



# Hydrogen production by catalytic cracking of rice husk over $\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$ catalyst

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## ABSTRACT

$\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  catalyst is prepared by incipient wetness impregnation. The catalyst is characterized by temperature programmed reduction (TPR), X-ray diffraction (XRD), scanning electron microscope (SEM) and thermogravimetric analysis (TGA). The catalytic activity of  $\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  catalysts is evaluated via the experimental study on the catalytic cracking of rice husk to produce hydrogen in a self made biomass continuous pyrolysis system. The results show that the reaction activities of the catalysts are greatly influenced by the calcinations temperature for catalyst, the secondary catalytic pyrolysis temperature and the mass ratio of Fe to Al. When the calcinations temperature is 550 °C, the pyrolysis temperature is 500 °C, the secondary catalytic pyrolysis temperature is 700 °C, and the Fe to Al mass ratio is 0.07, the experimental results indicate that  $\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  catalyst could fully convert the volatile matters from biomass pyrolysis into small molecular gases such as  $\text{H}_2$ ,  $\text{CH}_4$ ,  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{C}_2\text{H}_4$  and  $\text{C}_2\text{H}_6$ . Meanwhile, the catalyst has shown fine catalytic activity and stability as well as good resistance to coke deposition.

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## 1. Introduction

At present, there is a growing interest in the use of hydrogen as a clean energy vector, especially for power generation in fuel cells. In this respect, hydrogen production from renewable biomass is particularly suitable for sustainable development concerns [1]. The methods of hydrogen production from biomass energy at home and abroad are mainly thermochemical conversion, microbial conversion and chemical reforming. Biomass thermochemical conversion for hydrogen production includes gasification, supercritical conversion, high temperature decomposition and methane, methanol, ethanol conversion and so on [2,3]; the microbial conversion includes direct biological photolysis, indirect biological photolysis, light fermentation, dark fermentation, and microbial fuel cell technology; and the chemical reforming process can also convert methane, methanol, ethanol and other simple compounds into hydrogen [4–7].

To obtain hydrogen from biomass, pyrolysis and gasification are two main effective thermochemical conversion methods. In the process of traditional pyrolysis, with air introduced in the over all process, the energy density of gas product is decreased due to the

appearance of  $\text{N}_2$  and  $\text{CO}_2$  dilution, resulting in increased difficulty in gas separation [8]. More important, there is always large content of tar that is a serious threat to the downstream fuel cell system, both for the electrodes and for the pipelines in the traditional gas producing process [9–13]. The method of continue pyrolysis was adopted in order to avoid air being introduced, and to improve the purity of hydrogen. Moreover, the tar content in the pyrolysis gas was decomposed through the second catalytic cracking. At present, due to the advantages of converting tar into useful gases and adjusting the compositions of producer gases, the method of catalytic cracking for producing hydrogen-rich gas has been more interested since the middle 1980s. In the biomass catalytic cracking process, the dolomite and the Nickel-based catalysts are two kinds of the most common catalysts. The calcined dolomite is a highly efficient catalyst for removing tar, however, the conversion rate of tar catalyzed by dolomite was difficult to reach or exceed the range of 90–95%. Although dolomite could reduce the tar in the producer gas and change the distribution of tar compositions, it was difficult to convert the heavy tars [14]; as described by Zhang [15], Nickel supported on silica was active for tar catalytic cracking at relatively low temperature (550 °C), however, these catalysts could only maintain their activities for a short time because of large amounts of coke accumulation on their surfaces [16,17]. Merete Hellner Nilsen et al observed that Fe–Al–MCM-41 material could altered the quality of the bio-oil, especially significantly decreasing amount of phenols, acids, phenol compounds in comparison to the non-

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catalytic runs [18]. Moreover, the characteristics of  $\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  could be satisfied with the criteria for catalyst.

## 2. Experiment

### 2.1. Reagents and instruments

The rice husk in the experiment was purchased from a rice processing plant in Zengcheng, Guangzhou. The distribution of rice husk particle size and approximate analysis result were shown in Table 1. The compositions of volatile matters are some small molecular gases (such as  $\text{H}_2$ ,  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{CH}_4$  and etc.) and some organic substances (such as acids, phenols and etc.).

$\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  ( $\geq 98.50\%$  in purity) was purchased from Fuchen Chemical Reagent Co., Ltd. in Tianjin. And  $\gamma\text{-Al}_2\text{O}_3$  carrier was purchased from Xinyu Chemical Packing Co., Ltd, whose composition is as follows:  $\text{SiO}_2 + \text{Al}_2\text{O}_3 \leq 5\%$ ,  $\text{Fe}_2\text{O}_3 \leq 1\%$ ,  $\gamma\text{-Al}_2\text{O}_3 \geq 93\%$ ,  $D = 3.6\text{--}4.7$  mm. The  $\text{H}_2$  ( $\geq 99.99\%$  in purity) and  $\text{N}_2$  ( $\geq 99.99\%$  in purity) are from Wugang Gas Co., Ltd in Shanghai.

The temperature programmed reduction (TPR) of catalyst was carried out on the AutoChemII-2920 instrument from Micromeritics Co., Ltd. The 0.05 g of catalyst sample was pretreated by heating in Argon flow to a temperature of  $600^\circ\text{C}$  and keeping the temperature for 2 h in order to remove the adsorbed water and other contaminants and then cooling to  $40^\circ\text{C}$ . Subsequently, the sample was heated up to  $800^\circ\text{C}$  at a heating rate of  $10^\circ\text{C}/\text{min}$  while the  $10\%\text{H}_2/\text{N}_2$  mixture flowed over it at a flow rate of  $20\text{ ml}/\text{min}$ . The effluent gas passed through a cold trap for removing the water content before the amount of hydrogen consumed during the reduction process being measured by the TCD detector. The scanning electron microscopic analysis on the catalyst was performed by FEI-XL30 environmental scanning electron microscope (SEM) with the accelerating voltage of  $20\text{ kV}$ . The X-ray powder diffractograms were recorded following the step-scanning procedure (step size =  $0.028$ , two theta degree scanning from  $0$  to  $80$ ) by using a computerised D/max-Ra diffractometer (Cu K $\alpha$  radiation,  $\lambda = 0.15418\text{ nm}$ ). At a heating rate of  $10^\circ\text{C}/\text{min}$  and a nitrogen flow rate of  $50\text{ cm}^3/\text{min}$ , the thermal analysis (TG and DSC) on the catalyst was carried out on a STA449C Jupiter<sup>®</sup> Simultaneous produced in NETZSCH Co., Ltd of German. A Pt crucible was used to contain about  $0.89\text{ mg}$  of sample for the thermal analysis. The Fourier transmission infrared (FT-IR) spectra of the catalyst powders (as pellets in KBr) were recorded by using a Fourier transmission infrared spectrometer (Spectrum One FT-IR Spectrometer, Bruker VERTEX70, Germany) within the range of  $4000\text{--}400\text{ cm}^{-1}$ .

For the pyrolysis producer gas, the GC analysis was performed by Agilent 6820 Gas Chromatograph (for  $\text{H}_2$ ,  $\text{CO}$ ,  $\text{CH}_4$ ,  $\text{CO}_2$ ,  $\text{C}_2\text{H}_4$  and  $\text{C}_2\text{H}_6$ ) with  $\text{N}_2$  as carrier gas. The GC is equipped with a HP-PLOT-Q column which is  $30\text{ m}$  in length and  $30^\circ\text{C}$  in temperature. The thermal conductivity detector (TCD) temperature was  $250^\circ\text{C}$ .

### 2.2. Catalyst preparation

The  $\text{Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  catalysts were prepared by impregnating  $\gamma\text{-Al}_2\text{O}_3$  with  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  aqueous solutions of different concentrations, and stirring for 2 h at room temperature, followed by drying at  $70^\circ\text{C}$  overnight. The material was then calcined in air for 8 h at a desired value among  $500^\circ\text{C}$  and  $700^\circ\text{C}$ . By changing the concentration of  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  solution, the Fe dosages in the

catalyst were controlled according to the ratios of Fe to Al, which are 0.02, 0.05 and 0.07 respectively.

### 2.3. Testing and analysis on the catalytic activity

Catalytic tests were conducted by using the biomass continuous pyrolysis system, which was made by us and shown in Fig. 1. The screw conveyor is made of mild steel, which length and diameter were  $1000\text{ mm}$  and  $26\text{ mm}$ , respectively. The number of revolution of the conveyor center axis was set at  $18\text{ r}/\text{min}$ .

Rice husk was continuously transported to the pyrolysis reactor from the hopper by the screw feeder. The feeding rate was controlled by the rotary speed of the screw. The rice husk feeding rate was  $390\text{--}410\text{ g}/\text{h}$ . The temperature in the pyrolysis reactor was set at  $500^\circ\text{C}$ . The volatile pyrolysis constituents were piped into the catalytic cracking furnace through heat-insulated pipelines. Around  $200\text{ g}$  of catalyst was placed in the catalyst bed in a quartz tube reactor fixed by two quartz brackets in the cracking furnace. The catalyst bed temperature was monitored by the central thermocouple in catalytic cracking furnace. For the catalytic test, all the catalysts had been reduced in  $\text{H}_2/\text{N}_2$  ( $10/90$  in vol.%) mixture at  $800^\circ\text{C}$  for  $120\text{ min}$  with the heating rate of  $10^\circ\text{C}/\text{min}$ . After reduction of the catalyst, the catalytic cracking experiment was conducted. The charcoal yielded from rice husk pyrolysis, which is  $32\text{--}35\%$  of the total weight of rice husk, was pushed into the char box by the screw.

The gas flow rate was measured by a gas flowmeter. The pyrolysis gas, which was collected every  $5\text{ min}$  with collecting bag, was analyzed by GC (Agilent GC6820).

For the same experiment, it was run for two times. And the data of the experimental was similar. Therefore, one of them was chosen to finish the Figs. 7–9.

$T_0$ : Calcinations temperature,  $T_1$ : Pyrolysis temperature,  $T_2$ : Secondary catalyst cracking temperature, Fe/Al: Fe/Al mass ratio,  $W_{\text{H}_2}$ : Concentration of  $\text{H}_2$ ,  $W_{\text{H}_2} = V_{\text{H}_2}/V_{\text{gases}}$ .

## 3. Results and discussion

### 3.1. Characterization of catalyst

The TG/DTG/DSC curves were presented in Fig. 2. From the figure, the TG and DTG curves showed the mass losses due to thermal decomposition at a  $\text{N}_2$  atmosphere that occurred in two distinct regions. The Region 1 was observed that was from the ambient temperature to  $127^\circ\text{C}$  with a peak at  $92^\circ\text{C}$ . The mass loss in this region was characterized of released hygroscopic water. The Region 2, which was from  $127$  to  $480^\circ\text{C}$ , was characterized by a two-steps decomposition process of Nitrate hydrate. It was concluded from the TG curves that the catalyst calcinations temperature must be higher than  $480^\circ\text{C}$  in order to enable Nitrate hydrate to completely decompose. Between the ambient temperature and  $693^\circ\text{C}$ , the DSC curves showed three well defined exothermic peaks due to the three effects of mass losses. Over  $693^\circ\text{C}$ , the DTG curve was smooth. But there was an obvious peak appearing in DSC curve attributed to the hercynite formation by melting  $\text{Fe}_2\text{O}_3$  into  $\gamma\text{-Al}_2\text{O}_3$ , which was in accordance with XRD pattern. In XRD pattern, the special peaks of hercynite were found in catalyst that was calcined at  $700^\circ\text{C}$ .

**Table 1**  
Granularity distributing and industrial analysis of rice husk.

Distribution of particle size/%					Industrial analysis/(wt) %			
>350 $\mu\text{m}$	350–245 $\mu\text{m}$	245–198 $\mu\text{m}$	198–165 $\mu\text{m}$	<165 $\mu\text{m}$	Moisture	Ash	Volatile material	Carbon fixation
0.89	26.70	41.06	12.61	18.75	2.47	12.67	67.57	17.30

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