the protected regions at the Earth and the  $L_1/L_2$ regions. In addition, since LPO spacecraft are characterised by large dry masses, it is critical to clear these regions once the mission has ended.

Possible disposal strategies for LPO missions were investigated as a result of a European Space Agency (ESA) study on end-of-life (EOL) disposal concepts for Lagrange-point and Highly Elliptical Orbit Missions. The natural multi-body dynamics in the Earth environment and in the Sun–Earth system were exploited. The main idea is to either restrict the motion of the spacecraft to specific regions or to destroy the spacecraft through an impact with another body. The options investigated were Earth's re-entry, injection onto trajectories towards a Moon impact, heliocentric parking orbit by means of  $\Delta v$  or

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Abbreviations: AU, astronomical unit; CR3BP, circular restricted three body problem; EOL, end-of-life; ER3BP, elliptic restricted three body problem; ESA, European Space Agency; GEO, Geosynchronous Equatorial Orbit; JAXA, Japan Aerospace Exploration Agency; LPO, librationpoint orbit; SRP, solar radiation pressure; ZVC, zero velocity curve.

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## Nomenclature

$L_j/SL_j$ <i>j</i> th collinear Lagrangian/Pseudo-Lagrangian	$\Delta E$ variation of energy between the spacecraft and
point with $j = 1, \dots, 5$ U total notantial analysis which includes the notat	$L_j$ of $SL_j$
U total potential energy which includes the rotat-	$E_{SL_j}$ energy of the pseudo-Lagrangian point
ing system potential and the gravitational poten-	$\Delta \beta$ contribution of the increased area of the space-
tial	craft after the deployment where $\beta = \beta_0 + \Delta\beta$
$U_s$ potential of SRP	<i>V</i> magnitude of the spacecraft's velocity
x, y and z derivatives with respect to x, y and z	$V_{clsr}$ spacecraft's velocity required after the $\Delta v$
$r_{Sun-p}$ and $r_{Earth-p}$ spacecraft (p) and Sun and Earth	manoeuvre
distances respectively	$\Delta v_{eq}$ theoretical $\Delta v$
$m_{Earth}$ Earth's mass [kg]	<i>R</i> correspond to 60,000 [km]
M <sub>Sun</sub> Sun's mass [kg]	$d_{Earth-p}$ spacecraft-Earth distance
$\mu$ mass parameter $(m_{Earth}/(M_{Sun}+m_{Earth}))$ for the	$\mathbf{r}_{Earth}$ and $\mathbf{r}_p$ distances of the Earth and the spacecraft
Sun-(Earth+Moon) system is equal to	from the center of mass
$3.04042 \cdot 10^{-6}$	$A_0$ initial spacecraft's deployable area [m <sup>2</sup> ]
$x_{Sun}$ and $x_{Earth}$ Sun $(-\mu)$ and Earth $(1-\mu)$ positions	$m_{dry}$ dry mass [kg]
respectively	$A_0/m_{dry}$ initial area-to-mass ratio $[m^2 kg^{-1}]$
$\mu_{Sun}$ and $\mu_{Earth}$ Sun $(1 - \mu)$ and Earth $(\mu)$ unit masses	<i>r</i> Earth+Moon distance from the Sun [km]
respectively	a semimajor axis [km]
<i>m</i> spacecraft's mass [kg]	f true anomaly [rad]
A spacecraft's reflective area $[m^2]$	<i>e</i> Earth's orbit eccentricity
$\sigma$ mass-to-area ratio $(m/A)$ [kg m <sup>-2</sup> ]	$\dot{f}$ angular velocity [rad s <sup>-1</sup> ]
$\sigma^*$ Sun luminosity, 1.53 [g m <sup>-2</sup> ]	h angular momentum $[\text{km}^2 \text{ s}^{-1}]$
$\beta$ lightness parameter $(\sigma^*/\sigma)$	M <sub>Earth+Moon</sub> Earth+Moon mass [kg]
$c_R$ reflective coefficient	G constant of gravitation $[N m^2 kg^{-2}]$
$P_{srp-1AU}$ Sun pressure at 1 AU	$\tilde{\mu} \qquad G \cdot (M_{Sun} + M_{Earth+Moon}) [\text{km}^3 \text{ s}^{-2}]$
$r_{Earth-Sun}$ Earth to Sun distance	$\omega, \Omega$ and $\Omega'$ potential energy in the ER3BP
$x_{SL}$ position of the collinear pseudo-Lagrangian	$\mathbf{r}_d$ and $\mathbf{\dot{r}}_d$ dimensional position [km] and velocity
point	$[\text{km s}^{-1}]$ coordinates
<i>E</i> energy of the system	r and $r'$ non-dimensional pulsating position and velocity
$\beta_0$ lightness parameter for the spacecraft's initial	coordinates
dry area-to-mass ratio	I energy integral
$\Delta v$ variation in the spacecraft's velocity after a	$f_0$ initial true anomaly when leaving the LPO [rad]
manoeuvre	, , , ,

heliocentric parking orbit by means of solar radiation pressure (SRP) (Colombo et al., 2015, 2014).

Olikara et al. (2013) initially proposed a disposal option, which injects the spacecraft towards the inner or the outer solar system and closes the Hill's surfaces though a  $\Delta v$ manoeuvre at  $L_1$  or  $L_2$ . Olikara et al. (2013) suggested that the overall return trajectories to the Earth in the circular restricted three body problem (CR3BP) and in the full-body (ephemerides) are quite similar.

In this article, an alternative disposal strategy is investigated that allows the closure of the zero-velocity curves by means of SRP. In this case, the spacecraft is disposed at the EOL onto the unstable manifold leaving the LPO from  $L_2$ . An energetic approach is used to close the Hill's curves at  $SL_2$  (e.g., the pseudo Libration-point  $L_2$  when SRP is added (McInnes, 2000)) by increasing the energy of the system and then computing the reflective deployable area required for the EOL curves-closure. As a term due to SRP is added to the energy, the shape of the potential

energy of the pseudo-Lagrangian point contribution of the increased area of the spacecraft after the deployment where  $\beta = \beta_0 + \Delta \beta$ nagnitude of the spacecraft's velocity spacecraft's velocity required after the  $\Delta v$ nanoeuvre heoretical  $\Delta v$ correspond to 60,000 [km] pacecraft-Earth distance  $r_p$  distances of the Earth and the spacecraft rom the center of mass nitial spacecraft's deployable area [m<sup>2</sup>] lry mass [kg] nitial area-to-mass ratio  $[m^2 kg^{-1}]$ Earth+Moon distance from the Sun [km] emimajor axis [km] rue anomaly [rad] Earth's orbit eccentricity angular velocity [rad s<sup>-1</sup>] angular momentum [km<sup>2</sup> s<sup>-1</sup>] on Earth+Moon mass [kg] constant of gravitation [N m<sup>2</sup> kg<sup>-2</sup>]  $G \cdot (M_{Sun} + M_{Earth+Moon}) \, [\mathrm{km}^3 \, \mathrm{s}^{-2}]$  $\Omega'$  potential energy in the ER3BP  $\dot{\mathbf{r}}_d$  dimensional position [km] and velocity km s<sup>-1</sup>] coordinates non-dimensional pulsating position and velocity coordinates energy integral nitial true anomaly when leaving the LPO [rad]

surfaces changes and the required reflective area is computed via numerical optimisation, imposing the condition for the curves closure at SL<sub>2</sub>. After the closure, the spacecraft is bounded in its following motion at the right-hand side of the pseudo Libration point, thus, preventing the spacecraft's return to the Earth and protecting the  $L_2$ region. It is also demonstrated that the spacecraft cannot be confined towards the inner solar system due to the constraint in the direction of SRP acceleration and that the disposal through SRP can only be performed at SL<sub>2</sub>. This strategy can be achieved through a sun-pointing auto-stabilised deployable structure, such as light reflective surfaces that are already proven for attitude control applications (e.g., GOES's cone solar sail<sup>1</sup> (DRL-101-08, 1996)), with the advantage of saving propellant.

<sup>1</sup> The cone shape of the sail guarantees attitude passive stabilisation.

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