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Trajectory-property relationships in MOD-derived YBCO films

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Abstract

A study of the physical and chemical changes during processing in MOD-derived YBCO films was performed. Fully processed films were 70–85% of theoretical density. The sintering rate increased substantially in the compositional range $F/Ba = 1.8-1.5$. The activation energy for sintering decreased above a P(H₂O) dependent threshold temperature. XRD indicated this temperature/composition threshold also corresponded to YBCO nucleation, suggesting *ex situ* YBCO forms in contact with a melt. The ramp rate and $P(H_2O)$ were used to control F/Ba trajectories, which were correlated to performance. The nucleation of YBCO was strongly dependent on processing conditions. Nucleation temperature was varied by at least 60 °C in the study. The optimal YBCO nucleation temperature in the 300–800 nm films was around 725 °C. *a*-axis grains dominated the microstructures of films where YBCO nucleated at <700 °C. Large second phases, but no *a*-axis grains, were found when the nucleation temperature was >750 °C. 2006 Elsevier B.V. All rights reserved.

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1. Introduction

Metal-organic deposition (MOD) is a proven method for the preparation of $YBa_2Cu_3O_{7-x}$ (YBCO) thin-films and is used in pilot scale production of coated conductors [\[1\]](#page--1-0). The mechanism by which precursor film is converted to YBCO has, however, never been fully described due to the complexity of the process. The following overall reaction has been suggested:

$$
2BaF_2 + 2CuO + 0.5Y_2Cu_2O_5 + 2H_2O_{(g)}
$$

= YBCO + 4HF_(g) (1)

Reaction (1) does not describe a specific reaction in the system, but rather the overall conversion of precursors to the YBCO product. This reaction occurs in steps during heat treatment [\[2,3\].](#page--1-0) Recent investigations have suggested that reaction (1) poorly represents the actual conversion process. The overall fluorine-to-barium (F/Ba) ratio of films provides insight into the compositional changes that occur during processing. F/Ba ratio measurements by Yoshizumi, et al. showed that precursor films following decomposition have about three times as much fluorine in the film as barium (F/Ba \sim 3), indicating some fluorine is bound in the film as YF_3 [\[2\].](#page--1-0)

MOD precursor films undergo significant chemical changes before YBCO nucleates. Analysis of F/Ba ratio and P(HF) over the film during processing has revealed the decomposition of fluorides occurs in steps. YF_3 is thermodynamically less stable than $BaF₂$ and decomposes completely before BaF_2 decomposition begins. YF_3 decomposition results in removal of Y from a $BaF₂$ solid solution [\[2\]](#page--1-0). The decomposition product is unknown, but $Y_2Cu_2O_5$ phase is detected in XRD just before nucleation of YBCO [\[2\]](#page--1-0). Y_2O_3 , $Y(OH)_3$ [\[4\],](#page--1-0) and yttrium oxyfluoride [\[5\]](#page--1-0) have also been proposed as reaction products. $BaF₂$ begins to decompose without the formation of YBCO [\[2\]](#page--1-0). A number of reactions could possibly represent $BaF₂$ decomposition in the region of $2.0 > F/Ba > \sim 1.5$. The most likely, as estimated

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from $P(HF)$ measurements, is the formation of BaCuO₂ [\[2\].](#page--1-0) A Ba(O_xF_y) superstructure has been detected in e-beam derived films, and may form in MOD films as well [\[6,7\].](#page--1-0)

A transient liquid phase is speculated to exist during processing of *ex situ* films. Crystallites of $BaF₂$ phase material of up to 20 nm have been observed in TEM images of films quenched near the nucleation of YBCO, and these crystallites actually grow during heating as more Y is removed from solution [\[8\]](#page--1-0). Growth rates of YBCO, however, exceed 5 nm/s [\[9\].](#page--1-0) The large chemical inhomogeneity in precursor films indicates a phase with high cation mobility, such as a melt, is necessary to obtain the required growth rates. The chemical makeup or even the presence of a melt has never been established. McIntryre proposed the presence of a cuprate melt, some of which are known to exist at low-temperatures and have a $P(O_2)$ dependence [\[8\].](#page--1-0) Yoshizumi, et al. noted the additional fluorine in MOD-films could promote transient fluorine-rich melts during processing [\[2\].](#page--1-0) Solovyov, et al., while working with e-beam derived $BaF₂$ containing films, found a fluorine-free amorphous layer at the YBCO growth interface [\[10\].](#page--1-0) It was suggested that this was a quenched fluorine-free melt [\[4\]](#page--1-0).

The study of physical changes in ex situ films has been mostly limited to microstructure studies. Thickness changes of MOD-derived films were monitored in this study during high-temperature processing. Cross-sectional SEM studies have previously shown shrinkages in excess of 50% from decomposed to final film thicknesses [\[9,11\].](#page--1-0) Other researchers have suggested this is due to the presence of porosity in the decomposed film [\[8\].](#page--1-0) TEM and XRD studies of the films have shown that the decomposed films are nanocrystalline in nature, consisting of small crystals of $BaF₂$ and Y₂Cu₂O₅ in a mostly amorphous and porous matrix [\[9,8\].](#page--1-0) The small particle size in the precursor film and the initial porosity means there is a large driving force for shrinkage by sintering. Shrinkage also occurs because film fluorine is replaced with half as much oxygen during conversion. The solid products of Reaction [\(1\)](#page-0-0) have a 20% smaller volume than the solid reactants. Small thickness changes occur due to substrate reactions [\[12\].](#page--1-0) Sintering and conversion should account for most film thickness change.

Physical and chemical changes in MOD-derived films during ramping and annealing are reported in this paper. The physical changes observed included the change in film thickness and surface morphology of the films. The overall F/Ba compositional trajectory of the films and XRD phase relations were used to deduce chemical changes. Comparisons between physical and chemical changes were used to infer the presence of a fluorine-free melt that is associated with the nucleation and growth of YBCO. The relationships between trajectories and performance were explored.

2. Experimental

Samples were prepared according to well-described procedures for the production of MOD YBCO [\[11\].](#page--1-0) Solutions of two different concentrations were used to provide films of two thicknesses following decomposition $(\sim 1.1 \,\mu m$ and \sim 0.7 um). The higher concentration solution was prepared by allowing solvent to evaporate from the more dilute solution. Several substrates were used, including bare (100) aligned $Zr_{0.87}Y_{0.13}O_2$ (YSZ), YSZ coated with solutiondeposited epitaxial $CeO₂$, and bare (110) aligned LaAlO₃ (LAO). Details of the solution deposition process for epitaxial $CeO₂$ can be found elsewhere [\[13\].](#page--1-0) Samples were cleaned before spin-coating and coating was performed for 120 s at 2000 rpm (for thick films) or 4000 rpm (for thin films) in a particle containment hood. A low-temperature heat treatment described elsewhere [\[11\]](#page--1-0) was used to decompose samples following this spin-coating.

The edges of the samples were removed after decomposition using a razor blade. Film areas following edge removal were on average $5.32 \times 10^7 \,\text{\ensuremath{\mu}m}^2 \pm 6\%$, or approximately 7.5 mm \times 7.5 mm. Bridges were also scribed with a razor blade into samples designated for current testing. Debris from film removal was removed using a jet of dry nitrogen.

Film thickness measurements were performed using a Tencor P10 profilometer. Six measurements were performed on each sample, two in the center of the edges and four closer to each corner. Profilometer measurements were taken at a rate of 100 Hz and speed of 20 μ m/s, giving an approximate spacing of 200 nm between measurements. Typical scan lengths were \sim 700 μ m with 100–300 μ m on the film itself. The starting corner for the thickness measurement was marked with a scratch in the film so approximately the same positions could be measured after the high-temperature heat treatment. The profilometer accuracy was checked by testing a VLSI thickness standard of 4500 Å over the whole range of dates relevant to this study. The standard deviation of these measurements was 1.31% of the standard thickness. The error determined from 10 replicates of one experimental condition was 1.88%.

Conversion heat treatments were performed in a specially designed tube furnace with silica rails that allowed a silica setter plate with sample to be pushed into and out of a hot furnace. Sample temperatures were recorded by a thermocouple placed in a sleeve on the setter plate. The study of near-equilibrium film shrinkage behavior used a 5 °C/min ramp with a 1 h annealing at temperature followed by furnace cooling (approx. $5^{\circ}C/\text{min}$ above 500 $^{\circ}$ C). Heat treatments for other tests were modifications of heat treatment procedures that produced high J_c films [\[11\].](#page--1-0) [Fig. 1](#page--1-0) illustrates the conversion heat treatment profiles. The initial ramp rate (to 500 °C) was 25 °C/min. The ramp rate between 500 and 760 \degree C was varied in the experiment from $5^{\circ}C/\text{min}$ to $25^{\circ}C/\text{min}$. Samples were annealed at $760 °C$ for 2.25 h. All heat treatments were performed under 1 atm total, 100 ppm O_2/b alance N₂, process gas flowing at 3 SLM through a 53 mm diameter quartz furnace tube. Three gas switches were made. The first switch occurred after 10 min at 760 \degree C and changed the moisture content of the process gas from the experimental

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