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# Correlations of kinetic parameters with various system operating conditions for $CO_2$ sorption using $K_2CO_3/Al_2O_3$ solid sorbent in a fixed/ fluidized bed reactor

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#### ABSTRACT

The kinetic parameters for carbon dioxide sorption using potassium carbonate supported on an alumina oxide solid sorbent in a fixed/fluidized bed reactor were investigated using a deactivation kinetic model. The initial parameters of the deactivation model were explored by comparison of the obtained results with experimental data. Then, the effects of varying the three key system operating conditions (inlet gas velocity, sorption temperature and water vapor content) on the kinetic parameters were considered. The obtained breakthrough curves were used for calculation of the kinetic parameters. Finally, the relationship between the obtained kinetic parameters and the system operating conditions were summarized. The selected deactivation model was found to fit well with the experimental data. The reaction rate constant was highest in a turbulent fluidization flow pattern and the initial sorption and deactivation rate constant were dependent on the water vapor content except with excess water vapor content.

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### 1. Introduction

Carbon dioxide  $(CO_2)$  is recognized as a major cause of global warming. The concentration of  $CO_2$  in the atmosphere has increased progressively in the last ten years [7]. When analyzing the  $CO_2$  release contributions, coal combustion in power plants accounts for approximately three-quarters of the total anthropogenic  $CO_2$  emissions worldwide [2]. The U.S. Department of Energy states that more than 300 GW of coal-fired electricity generation currently in operation will increase the concentration of  $CO_2$  in the atmosphere to nearly 450 ppm by 2030 [17]. To mitigate this  $CO_2$  emission problem, methodology to capture or sequester  $CO_2$  is required.

To date, several methods for capturing  $CO_2$  from flue gas have been extensively explored such as solvent absorption, membrane separation and cryogenic fractionation. However, these methods have been restricted by either expensive operating cost or safety

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considerations. Sorption with dry alkali-metal-based solid sorbent is another promising technology for CO<sub>2</sub> capture. When compared to other solid sorbents, Potassium carbonate (K<sub>2</sub>CO<sub>3</sub>) is an interesting solid sorbent owing to easy handling and economic viability [29]. Therefore, solid sorbent development and sorption process improvement are considered to be important research topics. For the solid sorbent development, modifications of K<sub>2</sub>CO<sub>3</sub> solid sorbent have been conducted to improve its performance. The effect of supporting materials on the sorption characteristic has been explored [11], and it has been concluded that the use of K<sub>2</sub>CO<sub>3</sub> supported on Al<sub>2</sub>O<sub>3</sub> (K<sub>2</sub>CO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub>) could be a potential solid sorbent for a large scale operation unit [25]. The calcined K<sub>2</sub>CO<sub>3</sub> from KHCO<sub>3</sub> also showed excellent sorption capacity and a high reaction rate. When considering the process improvement, most of the recent studies that have focused on using  $K_2CO_3/Al_2O_3$  as a solid sorbent were carried out in a thermogravimetric analyzer and fixed bed reactor [14,16,27]. The fixed and fluidized bed reactors were successfully used for various adsorption studies to remove contaminants [8,10,19,23,22,6]. The use of K<sub>2</sub>CO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> solid sorbents with fluidization technology has been proposed as a solution for reducing released CO<sub>2</sub> [1] since fluidization can

#### Nomenclature

- a Activity of sorbent (–)
- $a_0$  Initial activity of sorbent (-)
- A Frequency factor (for  $k_0 = m^3/kg \min$ ; for  $k_d = m^3/kg \min$ )
- C Outlet concentration of  $CO_2$  (% or kmol/m<sup>3</sup>)
- $C_0$  Inlet concentration of  $CO_2$  (% or kmol/m<sup>3</sup>)
- $d_{\rm p}$  Sorbent diameter ( $\mu$ m)
- $E_{a}$  Activation energy (kJ/mol)
- *F* Outlet CO<sub>2</sub> fraction (–)
- $F_{input}$  Inlet gas volumetric flow rate (m<sup>3</sup>/min)
- $F_{\text{output}}$  Outlet gas volumetric flow rate (m<sup>3</sup>/min)
- H Height (m)
- I.D. Internal diameter (m)
- $k_{\rm d}$  Deactivation rate constant (1/min)
- $k_0$  Initial sorption rate constant (m<sup>3</sup>/kg min)
- m Order of reaction with respect to sorbent active site (-)
- *n* Order of reaction with respect to  $CO_2$  concentration (-)
- t Time (min)
- *T* Sorption temperature (K)
- $Q_o$  Volumetric flow rate (m<sup>3</sup>/min)
- *R* Universal gas constant (J/mol K)
- W Weight of sorbent (kg)

Greek letters

 $\rho$  Sorbent density (kg/m<sup>3</sup>)

provide better heat and mass transfers inside a reactor. With this technology, the general flow patterns can be divided into four regimes based on the criterion of the increasing of gas inlet velocity [9]. Jaiboon et al. [9] found that the CO<sub>2</sub> capture capacity of solid sorbent varied in relation to the inlet gas velocity. In addition, the effects of system operating conditions on sorption efficiency were investigated such as sorption temperature, inlet gas composition and gaseous impurities [28].

To design an efficient sorption unit, an understanding of the CO<sub>2</sub> sorption kinetics is important. For the gas-solid particle system, the mass transfer and reaction kinetics may have an effect on the chemical reaction. Recently, the shrinking-core, homogeneous, phenomenological and deactivation simplified models have been used for explaining the non-catalytic gas-solid particle reaction phenomena [15,16,12]. Comparing among these models, the deactivation model was the most successful in describing the decreasing activity of alkali-metal carbonate solid sorbents during the reaction with CO<sub>2</sub> in a thermogravimetric analyzer and in a fixed bed reactor. This can be explained by the changing solid sorbent structure throughout the chemical reaction. The formation of a dense product layer over the solid sorbent brings about additional diffusion resistance and a reduced chemical activity. However, the available data on the kinetic parameters in a fluidized bed reactor are still limited.

In this study, simplified kinetic models were first developed for  $CO_2$  sorption using  $K_2CO_3/Al_2O_3$  as the solid sorbent in both fixed and fluidized bed reactors. The deactivation model was successfully employed to compute the kinetic parameters. The obtained kinetic models were used as the input for mathematical modeling and computational fluid dynamics simulation programs with various system dimensions ranging from zero- to three-dimensions. The system operating conditions of the inlet gas velocity,

sorption temperature and water vapor  $(H_2O)$  content were investigated for their effects on the kinetic parameters of the deactivation model. In addition, the correlation between the obtained kinetic parameters and the system operating conditions were summarized.

#### 2. Kinetic model development

The CO<sub>2</sub> sorption reaction using an anhydrous  $K_2CO_3/Al_2O_3$  solid sorbent proceeds in the presence of  $H_2O$  to yield KHCO<sub>3</sub>, as shown in Eq. (1),

$$K_2 CO_{3(s)} + CO_{2(g)} + H_2 O_{(g)} \Leftrightarrow 2KHCO_{3(s)}$$
(1)

The sorption reaction is a heterogeneous gas-solid particle reaction [1]. As solute enters the bed, it contacts with the first layers of solid sorbent. Solute adsorbs and fills up some of the available sites. Then, it moves further by diffusing to the subsequent layers. This phenomenon takes place until each layer reaches its equilibrium. The simultaneous influence of both the chemical reaction and the transportation must take into account for a correct prediction of the reaction conversion as a function of time. In order to calculate the chemical kinetic of Eq. (1), the CO<sub>2</sub> breakthrough curve is employed in the deactivation model. The breakthrough curve shows the ratio of outlet solute concentration to inlet solute concentration as a function of time. It is a measure of the bulk or average reactor concentration. There are two important parameters related to the breakthrough curves, namely, breakthrough point (the point that the concentration ratio increases up to value higher than the initial one) and exhaust point (the point that the concentration ratio increases up to value about the final one). As stated in the introduction, this model is a proper choice for predicting the CO<sub>2</sub> sorption in a thermogravimetric analyzer and fixed bed reactor [15,16,26,27].

The development of the deactivation model is based on the diffusion resistance due to the formation of a product layer over the solid particle reactant [14,4]. This phenomenon then causes a drop in the chemical reaction rate with time. The effects of all the textural changes on the  $CO_2$  sorption are combined with the reaction rate in terms of the activity (*a*). The following assumptions are made:

- The sorption reaction is operated under isothermal condition.
- The water vapor concentration is constant [28] found that the CO<sub>2</sub> sorption was similar at high water vapor concentration).

With the above assumptions, the pseudo-steady state species conservation equation without axial dispersion [20,14] is expressed as follows:

$$-Q_0 \frac{dC}{dW} - k_0 aC = 0 \tag{2}$$

where *a* is the activity of the sorbent, *W* is the weight of sorbent, *C* is the outlet concentration of  $CO_2$ ,  $Q_o$  is the volumetric flow rate and  $k_o$  is the initial sorption rate constant.

This equation is derived based on the plug flow reactor model [5,13], which defines the solute flowing through the reactor as a series of infinitely thin coherent volume, each with a uniform composition [18]. The key assumption is that the solute is perfectly mixed in the radial direction but not in the axial direction. The plug flow reactor is the ideal reactor case for the real reactor cases, fixed and fluidized bed reactors. The key assumption for a plug flow reactor model then valids for the two reactors. This confirms the validity of using Eq. (2) for prediction of a kinetic parameter. This model has been used to simulate fixed and fluidized bed reactors in numerous studies [4,12]. The integrating of Eq. (2) is shown as the

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