

## Structure and magnetoelectric property of low-temperature sintering $(\text{Ni}_{0.8}\text{Zn}_{0.1}\text{Cu}_{0.1})\text{Fe}_2\text{O}_4/[0.58\text{PNN}-0.02\text{PZN}-0.05\text{PNW}-0.35\text{PT}]$ composites

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### ARTICLE INFO

#### Article history:

Received 23 December 2009

Received in revised form

14 June 2010

Accepted 16 June 2010

Available online 25 June 2010

#### Keywords:

Ceramic composites

Solid-state reaction method

X-ray diffraction

Electrical properties

Magnetoelectric property

### ABSTRACT

$(1-x)(\text{Ni}_{0.8}\text{Zn}_{0.1}\text{Cu}_{0.1})\text{Fe}_2\text{O}_4/x0.58\text{Pb}(\text{Ni}_{1/3}\text{Nb}_{2/3})\text{O}_3-0.02\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3-0.05\text{Pb}(\text{Ni}_{1/2}\text{W}_{1/2})\text{O}_3-0.35\text{PbTiO}_3$  ( $(1-x)\text{NZCF}/x\text{PNZNWT}$ ) magnetoelectric composites were prepared by conventional solid-state reaction method via low-temperature sintering technique. The low-temperature sintering technique can prepare dense composites, where the ferrite and piezoelectric phases coexist in the synthesized particulate composites, and no apparent mutual solubility takes place between the two phases. The  $(1-x)\text{NZCF}/x\text{PNZNWT}$  ceramic composites exhibit excellent integrated electrical properties, where diffused dielectric response peaks, typical P-E hysteresis loops and excellent piezoelectric property can be obtained. The  $(1-x)\text{NZCF}/x\text{PNZNWT}$  composites prepared by the low-temperature sintering process can be electrically and magnetically poled to exhibit apparent magnetoelectric effect, indicating that such technique is convenient to develop excellent particulate magnetoelectric materials in the future.

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## 1. Introduction

Magnetoelectric materials with coexistence of ferroelectric and ferromagnetic have attracted increasing interest due to their potential applications as multi-state memories, spintronics and heterogeneous read/write devices [1,2]. The magnetoelectric (ME) effect can be dated back to 1894, however, single-phase compounds exhibit poor inherent multiferroic coupling and low Neel or Curie temperature, which hinder their applications. Alternatively, multiferroic magnetoelectric composites composed of piezoelectric and magnetic materials have drawn significant interest in recent years, where the coupling interaction between the piezoelectric and magnetic materials could produce a large ME response [3–6]. Such excellent ME effect provides opportunities for potential applications as multifunctional devices such as magnetoelectric sensors, transducers and actuators.

As compared to single-phase magnetoelectric compounds, the ME effect in composites is extrinsic multiferroic response, which depends greatly on the composite microstructure and the coupling interaction across magnetic–piezoelectric interfaces. So far, 0–3 particulate and 2–2 laminate bulk magnetoelectric composites have

been investigated in experimental and theoretical [7–13]. The laminate structures exhibit the magnitude of  $V/(\text{cm Oe})$  ME voltage coefficient, which is two or three orders in magnitude of that of the single-phase ones and especially appropriate for commercial devices. However, due to the limitation in the feature size and miniaturizing difficulty of the layer structure, and the brittleness of ceramics, it is hard to prepare laminate composites. As a comparison, sintered particulate composites show inferior ME property due to the drawbacks such as low resistivity, interface diffusion, mismatch in elastic compliance, and degradation in individual material parameters. However, due to the advantages of cost effectiveness and fabrication process easiness, it practically and economically needs novel particulate magnetoelectric composites.

It is known that low anisotropy favors the magnetomechanical coupling in crystal, therefore,  $\text{NiFe}_2\text{O}_4$  with low anisotropy and high initial permeability is a promising candidate to give rise to the high ME effect. Furthermore, a larger net magnetic moment can be obtained by substituting some zinc into nickel ferrite, which also favors the ME effect [8]. On the other hand,  $\text{Pb}(\text{Ni}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-PbTiO}_3$  with the morphotropic phase boundary (MPB) composition is known to exhibit large piezoelectric response. Addition of slight content of  $\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$  can improve piezoelectric property and mechanical factor of the ferroelectric system [14].

In this paper, a novel particulate magnetoelectric composite consisting of ferromagnetic  $(\text{Ni}_{0.8}\text{Zn}_{0.1}\text{Cu}_{0.1})\text{Fe}_2\text{O}_4$  (NZCF) and

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relaxor-based ferroelectric  $0.58\text{Pb}(\text{Ni}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-}0.02\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-}0.05\text{Pb}(\text{Ni}_{1/2}\text{W}_{1/2})\text{O}_3\text{-}0.35\text{PbTiO}_3$  (PNZNWT) was prepared by conventional solid–state reaction method. To inhibit interdiffusion between the ferrite and piezoelectric phases,  $\text{WO}_3$  and  $\text{CuO}$  were used as sintering aids to decrease sintering temperature [15,16] and improve densification of the sintered particulate ceramic composites, which will improve the ME effect. The electrical properties and ME effect of the  $(1-x)\text{NZCF}/x\text{PNZNWT}$  composites were studied systematically together with the observation of microstructure and the analysis of chemical composition and elemental diffusion across the ferrite–piezoelectric interfaces in order to clarify the possible mechanism of the ME effect.

## 2. Experimental procedure

Particulate magnetoelectric ceramic composites  $(1-x)\text{NZCF}/x\text{PNZNWT}$  were prepared by conventional solid–state reaction method. Analytical-purity oxides,  $\text{NiO}$ ,  $\text{ZnO}$ ,  $\text{CuO}$ ,  $\text{Fe}_2\text{O}_3$ ,  $\text{PbO}$ ,  $\text{Nb}_2\text{O}_5$ ,  $\text{WO}_3$ , and  $\text{TiO}_2$ , were used as raw materials. To maintain stoichiometry the raw oxides were dried separately before weighing and the synthesized columbite precursors were weighed and introduced into the batch calculation. Stoichiometric mixture of  $\text{NiO}$ ,  $\text{ZnO}$ ,  $\text{CuO}$  and  $\text{Fe}_2\text{O}_3$  was ball-milled in distilled water for 12 h, and then the well-mixed slurry was filtrated, dried and calcined at  $1000^\circ\text{C}$  for 3 h to prepare ferrite NZCF. Ferroelectric PNZNWT was prepared by the columbite precursor method, where the columbite precursors,  $\text{NiNb}_2\text{O}_6$  and  $\text{ZnNb}_2\text{O}_6$ , were prepared by calcining of the stoichiometric mixtures of  $\text{NiO}$  and  $\text{Nb}_2\text{O}_5$ , and  $\text{ZnO}$  and  $\text{Nb}_2\text{O}_5$  at  $1000^\circ\text{C}$  for 4 h, respectively. Then the other oxides with the stoichiometric weight were added to the above precursors. After wet ball-milled using  $\text{ZrO}_2$  milling media, the well-mixed stoichiometric mixture was calcined at  $900^\circ\text{C}$  for 2 h to prepare perovskite PNZNWT.

$(1-x)\text{NZCF}/x\text{PNZNWT}$  composites were prepared by conventional ceramic processing using the above synthesized ferrite and ferroelectric precursors according to the formula  $(1-x)\text{NZCF}/x\text{PNZNWT}$  ( $x = 1.0, 0.9, 0.8$  and  $0.7$ , in weight ratio). The well-mixed powders were dry-pressed into pellets with the addition of 3 wt% polyvinyl alcohol (PVA) binder and sintered at  $950^\circ\text{C}$  for 2 h.  $\text{CuO}$  and  $\text{WO}_3$  were used as sintering aids, which could decrease sintering temperature of the particulate ceramic composites and improve densification and electrical properties of the sintered composites [15,16].

The sintered ceramic composites were ground and polished to obtain flat and parallel surfaces. Crystal structure of the sintered composites was characterized by X-ray diffraction measurement (XRD, D/max-2500/PC Rigaku X-ray Diffractometer). Microstructure was observed by scanning electron microscopy (SEM, Hitachi S-4800 Field Emission Scanning Electron Microscope) using free surfaces of the specimens. X-ray elemental analysis was performed by a INCA energy dispersive X-ray analysis (EDX) attached to the SEM equipment in order to identify any elemental interdiffusion across the ferrite–piezoelectric interfaces. For electrical properties measurements, silver paste was fired on both surfaces of the well-polished pellets to provide robust electrodes. Detailed electrical properties measurement procedures were described elsewhere [17].

## 3. Results and discussion

### 3.1. Phase structure and microstructure morphology

XRD patterns of the sintered  $(1-x)\text{NZCF}/x\text{PNZNWT}$  ceramic composites are shown in Fig. 1. The end members exhibit spinel and perovskite structure, respectively, where the characteristic

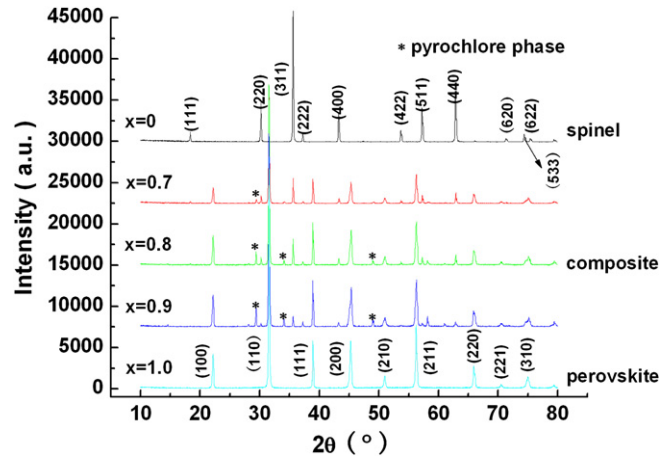


Fig. 1. XRD patterns of the  $(1-x)\text{NZCF}/x\text{PNZNWT}$  particulate ceramic composites sintered at  $950^\circ\text{C}$  for 2 h.

diffraction peaks can be indexed well based on the JCPDS data of spinel ferrite  $\text{NiFe}_2\text{O}_4$  and perovskite ferroelectric  $\text{Pb}(\text{Ni}_{1/3}\text{Nb}_{2/3})\text{O}_3$  (JCPDS files 34-0103 and 74-2081). In the composite compositions, the coexistence of ferrite NZCF and ferroelectric PNZNWT is confirmed by the XRD patterns, indicating that no apparent

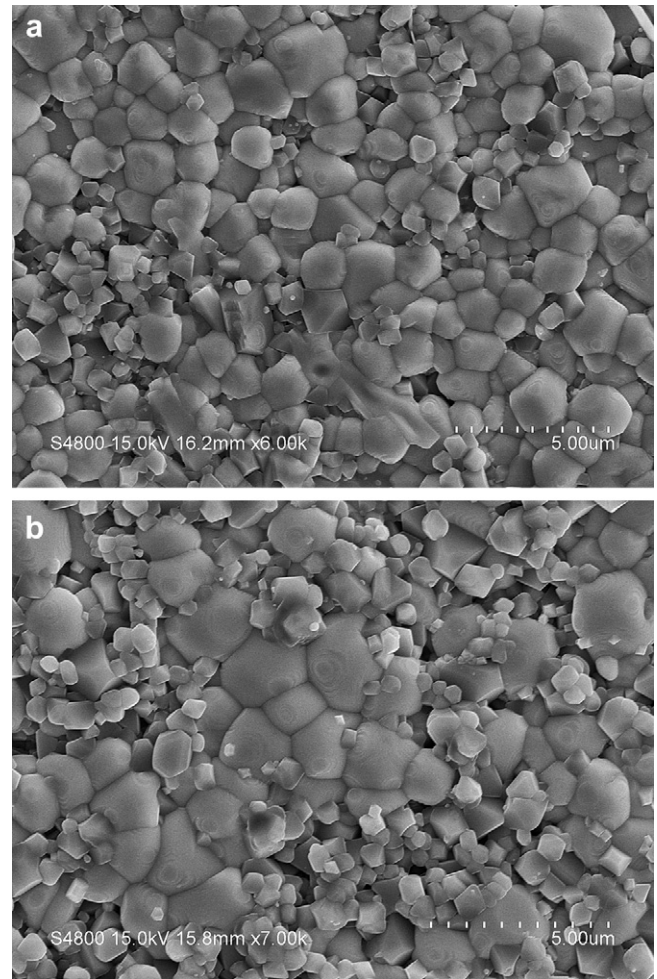


Fig. 2. Secondary electron images of free surfaces of the (a)  $0.1\text{NZCF}/0.9\text{PNZNWT}$  and (b)  $0.3\text{NZCF}/0.7\text{PNZNWT}$  ceramic composites sintered at  $950^\circ\text{C}$  for 2 h after thermal etching at  $825^\circ\text{C}$  for 30 min.

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