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# Varistor and dielectric properties of Cr<sub>2</sub>O<sub>3</sub> doped SnO<sub>2</sub>–Zn<sub>2</sub>SnO<sub>4</sub> composite ceramics

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#### A R T I C L E I N F O

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## $A \hspace{0.1in} B \hspace{0.1in} S \hspace{0.1in} T \hspace{0.1in} R \hspace{0.1in} A \hspace{0.1in} C \hspace{0.1in} T$

Cr<sub>2</sub>O<sub>3</sub> doped SnO<sub>2</sub>–Zn<sub>2</sub>SnO<sub>4</sub> composite ceramics were prepared by traditional ceramic processing and the varistor, dielectric properties were investigated. With increasing Cr<sub>2</sub>O<sub>3</sub> content, the breakdown electrical field  $E_B$  increases from 11 to 92 V/mm and the relative dielectric constant  $e_r$  measured at 1 kHz, 50 °C decreases from 11,028 to 3412, respectively. The barrier height  $\phi_B$  about 0.8–0.84 eV and the decreasing of SnO<sub>2</sub> grain size suggest that the varistor behavior with high  $e_r$  is originated from SnO<sub>2</sub> –SnO<sub>2</sub> or SnO<sub>2</sub>–Zn<sub>2</sub>SnO<sub>4</sub> grain boundary. In the dielectric spectra lower than 1 kHz, a dielectric constant also presents a dielectric peak in the temperature spectra and the peak becomes faint with increasing frequency. The exhibition of the dielectric peak is thought to be attributed to the conduction of grain boundary since it is accompanied by the sharp increase of dielectric loss. In addition, a dielectric relaxation with the activation energy about 0.4–0.5 eV was observed in the temperature range of 20 –100 °C. Based on the results, the formation mechanism of Schottky barriers at grain boundaries and the varistor behavior with high dielectric constant are well understood.

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## 1. Introduction

A varistor is a voltage-dependent resistor whose primary function is to sense and limit transient-voltage surges and hence, protect sensitive-state components. With the miniaturization and integration of electronic devices, varistor materials of multiple properties have attracted much attention for both scientific understanding and their numerous technological applications. For example, varistors with low breakdown voltage and high permittivity can be used as protectors to absorb the sparks in electrical micro-machines. Such typical and widely studied varistor materials are SrTiO<sub>3</sub> and TiO<sub>2</sub> ceramics [1–6]. In 2005, we discovered that without any doping, the composite SnO<sub>2</sub>–ZnO ceramics have electrical properties similar to SrTiO<sub>3</sub> and TiO<sub>2</sub> varistors [7]. Further study revealed that the varistor behavior is also a grain boundary barrier effect and ZnO has synthesized with SnO<sub>2</sub> during sintering, virtually, the composite ceramics are composed of SnO<sub>2</sub>, Zn<sub>2</sub>SnO<sub>4</sub>

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[8]. Recently, we found that the oxygen vacancies are the key factor to the formation of grain boundary barriers [9]. However, the electrical properties of SnO<sub>2</sub> and Zn<sub>2</sub>SnO<sub>4</sub> grains, the original mechanisms of the varistor and high permittivity behavior are not clearly understood up to now. For SnO<sub>2</sub> and ZnO ceramics, the varistor properties can be greatly improved by doping  $Cr_2O_3$  [10–13] and in this paper, the varistor and dielectric properties of  $Cr_2O_3$  doped SnO<sub>2</sub>–Zn<sub>2</sub>SnO<sub>4</sub> composite ceramics were investigated.

### 2. Experimental procedure

The ceramic samples with the compositions 0.8 mol  $SnO_2 + 0.2$  mol  $Zn_2SnO_4 + x$  mol%  $Cr_2O_3$  (x = 0, 0.02, 0.04, 0.06, 0.08) were prepared using analytical grades of  $SnO_2$ , ZnO and  $Cr_2O_3$ . Zn<sub>2</sub>SnO<sub>4</sub> was synthesized using  $SnO_2$  and ZnO powders at 1000 °C for 1 h. The chemicals were mixed in a nylon bottle for 12 h using ZrO<sub>2</sub> milling media in distilled water. The dried powders were mixed with 6% weight of polyvinyl alcohol (PVA) binder and pressed into 15 mm diameter disks with 1.5 mm thickness at 200 MPa. After burning out the PVA binder at 650 °C for 2 h, the disks were sintered at 1400 °C for 1 h. To measure the electrical







properties, silver electrodes were made on both surfaces of the sintered disks.

The microstructure of the sample surfaces was analyzed by scanning electron microscopy (SEM) (JSM-5900). For the measurement of electrical characterization of current density versus applied electrical field, Source Meter (Keithley 2410) was used. The permittivity spectra were measured from 40 Hz to 1 MHz with a bias voltage varied from 0 to 40 V by the impedance analyzer (Agilent 4294A). The temperature spectra of the dielectric properties were measured during the temperature range of 18–350 °C from  $10^2$  to  $10^{5.5}$  Hz (316 kHz).

## 3. Results and discussion

Fig. 1 shows the SEM micrographs for the samples of x = 0, 0.02, 0.04, 0.06. Besides dense structure, it can be observed that the size of the smooth-faced grains decreases apparently with increasing Cr<sub>2</sub>O<sub>3</sub> content, whereas, the small angular grains (as indicated by the ellipses) change slightly. It has been validated that the smooth-faced and small angular grains are composed of SnO<sub>2</sub> and Zn<sub>2</sub>SnO<sub>4</sub>, respectively [8]. That is, the SnO<sub>2</sub> grain growth is hindered by doping Cr<sub>2</sub>O<sub>3</sub>. The radius of Cr<sup>3+</sup> is 0.063 nm, which is smaller than that of Sn<sup>4+</sup> (0.071 nm) ions. As a result, some Cr<sup>3+</sup> substituting Sn<sup>4+</sup> brings lattice distortion; the remanent ions may accumulate in the grain boundary and the both factors are disadvantageous for the growth of grains.

The voltage–current relations are illustrated in Fig. 2. As can be seen, all the samples have varistor properties and the breakdown electrical field  $E_B$  increases obviously with increasing  $Cr_2O_3$  content. The variation of  $E_B$  is thought to be related to the decrease of SnO<sub>2</sub> grain size since it can be expressed by Equation (1):

$$E_{\rm B} = n \cdot V_{\rm g}.\tag{1}$$

In Equation (1), *n* is the average grain number per unit length,  $V_g$  is the breakdown voltage of one grain boundary. Because the composite ceramic varistor is composed of SnO<sub>2</sub> and Zn<sub>2</sub>SnO<sub>4</sub>



Fig. 2. *E*–*J* character of the samples doped with different Cr<sub>2</sub>O<sub>3</sub> content.

grains and  $E_B$  is affected greatly by SnO<sub>2</sub> grain size, it is reasonable to conclude that the varistor property must be mainly originated from SnO<sub>2</sub>–SnO<sub>2</sub> or SnO<sub>2</sub>–Zn<sub>2</sub>SnO<sub>4</sub> grain boundary. It is worth to note that the sample without doping has the lowest  $E_B$  value about 10 V/mm which is very important to low voltage protections. The grain size effect can also be confirmed by the dielectric spectra as shown in Fig. 3(a). At low frequency,  $\varepsilon_r$  decreases from about 13k to 6k with increasing x and it is proportional to the grain size d as described in Equation (2) [14].

$$\varepsilon_{\rm r} = \varepsilon_{\rm B} d/t_{\rm B}.\tag{2}$$

In Equation (2),  $\varepsilon_{\rm B}$  is the internal permittivity of the barrier material,  $t_{\rm B}$  is the mean thickness of the insulation barrier. Usually, the origination of large permittivity for varistor materials is mainly attributed to the grain boundary layer where located the back to



Fig. 1. SEM micrographs of SnO<sub>2</sub>-Zn<sub>2</sub>SnO<sub>4</sub> composite ceramics doped with different Cr<sub>2</sub>O<sub>3</sub> content, some of the Zn<sub>2</sub>SnO<sub>4</sub> grains are emphasized using the ellipse.

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