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## Pulverized coal combustion in air and in $O_2/CO_2$ mixtures with $NO_x$ recycle

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## Abstract

This paper presents experimental results of a 20 kW vertical combustor equipped with a single pf-burner on pulverised coal combustion in air and  $O_2/CO_2$  mixtures with NO<sub>x</sub> recycle. Experimental results on combustion performance and NO<sub>x</sub> emissions of seven international bituminous coals in air and in  $O_2/CO_2$  mixtures confirm the previous findings of the authors that the  $O_2$  concentration in the  $O_2/CO_2$  mixture has to be 30% or higher to produce matching temperature profiles to those of coal-air combustion while coal combustion in 30%  $O_2/70\%$  CO<sub>2</sub> leads to better coal burnout and less NO<sub>x</sub> emissions than coal combustion in air. Experimental results with NO<sub>x</sub> recycle reveal that the reduction of the recycled NO depends on the combustion media, combustion mode (staging or non-staging) and recycling location. Generally, more NO is reduced with coal combustion in 30%  $O_2/70\%$  CO<sub>2</sub> than with coal combustion in air. Up to 88 and 92% reductions of the recycled NO can be achieved with coal combustion in air and in 30%  $O_2/70\%$  CO<sub>2</sub> respectively. More NO is reduced with oxidant staging than without oxidant staging when NO is recycled through the burner. Much more NO is reduced when NO recycled through the burner (from 65 to 92%) than when NO is recycled through the staging tertiary oxidant ports (from 33 to 54%). The concentration of the recycled NO has little influence on the reduction efficiency of the recycled NO with both combustion media—air and 30%  $O_2/70\%$  CO<sub>2</sub>.

Keywords: NOx recycle; Pulverized coal combustion; Coal combustion in O2/CO2

## 1. Introduction

With conventional coal-air combustion,  $NO_x$  recycle is an alternative approach for the control of  $NO_x$  emissions from combustion [1]. It uses regenerable sorbent to adsorb  $NO_x$  in the flue gas from a combustor followed by desorption, producing a highly concentrated  $NO_x$ -laden stream. This stream is then sent back to the same combustor or to a separate combustor, where the  $NO_x$  is reduced in the flame and  $NO_x$  formation is inhibited. Obviously, the reduction efficiency of the recycled  $NO_x$  in the combustor decides the effectiveness of the  $NO_x$  recycle approach to reduce  $NO_x$  emissions. Previous investigations, such as Zhou et al. [1] who carried out their experiments on a 1.76 MW cyclone furnace, on  $NO_x$  recycle with conventional coal-air combustion found that the  $NO_x$  recycle location had a significant effect on the reduction efficiency of the recycled  $NO_x$ . New investigations on the reduction of the recycled  $NO_x$  with pf burners and other combustors will improve our understandings on the fate of the recycled  $NO_x$  in practical power plant boilers.

Coal combustion with oxygen and recycled flue gases is one of the encouraging methods to tackle  $CO_2$  emissions from coal-fired power plants. The recycled flue gases are mixed with pure oxygen, produced by air separation, to form the oxidant. This reduces or completely eliminates nitrogen from the combustion oxidant and hence produces flue gases with a high concentration of  $CO_2$  (up to 95%), which can be directly injected into the oceans and used for enhanced oil recovery [2]. The recycling flue gases will affect not only the coal combustion performance but also the formation of pollutant emissions, such as  $NO_x$ ,  $SO_2$  and CO. In addition, when flue gases are recycled back to the combustor, minor species in the flue gases, such as  $NO_x$  and  $SO_2$ , are also recycled. Therefore, it is environmentally of interest to know the fate of the recycled pollutants under

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conditions of coal-O<sub>2</sub>/flue gas recycling combustion. There have been a limited number of investigations on the reduction of recycled NO<sub>x</sub> in coal combustion with O<sub>2</sub> and recycled CO<sub>2</sub> [3–5].

Okazaki and Ando [3] studied NO<sub>x</sub> reduction mechanism in coal combustion with recycled CO<sub>2</sub>. Their tests were carried out with a flat CH4 flame burner laden with anthracite particles, with the maximum temperature being fixed at 1450 K and the initial  $O_2$  concentration at 21%. They concluded that more than 50% of the recycled NO was reduced to  $N_2$  in the combustion zone of coal volatile matter. More recently, Hu et al. [4,5] reported their investigations on the reduction of recycled-NO<sub>x</sub> in coal combustion with O<sub>2</sub>/recycled flue gas under high initial O<sub>2</sub> concentrations (60-100%). They carried out their experiments on a bench-scale, quasi-one-dimensional, electrically heated combustor (28 mm id) and found that the reduction efficiency of the recycled NO<sub>x</sub> increased with both the equivalence ratio and the recycling ratio of flue gas (the ratio of flue gas in inlet gas). The reduction efficiency for the recycled NO<sub>x</sub> reached as high as 80% at the fuel equivalence ratio of 1.4 [5].

None of the above mentioned investigations on the fate of the recycled  $NO_x$  in coal combustion with  $O_2/CO_2$  was carried out with a combustor equipped with pf burner(s). Investigations with a combustor equipped with pf burner(s) should produce more reliable results that may be applied to a power plant boiler. In addition, the initial O<sub>2</sub> concentration in the inlet gas should include the range (30-42%) that will likely produce matching temperature profiles to those of conventional coal-air combustion [6–9]. Miyamae et al. [6] reported that 42% O2 in CO2 was required to produce equivalent adiabatic flame temperature to coal-air combustion according to their calculations. Croiset et al. [7,8] found coal combustion in 35% O2/65% CO2 could produce equivalent flame temperature to coal-air combustion in their 0.3 MW vertical combustor. Our previous paper [9] reported our experimental results on the comparisons of combustion performance and NO<sub>x</sub> emissions between coal combustion with air and coal combustion with various O<sub>2</sub>/CO<sub>2</sub> mixtures in a 20 kW down-fired combustor (190 mm id  $\times$  3 m). It concluded that an initial O<sub>2</sub> concentration in CO<sub>2</sub> of 30% or higher was required to

Table 1			
Coal analyses	(%	as	received)

produce matching temperature profiles to those of coal-air combustion under the investigated conditions. It was also concluded that coal combustion in 30% O<sub>2</sub>/70% CO<sub>2</sub> produced less  $NO_x$  than coal combustion in air. No  $NO_x$ recycling experiments had been done at that stage. In this paper, experimental results on  $NO_x$  recycling with both coal-air combustion and coal-O2/CO2 combustion will be reported. The results with coal-air combustion will be particularly of interest to the  $NO_x$  recycle approach as one of the NO<sub>x</sub> control methods [1], while the results with coal- $O_2/$ CO<sub>2</sub> combustion will reveal the likely fate of the recycled  $NO_x$  with coal-O<sub>2</sub>/recycled flue gas combustion. New results with combustion of various coals in air and O<sub>2</sub>/ CO<sub>2</sub> mixture will be introduced first to complement our previous paper [9] and followed by results with  $NO_x$ recycle.

## 2. Experimental

Details of the 20 kW vertical coal combustor (190 mm  $id \times 3$  m) and the experimental procedures had been described in the previous paper [9]. Here only the essential and new information is presented.

The non-swirling primary oxidant carrying coal particles mixes with swirling secondary oxidant near the entrance to the burner quarl. Further down the combustor a tertiary oxidant can be added to simulate the air staging/OFA or low-NO<sub>x</sub> burners combustion. In the following sections of this paper, 'staging' will be used to indicate that a portion of the secondary oxidant is added as the tertiary oxidant.

Seven international bituminous coals have been tested with their analyses shown in Table 1. All of these pulverized coals were supplied from a UK commercial power plant. Experimental conditions are almost the same as reported in the previous paper [9] and given in Table 2. On each testing day, the combustor is heated by natural gas combustion for about 2 h before coal combustion starts. Every test always starts with conventional coal-air combustion and after stabilization and measurements of coal-air combustion, which takes about 2 h, the combustion air is changed over to the mixtures of  $O_2/CO_2$  with continuous coal feeding. The stabilization and measurements with coal- $O_2/CO_2$ 

Coal	Proximate analysis				Ultimate analysis			
	Moisture	Volatile	Ash	Fixed carbon <sup>a</sup>	С	Н	Ν	$O + S^a$
UK Bit 1	2.6	29.4	11.4	56.6 <sup>a</sup>	70.6	4.6	1.6	9.2
US Blend	3.4	31.6	11.6	53.4	69.6	4.50	1.4	9.5
Polish Blend	1.6	30.6	11.1	56.7	72.0	4.6	1.3	9.4
South African	3.6	25.6	10.9	59.9	69.4	4.2	1.8	10.1
Colombian	3.5	33.1	6.0	57.4	72.9	5.1	1.6	10.9
Australian	2.0	29.6	11.9	56.5	69.9	4.4	1.6	10.2
UK Bit 2	5.3	28.4	22.3	44.0	64.2	4.6	1.2	2.4

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