

# Resin-in-pulp method for uranium recovery from leached pulp of low grade uranium ore

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## Abstract

An improved process for the separation of uranium from the leached pulp of low grade uranium ore is reported using the resin-in-pulp method. For this study, four small pachucas were designed and calibrated. A series of tests were conducted batch-wise to determine the optimum conditions for uranium adsorption on a strong base anion exchange resin. The particle size of resin was 0.6–1.6 mm and the particle size of pulp was  $-0.1$  mm. Flow rates of resin and pulp were adjusted on 10 ml/h and 1 ml/h, respectively. The redox potential of pulp was 500 mV and the pH of pulp was 1.8. A McCabe Thiele diagram was constructed for the process and the experimental results confirmed the theoretical predictions. It is concluded that four stage counter-current resin-in-pulp operation under optimum conditions is sufficient to recover about 99% of the uranium from the leached ore.

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## 1. Introduction

It is a common practice to leach uranium ores with sulfuric acid and to remove the uranium by passing the leach liquor through columns containing suitable ion exchange resins, which take out a complex uranium anion. When the resin has taken out as much as it can, an eluting liquid is then passed through, removing the uranium values and regenerating the ion exchange resin, which is then used to treat further amounts of leach liquor (Ford, 1984). This process, which has been used on a commercial scale, has certain drawbacks. The

uranium ores are usually quite low grade, and the leach liquor has to be separated from a very large amount of ore solids. As a result there is a large filtration problem which adds markedly to the cost. The resin-packed columns also represent a relatively expensive construction cost which further increases plant fixed charges (Tatarnikov and Abramov, 1993; Anon, 1993). It has been proposed to eliminate the filtration step by exposing the leached ore pulp to resin in the form of moderately coarse beads, and then separating the uranium loaded beads from the ore solids in the pulp. This process is often referred to as the resin-in-pulp process (Laskorin et al., 1977; Arnold, 1981) and has been used in U.S.A, Russia, France, South Africa, China, Canada, and some other countries for separating the uranium from leached pulp (Laskorin et al., 1977; Skorovarov, 1975; Anon, 1993).

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## 2. Characteristics of ore

The major uranium mineral of this ore is uraninite. In most cases some uraninite minerals occur in relics of magnetite, where they have been excellently preserved. Much more seldom, uranium oxide is observed in serpentine and chlorite. A small portion of uranium is connected with urano-thorianite. In the re-deposited ores, uranium is generally concentrated in weeksite and to a lesser degree in boltwoodite and uranophane. The major gangue mineral is serpentine. In strongly weathered samples, serpentine is replaced by magnesia silicates of saponite–sepiolite type. At the sites of weakly altered serpentine, some chlorite and biotite remain.

Uranium and gangue minerals of the ore are given in Table 1 and results of chemical analysis are given in Table 2.

## 3. Description

### 3.1. Leaching process

To prepare leached pulp for resin-in-pulp process the optimum leaching conditions were as follows:

- Particle size:  $-0.1$  mm
- $H_2SO_4$  consumption: 250 kg/t of ore
- $MnO_2$  as oxidation reagent: 5 kg/t of ore
- Temperature: 70 °C

Table 1  
Uranium and gangue minerals of ore

| Mineral type    | Mineral name    | Chemical formula                                |
|-----------------|-----------------|---|
| Uranium mineral | Uraninite       | $(U_{1-x}^{4+}, U_x^{6+})O_{2+x}$               |
|                 | Weeksite        | $K_2(UO_2)_2(Si_2O_5)_3 \cdot 4H_2O$            |
|                 | Boltwoodite     | $K_2(UO_2)_2(SiO_3)_2(OH)_2 \cdot 5H_2O$        |
|                 | Uranophane      | $Ca(UO_2)_2(Si_2O_7) \cdot 6H_2O$               |
|                 | Uranothorianite | $Th_2UO_4$                                      |
| Gangue mineral  | Magnetite       | $(Fe, Mg)Fe_2O_4$                               |
|                 | Serpentine      | $(Mg, Fe)_3Si_2O_5(OH)_4$                       |
|                 | Talc            | $Mg_3Si_4O_{10}(OH)_2$                          |
|                 | Chlorite        | $(Mg, Fe^{2+}, Fe^{3+})_6AlSi_3O_{10}(OH)_8$    |
|                 | Hematite        | $Fe_2O_3$                                       |
|                 | Biotite         | $K(Mg, Fe^{2+})_3(Al, Fe^{3+})Si_3O_{10}(OH)_2$ |
|                 | Apatite         | $Ca_5(PO_4)_3(Fe, OH, Cl)$                      |
|                 | Opal            | $SiO_2 \cdot xH_2O$                             |
|                 | Gypsum          | $CaSO_4 \cdot xH_2O$                            |
|                 | Plagioclase     | $(Na, Ca)Al(Si, Al)Si_2O_8$                     |
|                 | Epidote         | $Ca_2(Al, Fe^{3+})_3(SiO_4)_3(OH)$              |
|                 | Feldspar        | $(K, Na, Ca, Rb, Ba, Sr, Fe)Al(Al, Si)_3O_8$    |
|                 | Chalcopyrite    | $CuFeS_2$                                       |
|                 | Brunnerite      | $(Mg, Fe, Mn)CO_3$                              |

Table 2  
Results of chemical analysis of ore

| Compound | ppm | Compound  | ppm   | Compound   | Percent |
|----------|-----|-----------|-------|------------|---------|
| U        | 348 | Co        | 100   | $V_2O_5$   | 0.34    |
| Th       | 35  | Pb        | 10    | $SiO_2$    | 25.47   |
| Mo       | 70  | Sc        | 10    | $TiO_2$    | 0.44    |
| Ni       | 220 | Sn        | <10   | $Al_2O_3$  | 2.16    |
| As       | 130 | Bi        | <30   | $Fe_2O_3$  | 32.14   |
| Zr       | <5  | Cd        | <100  | FeO        | 3.97    |
| Se       | <10 | Hg        | –     | MnO        | <0.01   |
| Y        | <50 | Ba        | <30   | CaO        | 1.22    |
| Nb       | <5  | Be        | <10   | MgO        | 25.31   |
| Ga       | <3  | Sb        | Trace | $Na_2O$    | 0.27    |
| Ge       | <3  | Te        | –     | $K_2O$     | 0.14    |
| Cr       | 30  | $S_{tot}$ | 3200  | $P_2O_5$   | 0.07    |
| Zn       | 10  | $SO_4$    | –     | $H_2O$     | 8.42    |
| Cu       | –   | TREE      | 90    | Au, Ag, Pt | –       |

- Contact time: 7 h
- Liquid to solid ratio: 1 to 1

Specifications of the leach liquor are given in Table 3.

### 3.2. Pachuca column

A pachuca column (volume 1.7 l as shown in Fig. 1) was used in order to implement the “resin-in-pulp” operation (Abramov and Brodski, 1993; Skorovarov, 1975; Laskorin et al., 1977; Tatarnikov and Abramov, 1993; Tatarnikov and Zvonarev, 1995). The entries 8 and 9 were used for agitating the mixture of pulp and resin by air. The air is introduced by entry 1 for holding up the mixture of pulp and resin from tee 12 and this mixture is flushed on the screen from exit 2. The openings of screen are designed for passing the particles of pulp but not resin beads which slide on the surface of screen and return to the column. The pulp

Table 3  
Specification of leach liquor

| Specification    | Amount | Specification      | Amount |
|------------------|--------|--------------------|--------|
| pH               | 1.3    | $SO_4^{2-}$ (g/l)  | 55.58  |
| EMF (mV)*        | 485    | $SiO_2$ (mg/l)     | 1820   |
| U (mg/l)         | 195    | As (mg/l)          | 7      |
| $Fe^{2+}$ (mg/l) | 850    | Th (mg/l)          | <2.5   |
| $Fe^{3+}$ (mg/l) | 1150   | $PO_4^{3-}$ (mg/l) | Trace  |
| V (mg/l)         | 65     | La (mg/l)          | <2.5   |
| Mo (mg/l)        | <5     | Ce (mg/l)          | <2.5   |
| Mn (mg/l)        | 400    | Y (mg/l)           | <2.5   |
| Co (mg/l)        | 32     | Recovery (%)       | 82.7   |
| Free acid (g/l)  | 31.5   |                    |        |

\* Pt versus calomel reference electrode.

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