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Flow rate distribution of cracked hydrocarbon fuel in parallel pipes

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HIGHLIGHTS

- Mal-distribution of coolant causes a waste of heat sink and even over-temperature.
- Distribution of cracked hydrocarbon fuel in parallel pipes are studied.
- Two flow rate deviation amplification mechanisms are found.
- The mal-distribution mode varies with thermal deviation.
- Higher pressure suppresses the mal-distribution.

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ABSTRACT

A model consisting of two parallel pipes with common inlet and outlet manifolds was established and used to run simulation and experimental study on the flow rate distribution of cracked hydrocarbon fuel in parallel pipes under supercritical pressure. Both simulation and experimental results indicated that mass flow rate and fuel temperature distribution of cracked hydrocarbon fuel in parallel pipes was closely related to the difference in fuel density in pipes. Two deviation amplification mechanisms were found. In addition, the mode of mal-distribution varies with thermal deviation and the distribution was effectively improved by the increase of pressure. And the total mass flow rate could hardly have any effects on the flow rate distribution. All these results could be used to help the full utilization of fuel heat sink and avoid over-temperature.

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1. Introduction

Scramjet is a promising propulsion system for hypersonic missile and reusable air-space integrated fight vehicle [1,2]. Due to high flight Mach number, the combustion temperature and heat transfer rate of a scramjet are very high. Thus, cooling becomes a major concern. Regenerative cooling is generally accepted as the most promising method [3]. Considering limited quantity of fuel on board, endothermic hydrocarbon fuel with extra chemical heat sink is used to further increase the cooling capacity [4–6]. Fuel flows through the parallel cooling channels as coolant to cool the wall before it's injected into the combustor [7,8] while a supercritical pressure is kept in the channels to avoid boiling crisis.

However, heat flux is not uniform or constant in the wall of a scramjet, which may lead to the mal-distribution of mass flow rate

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and fuel temperature in different channels. As a result, fuel heat sink is not fully utilized in the low temperature channels. Overtemperature may occur in the high temperature channels to cause thermal protection failure and damage to engine structure. Therefore, it's of great significance to study the flow rate distribution of cracked hydrocarbon fuel in parallel channels under supercritical pressure so that the fuel heat sink could be fully utilized to avoid over-temperature.

Much work has been done in recent years on boiler, solar power generator [9,10] and fuel cell [11,12] continuously, since the distribution characteristics are important to the safety and efficiency of above mentioned applications. Structure of inlet and outlet manifold has been another focus for the study on the flow rate distribution characteristics [13,14] of fluids including water, carbon dioxide and other refrigerants. Due to pyrolysis, the flow and heat transfer of hydrocarbon fuel is quite different from other fluids [15,16]. A lot of work has been done on the pyrolysis of hydrocarbon fuel through single heated channel experiments [17–20] to improve its chemical heat sink [21,22] and to avoid thermal oxidation coking [23,24].







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Nomenclature

m_t m_A m_B ho u h C	total mass flow rate (kg/s) mass flow rate of pipe A (kg/s) mass flow rate of pipe B (kg/s) density of fuel (kg/m ³) velocity of fuel (m/s) enthalpy (J/kg)	A_h A_{inner} K_c K_h ΔQ Δm ΔT	flow area of throttle in hot end (m ²) flow area of pipe (m ²) throttle coefficient for cold end throttle coefficient for hot end thermal deviation deviation in mass flow rate deviation in fuel temperature
C_P μ f q_f ΔP Re δ	constant-pressure specific heat (J/(kg K)) dynamic viscosity (Pa s) friction coefficient heat flux (W/m ²) pressure drop (Pa) Reynolds number surface roughness	ΔT _f Δρ Y R Subscrip	deviation in fuel temperature deviation in density mass conversion of reactant universal gas constant (J/(mol K))
H_c k A E_a A_c	chemical heat sink (J/kg) chemical reaction rate constant (s^{-1}) pre-exponential constant (s^{-1}) activation energy (J/mol) flow area of throttle in cold end (m^2)	lh f 1 2	local resistance at total end frictional resistance heating power Q_1 heating power Q_2

So far, the research on flow rate distribution of cracked hydrocarbon fuel in parallel channels is hardly found. Only Ran et al. (2012) studied the flow distribution of kerosene in parallel pipes before pyrolysis occurs [25].

A model consisting of two parallel pipes was established and used to run simulation and experimental study on the flow rate distribution of cracked hydrocarbon fuel in parallel pipes under supercritical pressure and the influences of thermal mal-distribution, pressure and total mass flow rate as well.

2. Modeling with parallel pipes

2.1. Geometry model and hypotheses

In the scramjet, there're usually hundreds of parallel cooling channels through which fuel flows to cool the thermal structure at a temperature of 300–1000 K. Two parallel pipes are used in the model as simplified cooling channels of scramjet, since the close-coupled characteristics of mass flow rate and fuel temperature is clearly presented in this configuration. Similar simplifications are common in studies about parallel systems [9,10].

The following are the hypotheses used by the modeling:

- (1) The radial difference in all parameters is ignored.
- (2) The kinetic energy and heat generated by the viscous effect of hydrocarbon fuel is ignored.
- (3) Channels are horizontal and gravitational potential energy of hydrocarbon fuel is constant.
- (4) Axial heat conduction of hydrocarbon fuel is ignored.
- (5) The effect of coke is ignored since the high flow velocity set in this work.

2.2. Mathematical model

A homogeneous one dimensional model was developed to demonstrate the steady state solution of mass flow rate and temperature distribution. The common inlet and outlet ensures the two parallel pipes an equal pressure drop and the total mass flow rate is set to be constant.

Mass conservation equation can be expressed as:

$$\frac{\partial(\rho u)}{\partial x} = 0 \tag{1}$$

Momentum conservation equation can be written as:

$$\frac{\partial(\rho u^2)}{\partial x} = -\frac{1}{2}\frac{f}{d}\cdot(\rho u^2) - \frac{\partial P}{\partial x}$$
(2)

where d is the equivalent diameter of a pipe and f is the friction coefficient.

$$\frac{\partial(\rho uh)}{\partial x} = \frac{4}{d} \cdot q_f - \rho \cdot (1 - Y) \cdot k \cdot H_c \tag{3}$$

where Y is the mass conversion of reactant. H_c is the chemical heat sink of fuel.

Hydrocarbon fuel is a complex mixture with most of its components following the complicated mechanism of pyrolysis including hundreds of species and reactions with possible interactions. In order to highlight the characteristics of mass flow rate distribution instead of the detailed chemical kinetic processes, the model is simplified using n-dodecane, one of the main components of hydrocarbon fuel and used in many related researches [26–28]. In addition, pyrolysis is considered as the first order reaction and global chemical mechanism is adopted. PPD assumption is used to describe the products of pyrolysis [29].

So the conservation equation of cracking products for n-dodecane can be expressed as:

$$\frac{\partial(\rho uY)}{\partial x} = \rho \cdot (1 - Y) \cdot k \tag{4}$$

where *k* is the chemical reaction rate.

Additional equations of physical properties based on NIST database are required to form a complete system. The density and constant-pressure specific heat of the mixture can be calculated from the mole percentage.

$$\begin{cases} \rho = \sum x_i \cdot \rho_i \\ C_p = \sum x_i \cdot C_{p_i} \end{cases}$$
(5)

This model is mainly used to qualitatively analyze the characteristics of the mass flow rate distribution of hydrocarbon fuel by using n-dodecane.

3. Experimental set-up

As shown in Fig. 1, two high temperature alloy pipes with an inner diameter of 2 mm were used to simulate the parallel cooling channels. China No. 3 kerosene (RP-3) was used as the fuel and

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