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# Application of ozone decomposition catalysts to electron-beam irradiated xylene/air mixtures for enhancing carbon dioxide production

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#### Abstract

The electron beam (EB) oxidation of gaseous xylene in air, appearing as ventilation gases emitted from painting factories, was investigated under various experimental conditions. Thereby, the implementation of an ozone decomposition catalyst,  $MnO_2$ , into EB-induced oxidation of xylene/air mixtures strongly contributed in the achievement of a better purification degree. (C) 2007 Elsevier Ltd. All rights reserved.

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#### 1. Introduction

Various volatile organic compounds (VOCs) have been widely used in the industry, e.g. as solvents, basic material for chemical synthesis, etc. Because of their light volatility, they appear frequently as air pollutants and cause environmental problems when released into the atmosphere (Wiederkehr, 1984).

Electron beam (EB) technology is one of the advanced technologies for treating environmental pollutants in gases and water. This technology is based on oxidation reactions of pollutants with oxidizing species produced from such media by the irradiation. When irradiated to air, various oxidizing species such as OH radicals, O atoms, and O<sub>3</sub> are produced from air components (N<sub>2</sub>, O<sub>2</sub>, and H<sub>2</sub>O) through their ionization and dissociation (Mätzing, 1991). Among these species, OH radicals can oxidize gaseous pollutants such as VOCs and NO<sub>x</sub>/SO<sub>2</sub> in air. However, most of the O atoms rapidly react with 21 vol% O<sub>2</sub> in air and produce O<sub>3</sub> with the assistance of a third body, M (=N<sub>2</sub>/O<sub>2</sub>). The resulting O<sub>3</sub> can hardly oxidize gaseous VOCs in the gas

phase within a few seconds because of its lower reactivity than that of OH radicals (Atkinson et al., 1982). If the  $O_3$ remaining in the irradiated VOCs/air mixtures can be utilized for the oxidation of VOCs or their irradiation byproducts, the absorbed dose of irradiation required for purification of the VOC/air mixture will be reduced.

In the water phase,  $O_3$  has been known as strong and active oxidizing species for oxidation of organic contaminants. The synergetic effect has been reported for implementation of  $O_3$  to radiation-induced degradation of pollutants in water because of the attack of active species from radiolysis of water and that of injected  $O_3$  and its originated radical anions (Getoff, 2002; Popov and Getoff, 2006). The degradation pathway of organic pollutants has been clarified (Getoff, 1996).

On the other hand, in the gas phase, a promising method for the activation of inactive  $O_3$  seems to be the application of  $O_3$  decomposition catalysts to irradiated VOCs/air mixtures. The oxidation of VOCs at concentrations of a few thousand ppmv by exposing both VOCs/air mixtures and injected  $O_3$  to  $O_3$  decomposition catalysts at temperatures in the range of 298–723 K has been studied (Li and Oyama, 1996, 1997; Naydenov and Mehandjiev, 1993; Ragaini et al., 1993; Gervasini et al., 1994). The oxidation

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of VOCs is initiated through the reaction of the active oxygen, such as O atoms,  $O^-$ ,  $O_2^-$ , and  $O_3$  transients, produced by the O<sub>3</sub> decomposition on the surface of the catalysts. Catalysts for both O<sub>3</sub> decomposition and VOC oxidation include MnO<sub>2</sub>, MgO, MoO, and Co<sub>3</sub>O<sub>4</sub>. Manganese dioxide is the most active O<sub>3</sub> decomposition catalyst among the transition metal oxides (Dhandapani and Oyama, 1997).

The aim of the present paper concerns the EB-induced oxidation of xylene occurring as an air pollutant at painting factories in Japan. The experiments embrace the application of  $MnO_2$  to an irradiated xylene/air mixture containing remaining  $O_3$  in the frame of EB treatment of polluted air.

#### 2. Experimental

The experimental setup for the preparation of sample gases, the EB irradiation of them, the catalytic process, and the analysis of the irradiated them with and without the catalytic process is described in the following sections.

#### 2.1. MnO<sub>2</sub>

Manganese dioxide (obtained from Mitsui Mining and Smelting Co., Ltd.) containing Mn and Cu contents by  $52\pm 5$  and 3 wt%, respectively, was used as an O<sub>3</sub> decomposition catalyst. MnO<sub>2</sub> is in the form of pellets (diameter, 4 mm; length, 4-10 mm). The average surface area of the MnO<sub>2</sub> pellet was measured to be  $205.6 \text{ m}^2/\text{g}$  by an automatic surface area analyzer (Mountech Co., Ltd., Macsorb HM Model-1201) using a dynamic Brunauer– Emmet–Teller (BET) method (Brunauer et al., 1938).

#### 2.2. EB irradiation of xylene/air mixture

Air containing 100 ppmv *o*-xylene  $(C_6H_4(CH_3)_2)$  and  $1.0 \times 10^4$  ppmv water vapor, hereafter referred to as the xylene/air mixture, was prepared as a sample gas. The concentration of xylene in the gas mixture was evaluated by a gas chromatograph (Shimadzu Co. Ltd., GC-8A) (GC) equipped with a flame ionization detector (FID). Air

containing  $1.0 \times 10^4$  ppmv water vapor, hereafter referred to as air, was also prepared for use as an experimental reference.

A compact EB generator with a maximum accelerating voltage of 55 kV and maximum current of 0.5 mA (Hakoda et al., 2006) was used as a radiation source for irradiating the air and xylene/air mixture as shown in Fig. 1. The xylene/air mixture and air were introduced into the irradiation cup at a flow rate of 5.0 L/min and irradiated with an EB of 53 keV. The temperatures of air and xylene/air mixture were maintained at 298 K during irradiation by the circulation of cooling water outside the cup. The average absorbed dose in the gas sample was estimated from the concentration of O<sub>3</sub>, which is produced by the irradiation of pure O<sub>2</sub> gas at a flow rate of 5.0 L/min at 298 K, using the *G* value of 0.62 µmol/J for the generation of O<sub>3</sub> (Namba et al., 1989).

Xylene in air was oxidized into gaseous and particulate byproducts besides  $CO_2$  and CO under EB irradiation (Hakoda et al., 2006). An irradiated xylene/air mixture containing no particulate byproducts was also prepared by removing 98 wt% (carbon concentration) of particulate byproducts from the gas phase by performing filtration using quartz fibers. This was done to examine the chemical form (gaseous and particulate forms) of the byproducts, which are oxidized into  $CO_x$  through the catalytic process.

### 2.3. Catalytic processing of irradiated air and xylene/air mixture

The MnO<sub>2</sub> pellets with a total weight of 3.1 and 15.5 g in a quartz cylinder (i.d., 23 mm; length, 140 mm) were placed in an oven and maintained at a constant temperature. The MnO<sub>2</sub> pellets weighing 3.1 and 15.5 g can decompose 50% and 100%, respectively, of 150 ppmv O<sub>3</sub> in air at room temperature; this O<sub>3</sub> is generated by an UV-type O<sub>3</sub> generator. This MnO<sub>2</sub> pellet layer was placed downstream of the irradiation cup as shown in Fig. 1. The time taken for the irradiated air and xylene/air mixture (5.0 L/min) to travel from the irradiation cup to the upper surface of the MnO<sub>2</sub> layer was 0.20 s. The irradiated air and xylene/air mixture were preheated to different temperatures, 303, 353,



Fig. 1. Apparatus for electron beam irradiation of air and xylene/air mixture, their catalytic process using MnO<sub>2</sub>, and analysis of these gases before and after the catalytic process.

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