



Influence of the light incidence angle on the precision of generalized magneto-optical ellipsometry



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ABSTRACT

We study theoretically and experimentally the influence of the light incidence angle φ_0 on the precision of generalized magneto-optical ellipsometry (GME). A brief review of the GME methodology is presented together with a study of the error propagation from measurement uncertainties to the precision of the resulting complex index of refraction N and magneto-optical constant Q . The results are compared with longitudinal GME measurements on bulk polycrystalline cobalt. We observe a strong increase of the resulting relative error as φ_0 decreases below 45° . We tested our theoretical estimates by performing GME measurements for polycrystalline cobalt ($N = 2.20 + 3.42i$; $Q = (2.25 - 0.80i) \times 10^{-2}$) and found GME measurements to clearly exhibit improved reliability for $\varphi_0 > 30^\circ$.

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1. Introduction

Generalized magneto-optical ellipsometry (GME) [1] is a powerful, nondestructive technique that combines in a single experimental setup and sequence magneto-optical Kerr effect (MOKE) magnetometry and ellipsometry. It is therefore capable of determining by means of a single measurement sequence the complex index of refraction $N = n + ik$, the magneto-optical coupling constant $Q = Q_r + iQ_i$, as well as the magnetization orientation of a ferromagnetic material [2,3].

It was also demonstrated that GME can be extended to variable wavelength and temperature dependent measurement types [4,5]. Some recent works have furthermore improved the efficiency of data acquisition [6] and used GME to characterize purely optical anisotropy effects [7].

It is known that the sensitivity of a conventional, non-magneto-optical ellipsometer is in general better for higher incidence angles [8] (as measured from the sample normal), with recommended angles being typically larger than 40° . Until now, no significant attention has been given to the incidence angle of the light in GME experiments, which could affect the precision and accuracy of results in a significant way.

In this work we present a thorough study of error propagation for N and Q at different incidence angles of the light φ_0 and we compare these theoretical results with GME measurements on polycrystalline cobalt films for different values of φ_0 .

2. Theory

For simplicity, we restrict our analysis here to the assumption of a bulk material that is optically isotropic and has isotropic magneto-optical response in that it can be described by a single magneto-optical coupling constant Q . The light used in the GME experiment is assumed to be a fully polarized plane wave. The electric field of such a light wave can be expressed as the superposition of components that are perpendicular and parallel to the plane of incidence, as shown in Fig. 1:

$$\mathbf{E} = \begin{pmatrix} \mathbf{E}_s \\ \mathbf{E}_p \end{pmatrix}. \quad (1)$$

The surface acts as a transformation matrix

$$\mathbf{R} = \begin{pmatrix} r_{ss} & r_{sp} \\ r_{ps} & r_{pp} \end{pmatrix} \quad (2)$$

for the incoming beam. The diagonal components of \mathbf{R} , r_{ss} and r_{pp} are the conventional, nonmagnetic reflection coefficients of the

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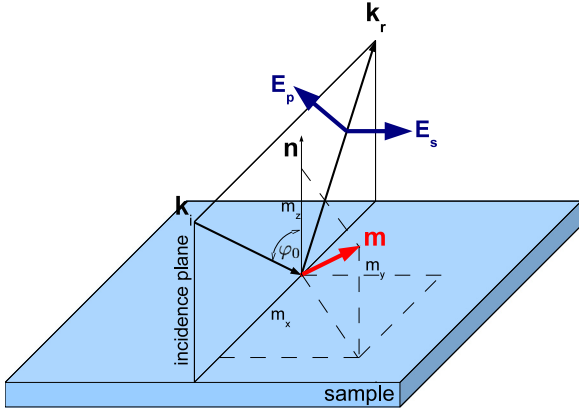


Fig. 1. Reflection of light at the surface of a magnetized medium with arbitrary direction of the magnetization. \mathbf{m} represents the unit vector of the magnetization. \mathbf{n} is the vector normal to plane and lies in POL. m_x , m_y , m_z are the longitudinal, longitudinal and polar components of \mathbf{m} respectively.

perpendicular and parallel components, respectively, i.e. the Fresnel reflection coefficients, which are known to follow [9]

$$\tilde{r}_s = \frac{r_{ss}}{r_{pp}} = -\frac{\cos(\varphi_0 - \varphi_1)}{\cos(\varphi_0 + \varphi_1)}, \quad (3)$$

with

$$\tan(\varphi_1) = \cot(\varphi_0) \left(\frac{\tilde{r}_s + 1}{\tilde{r}_s - 1} \right), \quad (4)$$

where φ_1 is the complex angle of refraction. The non-diagonal components of matrix \mathbf{R} are terms that appear if the sample material is magnetized. In the case studied here, we restrict ourselves to magnetization orientations along the longitudinal axis only, so that

$$\mathbf{R} = r_{pp} \begin{pmatrix} \tilde{r}_s & \tilde{\alpha} \\ -\tilde{\alpha} & 1 \end{pmatrix} \quad (5)$$

with [3]

$$\tilde{\alpha} = -\frac{ibQ \sin(2\varphi_0) \sin^2(\varphi_1)}{\sin(\varphi_0 + \varphi_1) \cos(\varphi_1) [\sin(2\varphi_0) - \sin(2\varphi_1)]} \quad (6)$$

for a bulk like sample, where Q is defined via the dielectric tensor

$$\boldsymbol{\epsilon} = \epsilon_r \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} + iQ\boldsymbol{\epsilon}_r \begin{pmatrix} 0 & m_z & -m_y \\ -m_z & 0 & m_x \\ m_y & -m_x & 0 \end{pmatrix}, \quad (7)$$

with ϵ_r being the permittivity of the medium in the absence of magnetization.

For a GME set-up like the one shown [6] in Fig. 2, the polarizers are described by the transformation matrix

$$\mathbf{P} = \begin{pmatrix} \cos^2(\theta) & \sin(\theta)\cos(\theta) \\ \sin(\theta)\cos(\theta) & \sin^2(\theta) \end{pmatrix} \quad (8)$$

acting upon the incoming electric field vector. Hereby, θ is the angle between the polarizer transmission axis and the s-polarization orientation. The electric field vector \mathbf{E}_D arriving at the photodetector is then given by

$$\mathbf{E}_D = \mathbf{P}(\theta_2) \cdot \mathbf{R} \cdot \mathbf{P}(\theta_1) \cdot \mathbf{E}_0, \quad (9)$$

with \mathbf{E}_0 being the electric light field produced by the laser. Correspondingly, the intensity of the light at the photodetector is

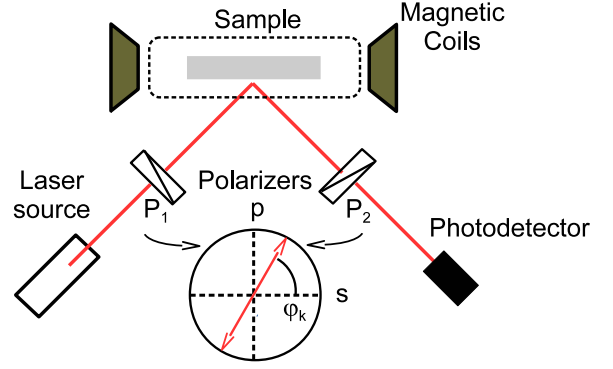


Fig. 2. Scheme of the GME setup.

$$I_D = \mathbf{E}_D \cdot \mathbf{E}_D^*. \quad (10)$$

The analysis of light intensity changes at the detector upon magnetization state inversion, while varying the angles of the polarizers θ_1 and θ_2 , enables now the determination of \mathbf{R} , which in turn allows for the extraction of N and Q , in both their real and imaginary parts. We define here the fractional intensity change:

$$\frac{\delta I}{I}(\theta_1, \theta_2) = 2 \frac{I_1 - I_i}{I_1 + I_i}, \quad (11)$$

where I_1 and I_i are the light intensities for inverted magnetization states of the sample. It has been shown [1] that

$$\frac{\delta I}{I} = \frac{B_1 f_1 + B_2 f_2}{B_5 f_5 + 2B_6 f_4 + f_3} \quad (12)$$

with

$$\begin{aligned} B_1 &= \Re(\tilde{\alpha}), \\ B_2 &= \Re(\tilde{r}_s \alpha^*), \\ B_5 &= |\tilde{r}_s|^2, \\ B_6 &= \Re(\tilde{r}_s) \end{aligned} \quad (13)$$

and¹

$$\begin{aligned} f_1 &= \sin \theta_2 \cos \theta_2 \sin^2 \theta_1 - \sin \theta_1 \cos \theta_1 \sin^2 \theta_2, \\ f_2 &= \sin \theta_1 \cos \theta_1 \cos^2 \theta_2 - \sin \theta_2 \cos \theta_2 \sin^2 \theta_1, \\ f_3 &= \sin^2 \theta_1 \sin^2 \theta_2, \\ f_4 &= \sin \theta_1 \cos \theta_1 \sin \theta_2 \cos \theta_2, \\ f_5 &= \cos^2 \theta_1 \cos^2 \theta_2. \end{aligned} \quad (14)$$

From Eq. (13) we obtain

$$\tilde{r}_s = B_6 + i\sqrt{B_5 - B_6^2} \quad (15)$$

The relation between r_s and the index of refraction is given by [9]

$$\tilde{r}_s = \frac{\sin^2(\varphi_0) + \cos(\varphi_0) \sqrt{N^2 - \sin^2(\varphi_0)}}{\sin^2(\varphi_0) - \cos(\varphi_0) \sqrt{N^2 - \sin^2(\varphi_0)}}. \quad (16)$$

Thus we obtain

¹ If the orientation of magnetization is arbitrary, the numerator in right part of Eq. (12) will have four additional terms describing the transversal and polar components of magnetization [5].

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