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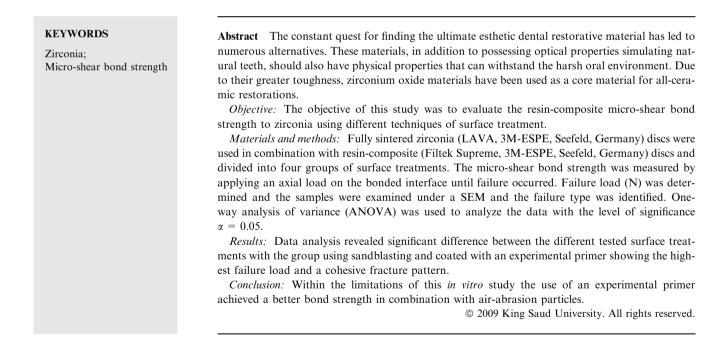
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# Effect of surface treatment on the micro-shear bond strength to zirconia

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### 1. Introduction

A need for non-metallic restorative materials with optimal esthetics and characteristics such as biocompatibility, colour stability, high wear resistance and low thermal conductivity is often stated as a reason for the use of ceramics in dentistry (Vult Von Stevern et al., 2001; Oden et al., 1998). Various materials can be used as all-ceramic core materials such as leucite-reinforced ceramics, glass-infiltrated ceramics, lithium disilicate, alumina and zirconia (Aboushelib et al., 2007).

The greater toughness of zirconium oxide ceramics compared to that of aluminum oxide ceramics has made zirconia a favorite choice as core material for all-ceramic restorations (Christel et al., 1989). In contrast to conventional felspathic ceramics, the matrix pressure on the tetragonal particles of zirconium oxide is reduced by tensile stresses that induce a transformation of the tetragonal to a monoclinic phase, known as the transformation-toughening property. This property is associated with a localized volumetric increase of 3-5% resulting in compressive stresses that counteract the external tensile stresses and, in this way, may prevent cracks from propagating (Christel et al., 1989; Luthardt et al., 2002).

Due to their chemical inertness, zirconia frameworks are resistant to aggressive chemical agents such strong acids as hydrofluoric acid (Derand and Derand, 2000), alkalis, and organic and inorganic dissolving agents. Other techniques which are based on increasing their surface roughness failed to establish a strong and durable bond with adhesive resin cements. Different investigations have examined and measured the shear bond strength of different cements on zirconium oxide ceramic surface after different pre-treatments. These studies provide varying and controversial results (Derand and Derand, 2000; Blatz et al., 2004; Wegner and Kern, 2000; Piwowarczyk et al., 2005).

Several coating agents were used to enhance the formation of chemical bonding with zirconia and only those agents that contain a phosphate monomer agent (MDP) were effective in establishing a reliable bond with zirconia materials (Blatz et al., 2004; Wegner and Kern, 2000).

In a recent study, application of MDP monomer on nonretentive (as-sintered) zirconia surface failed to produce any bond with zirconia as most of the specimens demonstrated premature failure which questions the role of this MDP agent (Aboushelib et al., 2008).

Focusing on the long-term zirconia resin bond stability, a recent study shows that it is directly related to the chemistry of the used materials, including primers. The authors suggested that a more hydrophobic compound is required to better resist the detrimental effect of hydrolysis in order to gain full benefit from the used primers (Aboushelib et al., 2009).

As a novel approach to enhance zirconia resin bond strength, selective infiltration-etching (SIE) of zirconia-based materials was introduced to create a retentive surface where the adhesive resin can infiltrate and interlock in order to establish a strong and a durable bond with zirconia (Aboushelib et al., 2007).

The micro-shear bond test method for measuring bond strength was introduced (Mcdonough et al., 2002). Compared with the conventional shear bond test, the stress distribution is more concentrated at the interface in the micro-shear bond test (Banomyong et al., 2007) which reduces the chance of cohesive failure in the material that does not represent the "true" interfacial bond strength.

The aim of this study was to evaluate the resin-composite micro-shear bond strength to zirconia using different techniques of surface treatment. The null hypothesis tested was that there was no difference between different surface treatments on bond strength of resin-composite to zirconia.

#### 2. Materials and methods

#### 2.1. Preparation of the specimens and bonding procedure

Fully sintered zirconia (LAVA, 3M-ESPE, Seefelf, Germany) discs (19.5 mm  $\times$  3 mm) were used in combination with resincomposite (Filtek Supreme, 3M-ESPE, Seefeld, Germany) discs (2 mm  $\times$  2 mm) and were divided into four groups as follows:

Group 1 (Control): Ten resin-composite discs (n = 10) were bonded on top of the surface of the zirconia disc using a self-cured resin-composite cement (Multilink, Ivoclar-Vivadent, Schaan, Liechtenstein) under a fixed load of 20 N. Excess cement was wiped off using microbrush.

Group 2: n = 10: Same procedure as that for Group 1 but zirconia disc was sandblasted with 120 µm aluminum oxide particles (S-U-Alustral, Schuler-Dental, Ulm, Germany) at 0.35 MPa pressure prior to bonding procedures.

*Group 3:* n = 10: Same procedure as that for Group 2 but the sandblasted zirconia disc was coated with adhesive agent (Multilink primers A and B) prior to bonding procedures.

Group 4: n = 10: Same procedure as that for Group 2 but the sandblasted zirconia disc was coated with an experimental primer as described by Aboushelib et al. (2008) (The silane monomers used in the primers were 3-acryloyloxypropyltrimethoxysilane, 3-isocyanatopropyltriethoxysilane, styrylethyltrimethoxysilane, 3-methacryloyloxypropyltrimethoxysilane and 3-(*N*-allylamino)propyltrimethoxysilane.) prior to bonding procedures.

#### 2.2. Testing procedure

The micro-shear bond strength was measured by applying an axial load on the bonded interface using a universal testing machine (Accuforce Elite Test Stand, Ametek, Mansfield & Green Division 8600 Somerset Drive Largo, Florida, USA). Loading was performed at a crosshead speed of 1 mm/min until failure occurred.

Failure load (N) was extracted from the computer-generated data files.

The broken resin discs and zirconia discs were ultrasonically cleaned, dried, gold sputter coated and examined under a SEM (JEOL JSM-6360LV, Japan) and failure type was classified into interfacial failure across the zirconia–resin interface resulting in exposure of the zirconia surface or cohesive failure in the composite material or the adhesive resin.

One-way analysis of variance (ANOVA) was used to analyze the data with the level of significance  $\alpha = 0.05$ . The Kolmogorov–Smirnov post-hoc test was used and showed normal distribution.

### 3. Results

Data analysis revealed significant differences with regard to the mean micro-shear bond strength values measured in MPa units between Groups 1, 2 and 3 (Table 1), while significant difference was noted between the previous groups and Group 4 (F = 25.683, P < 0.001). No significant difference was noted between Groups 2 and 3 (P > 0.001).

SEM observations of the specimens showed predominant interfacial failure type especially in Groups 1, 2 and 3 while Download English Version:

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