



# Energy dispatching based on predictive controller of an off-grid wind turbine/photovoltaic/hydrogen/battery hybrid system



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## ARTICLE INFO

### Article history:

Received 27 December 2013

Accepted 4 August 2014

Available online 30 August 2014

### Keywords:

Energy dispatching

Hydrogen system

Off-grid system

Predictive control

Renewable energy

## ABSTRACT

This paper presents a novel energy dispatching based on Model Predictive Control (MPC) for off-grid photovoltaic (PV)/wind turbine/hydrogen/battery hybrid systems. The renewable energy sources supply energy to the hybrid system and the battery and hydrogen system are used as energy storage devices. The denominated “hydrogen system” is composed of fuel cell, electrolyzer and hydrogen storage tank. The MPC generates the reference powers of the fuel cell and electrolyzer to satisfy different objectives: to track the load power demand and to keep the charge levels of the energy storage devices between their target margins. The modeling of the hybrid system was developed in MATLAB-Simulink, taking into account datasheets of commercially available components. To show the proper operation of the proposed energy dispatching, a simpler strategy based on state control was presented in order to compare and validate the results for long-term simulations of 25 years (expected lifetime of the system) with a sample time of one hour.

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## 1. Introduction

The current situation of the energy sector with a continuous increase in the energy demand, together with the Greenhouse gas emissions and the exhaustion of the fossil fuel reserves have enhanced the combination of renewable energy sources for distributed generation. This combination is denominated Hybrid Renewable Energy Systems (HRES) or simply Hybrid Systems (HS) which are composed by one or more renewable energy sources and energy storage systems (ESS). ESS allow adapting the unregulated power generated by the renewable sources to a specific demanded power. This HS can work in stand-alone [1,2] or grid-connected mode [3–7].

The correct design of the energy dispatching for HS is essential for their operation. energy dispatching strategies are designed to track the load power satisfying secondary objectives such as keeping the charge level of the energy storage devices within their operational limits, minimizing the generation costs, operating the

system at high efficiency, reducing the fuel consumption, etc. The papers related to energy dispatching can be classified according to these objectives [8].

Depending on the objectives to meet by the energy dispatching there are two kinds of simulations that can be carried out: short-term and long-term simulations. Short-term simulations are focus on the dynamics of the sources which compose the system and take them into account to face the net power variations due to the changes in load power or disturbances in the renewable energy sources. The length of this kind of simulations goes from 200 s to one day [9–11]. Long-term simulations are used when the main objective is to show the proper operation of the system during a considerable period of time (from months to the whole life of the system) [12–15]. In this case, the dynamics of the energy sources are neglected and they pay attention to other parameters such as operation costs, degradation of the sources, level of charge of the storage devices, etc. Model Predictive Control (MPC) has been widely used in the energy dispatching design because of its ability to deal with constraints in a systematic and straightforward manner. In Ref. [16], the HS was composed by wind turbine, PV, electrolyzer and fuel cell. The energy generated by the renewable sources (both controlled by Maximum Power Point Tracking – MPPT-algorithms) was stored as hydrogen. Depending on if the

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**Nomenclature**

$A, B, C$	matrices of the HS state space model	$P_{rnw}$	power generated by the renewable energy system, (W)
$A_{bat}$	exponential zone amplitude of the battery, (V)	$P_{turb}$	power captured by the wind turbine blades, (W)
$B_{bat}$	exponential zone time constant inverse of the battery, (Ah) <sup>-1</sup>	$P_{wt}$	power generated by the wind turbine, (W)
$C_{1,...,6}$	power curve coefficients of the wind turbine, (-)	PEM	proton exchange membrane
$C_p$	power coefficient of the wind turbine, (%)	PV	photovoltaic
$D_c$	duty cycle, (pu)	PWM	pulse width modulation
$E_{low,H_2}$	lower heating value of hydrogen, (J/kg)	$p_{bat}^{char}$	battery charge power, (W)
$E_{bat}^0$	battery constant voltage, (V)	$p_{bat}^{dis}$	battery discharge power, (W)
$E_{fc}^{cycle}$	energy supplied by the fuel cell which reduces the level of the hydrogen tank from 100% to 20%, (Wh)	$p_{H_2}$	hydrogen partial pressure, (Pa)
$E_{lz}^{cycle}$	energy supplied to the electrolyzer which increases the level of the hydrogen tank from 20% to 100%, (Wh)	$p_{H_2O}$	water partial pressure, (Pa)
$E_{bat}^{char}$	charge energy that the battery must absorb with the EMS, (Wh)	$p_{O_2}$	oxygen partial pressure, (Pa)
$E_{bat}^{dis}$	discharge energy that the battery must deliver with the EMS, (Wh)	$q$	elementary charge of an electron, (C)
$E_{bat}^{year}$	energy that the battery is expected to deliver during a year, (Wh)	$Q$	battery capacity, (Ah)
$E_{fc}^{dis}$	energy that the fuel cell must deliver with the EMS, (Wh)	$q_{H_2,in}$	hydrogen input flow to the anode, (kg/s)
$E_{lz}^{char}$	energy that the electrolyzer must absorb with the EMS, (Wh)	$q_{H_2,out}$	hydrogen output flow to the anode, (kg/s)
$E_{net}^{char}$	total net charge energy, (Wh)	$q_{H_2,react}$	hydrogen flow that reacts in the anode, (kg/s)
$E_{net}^{dis}$	total net discharge energy, (Wh)	$q_{O_2,in}$	oxygen input flow to the anode, (kg/s)
ESS	energy storage system	$q_{O_2,out}$	oxygen output flow to the anode, (kg/s)
$F$	Faraday constant, (C/kmol)	$q_{O_2,react}$	oxygen flow that reacts in the anode, (kg/s)
$H_C$	control horizon	$R_{bat}$	battery internal resistance, ( $\Omega$ )
$H_P$	prediction horizon	$R_p$	PV parallel resistance, ( $\Omega$ )
HRES	hybrid renewable energy systems	$R_s$	PV series resistance, ( $\Omega$ )
$I_{ph}$	solar-induced current, (A)	SOC	state of charge
$I_{ph0}$	solar-induced current at a temperature of 300K, (A)	SPWF	series present worth factor
$I_{sat}$	saturation current of the diode, (A)	$T_a$	aerodynamic torque acting on the blades, (Nm)
$i^*$	battery filtered current, (A)	$T_{pv}$	PV operating temperature, (K)
$i_{bat}$	battery current, (A)	$T_{ref}$	aerodynamic torque reference, (Nm)
$i_{bat}^t$	actual battery charge, (Ah)	$u_{min}$	lower constraints for the model inputs
$i_{lz}$	electrolyzer current, (A)	$u_{max}$	upper constraints for the model inputs
$K$	Boltzmann constant, (JK <sup>-1</sup> )	$V_{act}$	fuel cell activation voltage drop, (V)
$K_0$	constant depending on the characteristics of the PV, (-)	$V_{bat}$	battery voltage, (V)
$K_1$	constant depending on the characteristics of the PV, (-)	$V_{conc}$	fuel cell concentration voltage drop, (V)
$K_b$	battery polarization constant, (V/(Ah))	$V_{fc}$	fuel cell output voltage, (V)
$k$	sampling time	$V_g$	band gap voltage of the semiconductor used in the PV, (V)
$M_{H_2}$	total hydrogen mass consumption, (kg)	$V_{irrev}$	fuel cell irreversible voltage, (V)
MPC	model predictive control	$V_{oh}$	Fuel cell ohmic voltage drop, (V)
MPPT	maximum power point tracking	$V_{pv}$	voltage across the solar cell electrical ports, (V)
$N$	quality factor of the diode of the PV model, (-)	$v_t$	wind speed, (m/s)
$n_{H_2}$	produced hydrogen, (mol/s)	$W_u$	input weight factors
$n_{lz}$	number of electrolyzer cells in series, (-)	$W_y$	output weight factors
$P_{fc}$	fuel cell power, (W)	$x, r, u, y$	model states, setpoints, manipulated variables and model outputs
$P_{load}$	power demanded by the load, (W)	$y_{min}$	lower constraints for the model outputs
$P_{lz}$	electrolyzer power, (W)	$y_{max}$	upper constraints for the model outputs
$P_{net}$	net power, (W)	$\eta_F$	Faraday efficiency, (%)
$P_{pv}$	power generated by the PV system, (W)	$\eta_{H_2}$	hydrogen system efficiency
		$\eta_{bat}$	battery efficiency
		$\eta_{HS}$	HS efficiency
		$\lambda$	tip speed ratio of the rotor blade tip speed to wind speed, (-)
		$\lambda_{O_2}$	oxygen excess ratio, (-)
		$\rho$	air density, (kg/m <sup>3</sup> )
		$\omega_t$	rotational speed, (rad/s)

renewable power was higher or lower than the demanded power, the electrolyzer or the fuel cell worked. Both, the fuel cell and the electrolyzer, had a MPC which generated their reference current subject to their dynamic constraints. The objective of the strategy was to meet the load demand taking into account the dynamic limitations of the energy sources but it was not shown if the

strategy is able to maintain the hydrogen level in the tank. Vahidi et al. [17] studied a simple HS for stand-alone applications composed by a fuel cell connected to a load by a DC/DC converter. The fuel cell was assisted by an ultra-capacitor which was directly connected to the DC bus. A MPC generated the reference current of the fuel cell in order to ensure an optimal distribution of current

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