



# Heat treatment effects on microstructure and magnetic properties of Mn–Zn ferrite powders

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## ABSTRACT

Mn–Zn ferrite powders ( $\text{Mn}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ ) were prepared by the nitrate–citrate auto-combustion method and subsequently annealed in air or argon. The effects of heat treatment temperature on crystalline phases formation, microstructure and magnetic properties of Mn–Zn ferrite were investigated by X-ray diffraction, thermogravimetric and differential thermal analysis, scanning electron microscopy and vibrating sample magnetometer. Ferrites decomposed to  $\text{Fe}_2\text{O}_3$  and  $\text{Mn}_2\text{O}_3$  after annealing above 550 °C in air, and had poor magnetic properties. However,  $\text{Fe}_2\text{O}_3$  and  $\text{Mn}_2\text{O}_3$  were dissolved after ferrites annealing above 1100 °C. Moreover, the 1200 °C annealed sample showed pure ferrite phase, larger saturation magnetization ( $M_s=48.15 \text{ emu g}^{-1}$ ) and lower coercivity ( $H_c=51 \text{ Oe}$ ) compared with the auto-combusted ferrite powder ( $M_s=44.32 \text{ emu g}^{-1}$ ,  $H_c=70 \text{ Oe}$ ). The 600 °C air annealed sample had the largest saturation magnetization ( $M_s=56.37 \text{ emu g}^{-1}$ ) and the lowest coercivity ( $H_c=32 \text{ Oe}$ ) due to the presence of pure ferrite spinel phase, its microstructure and crystalline size.

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## 1. Introduction

Mn–Zn ferrites are very important soft magnetic materials because of their high initial magnetic permeability, saturation magnetization, electrical resistivity and low power losses [1,2]. These materials are extensively used as inductors, transformers, antenna rods, loading coils, deflection yokes, choke coils, recording heads, magnetic amplifiers, electromagnetic interference devices (EMI), power transformers and splitters [3,4]. Moreover, Mn–Zn ferrites are very important in biomedicine as magnetic carriers for bioseparation, enzymes and proteins immobilization [5–8].

Recently, with the development of high frequency, low power miniaturized electronic devices, special focus has been placed on preparation of high performance Mn–Zn ferrite powders. To prepare high electromagnetic performance Mn–Zn ferrites, various synthesizing methods have been reported recently, including co-precipitation, alcohol dehydration, hydrothermal synthesis, spray drying, and sol–gel methods [9–13]. However, these methods are economically unfeasible for large-scale

production. Recently more attention has been paid to the citrate–nitrate precursor auto-combustion method, which allows producing ultra-fine powders with chemically homogeneous composition, uniform size and good reactivity [14,15]. The advantages of this method are processing simplicity, low energy loss, high production efficiency and high-purity products.

In the present work, Mn–Zn ferrite powders were prepared by the citrate–nitrate precursor auto-combustion method. Then the as-prepared powders were annealed at different temperatures ranging from 400 to 1200 °C for 1 h in air and argon. Structural and magnetic properties of annealed Mn–Zn ferrites were investigated.

## 2. Experiment

Mn–Zn ferrite powders ( $\text{Mn}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ ) were prepared by the citrate–nitrate precursor auto-combustion method using ferric nitrate ( $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ ), zinc nitrate ( $\text{Zn}_2(\text{NO}_3)_6 \cdot 6\text{H}_2\text{O}$ ), manganese nitrate ( $\text{Mn}_2(\text{NO}_3)_6$ ), citric acid ( $\text{C}_6\text{H}_8\text{O}_7 \cdot \text{H}_2\text{O}$ ) and ammonia as raw materials. Equimolar metal nitrates and citric acid were dissolved in appropriate amounts of distilled water, and the solution pH value was adjusted to 5.5 with ammonia. The solution was heated to 60 °C and continuously stirred using

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magnetic agitation. After 4 h the solution became a homogeneous viscous sol–gel. Then the sol–gel was oven dried at 120 °C for 24 h to obtain a dried gel. A loose, brown and very fine Mn–Zn ferrite powder was produced after the dried gel had spontaneously combusted in air.

In order to investigate the influence of annealing temperature on structural and magnetic properties, as-prepared auto-combusted  $\text{Mn}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  powders were annealed at 400, 550, 600, 700, 800, 900, 1000, 1100, and 1200 °C respectively for 1 h in air.

X-ray diffraction (XRD) was used to determine the phases and crystalline size. XRD patterns were recorded on a Philips APD-10 diffractometer using  $\text{Cu-K}\alpha$  source. Thermogravimetric and differential thermal analysis (TG-DTA) (METTLER TOLEDO STAR<sup>e</sup> system, Switzerland) of the auto-combusted ferrites was carried out with a heating rate of 10 °C/min in air. The morphology and size of particles were observed by scanning electron microscopy (SEM) (LEO 1450). LDJ 9600 (LDJ Electronics, Troy, MI, USA) vibrating sample magnetometer (VSM) was used to investigate the magnetic properties at room temperature.

### 3. Results and discussion

#### 3.1. Products phase analysis

Fig. 1 shows XRD patterns of the auto-combusted powder and samples annealed at different temperatures ranging from 400 to 1200 °C for 1 h in air. The as-prepared auto-combusted powder has a pure spinel structure (JCPDS 74-2401), which indicates that one can obtain a pure Mn–Zn ferrite phase by the method of citrate–nitrate precursor auto-combustion. At low 400 °C annealing temperature, powders also have pure spinel structure. However, above 550 °C, the annealed powders contain some impurity XRD reflections, which are due to the  $\text{Fe}_2\text{O}_3$  and  $\text{Mn}_2\text{O}_3$  phases (JCPDS 33-0664 and 24-0508).  $\text{Fe}_2\text{O}_3$  and  $\text{Mn}_2\text{O}_3$  begin to dissolve at 1100 °C. Moreover, at 1200 °C, a well-crystallized pure Mn–Zn ferrite phase is formed.

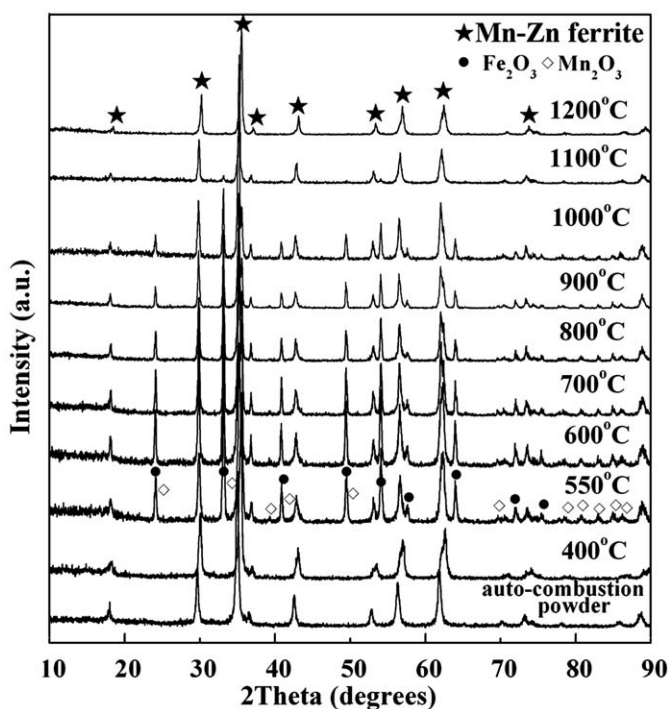


Fig. 1. XRD patterns of  $\text{Mn}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$  powders annealed at different temperatures.

Fig. 2 shows the effect of the annealing temperature on the crystalline sizes of the annealed powders. The average crystalline sizes were determined using the Debye–Scherrer's formula [16]. The crystalline size of auto-combusted powder is about 23.6 nm. The crystallite sizes of annealed powders first increases from 24.8 to 39.8 nm with the annealing temperature increase from 400 to 1100 °C. Then it decreases to 32.9 nm at 1200 °C. The reason for the decrease will be explained later.

#### 3.2. TG-DTA analysis of ferrite powders auto-combustion

In order to investigate the mechanism of the Mn–Zn ferrites auto-combustion, thermal analysis (TG-DTA) was carried out and the results are shown in Fig. 3. In the DTA curve, the 541.4 °C endothermic peak is relatively sharp and intense; however, the TG curve is quite flat. With annealing temperature increase, there is an intense 1043.01 °C exothermic peak in the DTA curve, and the TG curve exhibits continuous weight loss here.

Mn and Fe elements have varying valencies in Mn–Zn ferrites, therefore, oxidation and reduction reactions would probably occur in Mn–Zn ferrites. The reactions would depend on the oxygen partial pressure in the environment and the heat treatment

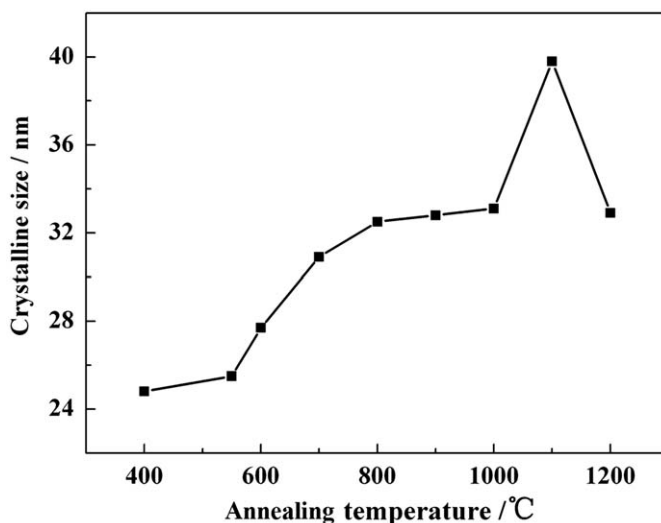


Fig. 2. Mn–Zn ferrite crystalline size dependence on the annealing temperature.

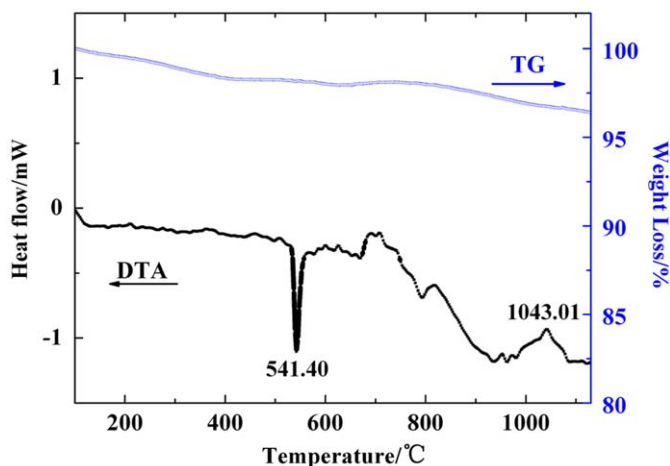


Fig. 3. TG-DTA curves of Mn–Zn ferrite powders.

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