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# Structural behaviour of a GFRP-concrete hybrid footbridge prototype: Experimental tests and numerical and analytical simulations



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## ABSTRACT

Glass fibre reinforced polymer (GFRP) pultruded profiles are being increasingly used in the construction industry since the last few decades. The high potential of GFRP profiles for structural applications stems from their high strength, low self-weight and corrosion resistance. In opposition, the high deformability, the susceptibility to instability phenomena and the lack of specific design codes have been hindering a wider use of these advanced composite materials. Several hybrid systems in which GFRP materials are combined with traditional materials, namely concrete, have been proposed in order to overcome the aforementioned limitations of the GFRP material. This paper presents experimental, analytical and numerical investigations about the flexural behaviour of a GFRP-concrete hybrid footbridge prototype comprising two I-shaped GFRP main girders and a thin steel fibre reinforced self-compacting concrete (SFRSCC) deck. With the aim of limiting the structure's deformability, the footbridge features an external prestress system consisting of two ordinary steel rebars screwed tighten to the structure at the support sections. A small-scale footbridge prototype, 6.0 m long and 2.0 m wide, was built and tested in a 5.5 m simply supported span. The experimental programme included (i) serviceability tests, with and without the application of the external prestress system, and (ii) failure tests. Results of flexural tests proved the feasibility and advantages of the structural concept proposed: the judicious combination of GFRP and SFRSCC enabled the development of a lightweight, high performance and relatively inexpensive structural system for footbridges; furthermore, the external prestress system was very effective in limiting deflections. The analytical and numerical models developed in this study were able to predict with good accuracy (i) the linear elastic behaviour of the structure up to failure, (ii) the effects of the external prestress, and (iii) the failure mode and strength, proving to be accurate tools for the design of GFRP-concrete structural solutions.

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#### 1. Introduction

In the last few decades, the use of fibre reinforced polymer (FRP) materials in general, and of glass fibre reinforced polymer (GFRP) pultruded profiles in particular, has found a significant increase in civil engineering structural applications. In fact, these materials have high potential for both building and bridge structural applications owing to their high strength, low self-weight, chemical resistance, ease of installation and electromagnetic transparency [1–3]. However, the lack of specific standards dealing with the various aspects of the design, the brittle failure, the high deformability and the susceptibility to instability phenomena, which often govern design and seldom allow the full exploitation of the materials' resistance [4–6], have been delaying the widespread use of these materials [7–10].

\* Corresponding author. Tel./fax: +351 2184 17000/99242. E-mail address: jose.gonilha@tecnico.ulisboa.pt (J.A. Gonilha). Several hybrid structural systems combining GFRP elements with traditional materials have been proposed in order to overcome the aforementioned limitations while maintaining the main attractiveness of advanced composite structures. In those systems, the careful combination of GFRP with concrete in flexural members has proven to be particularly effective, namely in reducing shortand long-term deformability and in delaying instability phenomena (*e.g.* [11–19]).

The research presented in this paper is part of a broader research project – *PONTALUMIS* – a collaborative study between Instituto Superior Técnico (IST), Minho University (UM) and composites manufacturer *ALTO*, *Perfis Pultrudidos*, *Lda*. This project aims at developing a lightweight, durable and maintenance-free hybrid footbridge made of two I-shaped GFRP pultruded profiles acting as main girders and a steel fibre reinforced self-compacting concrete (SFRSCC) deck. In order to fully understand the feasibility and structural behaviour of the structural system proposed, the research project included the construction of a small-scale prototype, with a length of 6.0 m, approximately half of the length of the







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### Nomenclature

Symbol	Description	$M_F$	bending moment due to the applied load F
a, b	geometrical parameters of the 4-point bending load	M <sub>max</sub>	maximum bending moment
	configuration	$M_u$	ultimate bending moment
$b_p$	width of the GFRP profiles' flanges	$M_{SW}$	bending moment due to the self-weight
ď	distance between the theoretical support and the rota-	NA	neutral axis position measured from the top fibre of the
0	acceptricity of the prestress repars with respect to NA	D	prostress force
e f	tangila strength of the anowy adhesive	r	prestress force
Jau f	characteristic tensile strength of the stainless steel belts	V(v)	shear force at position y
Jbk f	compressive strength of the SEPSCC	V(X)	shear force due to the applied load E
Jcm f	tonsile cracking strength of the SERSCC	V <sub>F</sub>	shear force due to the self weight
Jcr f	compressive strength of the enough mortan	V <sub>SW</sub>	siled force due to the sen-weight
Jmu f	complessive strength of the CEPD for the longitudinal direct	V <sub>u</sub> V	ultiliate Silear force
Jtu,L	tensile strength of the GFKP for the longitudinal direc-	A V	axial strength in direction 1
1.	LIOII this has a set that CERCCC shall	Y S()	axial strength in direction 2
n <sub>c</sub>	thickness of the SFRSCC slad	$\partial(X)$	deflection at position x
$n_p$	neight of the GFRP profiles	0 <sub>ms</sub>	average midspan deflection
$n_t$	total height of the cross-section	$\partial_{ms1-2}$	midspan deflection measurement positions
1	number of element	$\partial_{ms-u}$	midspan deflection at failure
kA	Timoshenko shear area	$\delta_P(\mathbf{X})$	upwards deflection at position x caused by the prestress
l	free length of the rebars		load P
$t_f$	thickness of the GFRP profiles' flanges	Е <sub>с1-3</sub>	midspan strain measurement positions on the SFRSCC
$t_w$	thickness of the GFRP profiles' webs	Ef1-2	midspan strain measurement positions on the GFRP
x	longitudinal development of the structure		flanges
Z	vertical distance to $z_g$	$\varepsilon_{w1-2}$	midspan strain measurement positions on the GFRP
$Z_g$	neutral axis height with respect to the mid-line of the		webs
	GFRP bottom flanges	$\theta_L$	rotation of the support section due to vertical loads
$Z_{gi}$	vertical position of the stiffness centre of element <i>i</i>	$\theta_P$	rotation of the support section due to prestress loads
$A_i$	area of element <i>i</i>	$\theta_T$	total rotation of the support section
$A_s$	area of the steel rebars	ho	volumetric weight
$A_w$	area of the GFRP webs	$\sigma(x,z)$	axial stress at position $x$ , $z$
Ea	elasticity modulus in tension of the epoxy adhesive	$\sigma_1$	axial stress in direction 1
Ec	elasticity modulus in compression of the SFRSCC	$\sigma_2$	axial stress in direction 2
Ei	elasticity modulus of element <i>i</i>	$\sigma_F$	axial stress due to the applied load F
EI	flexural stiffness of the cross-section	$\sigma_L$	axial stress in longitudinal direction
$E_{L,t}$	elasticity modulus in tension of the GFRP for the longi-	$\sigma_{SW}$	axial stress due to the self-weight
	tudinal direction	$\sigma_T$	axial stress in transverse direction
$E_m$	elasticity modulus in compression of the epoxy mortar	$\tau(x,z)$	shear stress at position $x, z$
$E_s$	elasticity modulus of steel	$\tau_{12}$	shear stress in the plane 1–2
$E_{Tc}$	elasticity modulus in compression of the GFRP for the	$\tau_F$	shear force due to the applied load F
1,0	transverse direction	$\tau_{IT}$	shear stress in the plane defined by the longitudinal and
F	applied load in the 4-point bending load configuration	LI	transverse directions
Faur	compressive strength of the GFRP for the transverse	τ	shear strength of the epoxy mortar
- <i>cu,L</i>	direction	Tew	shear stress due to the self-weight
F.,	failure load	•3₩ 7	in-plane shear strength of the GFRP
G	shear modulus	vu,L1	Poisson's ratio of the SFRSCC
G	shear modulus of the CERP	2	curvature of the cross-section
K	average midsnan stiffness		elongation of the rebars
I	Snan		additional force on the rebars caused by the vertical
$M(\mathbf{v})$	bending moment at position y	Δr	loade
IVI(X)			ivaus

full-scale prototype. Previous studies were already performed in order to investigate the structural behaviour of this small-scale prototype, namely in what concerns the following aspects: (i) performance of different shear connection systems used at the GFRP–SFRSCC interface [20]; (ii) modal (dynamic) identification [21]; (iii) dynamic response of the footbridge under pedestrian loads [6]; and (iv) creep behaviour of the footbridge under sustained loads [19].

This paper presents experimental, analytical and numerical investigations about the short-term static behaviour up to failure of the hybrid GFRP-SFRSCC small-scale footbridge prototype. The remainder of the paper is organised as follows. Section 2 describes the underlying structural concept of the footbridge prototype and details its geometry. Section 3 presents the experimental programme, which included the construction of the footbridge prototype, material characterisation tests on the constituent materials and 4-point bending flexural tests, which aimed at evaluating both the serviceability and failure responses of the prototype, as well as to assess the efficacy of an external prestress system in limiting the deformability of the hybrid structure. Sections 4 and 5 present analytical and numerical simulations of the structural behaviour of the footbridge, in which simple analytical formulae and a three-dimensional finite element model, respectively, were used to predict the serviceability and failure responses of the hybrid footbridge structure.

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