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#### Review

# Transverse combustion instabilities: Acoustic, fluid mechanic, and flame processes



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#### ABSTRACT

Thermoacoustic oscillations associated with transverse acoustic modes are routinely encountered in combustion chambers. While a large literature on this topic exists for rockets, no systematic reviews of transverse oscillations are available for air-breathing systems, such as in boilers, aircraft engines, jet engine augmentors, or power generating gas turbines. This paper reviews work on the problem for air-breathing systems, summarizing experimental, modeling, and active control studies of transverse oscillations. It then details the key physical processes controlling these oscillations by describing transverse acoustic wave motions, the effect of transverse acoustic waves on hydrodynamic instabilities, and the influence of acoustic and hydrodynamic fluid motions on the unsteady heat release. This paper particularly emphasizes the distinctions between the direct and indirect effect of transverse wave motions, by arguing that the dominant effect of the transverse acoustics is to act as the "clock" that controls the frequency and modal structure of the disturbance field. However, in many instances, it is the indirect axial flow disturbances at the nozzles (driven by pressure oscillations from the transverse mode), and the vortices that they excite, that cause the dominant heat release rate oscillations. Throughout the review, we discuss issues associated with simulating or scaling instabilities, either in subscale experimental geometries or by attempting to understand instability physics using identical nozzle hardware during axial oscillations of the same frequency as the transverse mode of interest. This review closes with a model problem that integrates many of these controlling elements, as well as recommendations for future research needs.

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Nomenclature			unsteady heat release rate per unit volume
		r	radial coordinate
$A_{cs}$	cross-sectional area	$u_i$	velocity along coordinate direction i
$\widehat{B}_{i,m_h}$	complex amplitude of helical mode $m_h$ for velocity	$S_L$	laminar flame speed
ı,,,,,	along coordinate i	S	nozzle index in annular combustor, in Fig. 2 and Sec. (
A,G	acoustic wave amplitude	t	time
D.	diameter of inlet nozzle	<i>x</i> , <i>y</i>	Cartesian coordinates for transverse direction
D D	molecular diffusivity	Z	axial coordinate
F	flame transfer function (FTF), defined in Eq. (6)		
G	level-set iso-contour variable	Greek l	etters
G Не	Helmholtz number, $=\omega R/c_0$	Φ	phasing between unsteady heat release and unsteady
	, , ,	_	pressure
L	axial length of model annular combustor	α	aspect ratio of annular combustor, $=L/R$
$L_{\theta}$	circumference of annular combustor based on average	β	ratio of $L_i/L$
	radius, R	р К	temperature ratio between burnt and unburnt gases
$L_i$	axial location of interface of temperature jump	$\phi$	•
$L_f$	flame height	*.	equivalence ratio
M	mach number, $=u_0/c_0$	$\phi_{Ox}$	stoichiometric mass ratio of oxidizer to fuel
Q	global, spatially integrated, unsteady heat release rate	$\varphi$	local azimuthal angle for cylindrical coordinate
R	average radius of annular combustor, $=(a_1 + a_2)/2$		centered on a nozzle
S	swirl number	λ	acoustic wavelength
St	Strouhal number, $=\omega L_f/u_0$	$\mu$	temporal damping coefficient in $exp(-\mu t)$
T	temperature	$\vartheta$	time-varying phase for acoustic wave
$T_a$	acoustic time period	ho	density
V V	combustor control volume	$\theta$	global azimuthal coordinate for annular combustor
-		$ au_{()}$	time-delay parameter
$\widehat{Z}_{o},\widehat{Z}_{out}$	acoustic impedance at burner inflow and combustor	ω	angular frequency, $=2\pi f$
	exit, respectively	χ	flame aspect ratio, $2L_f/D$
$\widehat{Z}_{tr}$	translated impedance	,•	· J.
Z	non-dimensional mixture fraction for non-premixed	Subscri	pts and superscripts
	flames	( )°	stagnation value
$z_{st}$	stoichiometric mixture fraction, =1/(1 + $\phi_{Ox}$ )	( ) <sub>u</sub>	quantity in unburnt region
$a_1, a_2$	inner and outer radius of annular combustor	( ) <sub>b</sub>	quantity in burnt region
u 1, u 2	respectively	( ) <sub>0</sub>	time-averaged component
С	speed of sound	()1	unsteady first order perturbation component
$d_s$	nozzle/burner/injector spacing		
f	frequency	$\widehat{\widetilde{()}}$	Fourier transformed variable
) h	axial length of inlet nozzle section	$\widetilde{()}$	non-dimensionalized variable
	heat of reaction	$\overrightarrow{()}$	vector quantity
$h_R$		$\binom{0}{r}$	radial component
j, n	radial and axial acoustic mode number, respectively		azimuthal component in the nozzle coordinate system
$k,k_h$	spatial wavenumber for acoustics and hydrodynamics,	$()_{\varphi}$	
	respectively	$()_z$	axial component
$m_a$ , $m_h$	azimuthal mode number for acoustics and	$()_{\theta}$	azimuthal component in the annular combustor
	hydrodynamics, respectively		coordinate system
$\dot{m}_F^{''}$	mass burning rate per unit area of flame surface	()ref	reference value
n	FTF gain for thermo-acoustics model in Sec. 6	$()_{MBR}$	mass burning rate contribution
р	pressure		

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