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# Determination of mean shear wave velocity to 30 m depth for site classification using shallow depth shear wave velocity profile in Korea



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#### ABSTRACT

The mean shear wave velocity to a depth of 30 m ( $V_S30$ ), established in the western United States, is the current site classification criterion for determining the seismic design ground motion, taking site amplification potential account into. To evaluate  $V_S30$  at a site, a shear wave velocity ( $V_S$ ) profile extending to a depth of at least 30 m must be acquired using in situ seismic tests. In many cases, however, the obtained  $V_S$  profile does not extend to a depth of 30 m due to unfavorable field conditions and limitations of testing techniques. In this study,  $V_S30$  and the mean shear wave velocity to depths less than 30 m ( $V_SDs$ ) were calculated using  $V_S$  profiles of more than 30 m obtained by seismic tests at 72 sites in Korea, and the correlation between  $V_S30$  and  $V_SDs$  was drawn based on the computed mean  $V_S$  data. Additionally, a method for extrapolating the  $V_S$  profile from shallow depths to 30 m and bedrock was developed by building a shape curve based on the average data of all  $V_S$  profiles. These two methods of extrapolating  $V_S30$  from shallow  $V_S$  profiles, using  $V_SDs$  and a shape curve, resulted in less bias than the simple method in which the lowermost  $V_S$  value obtained is extended to the depth of 30 m. These two extrapolation methods are useful for  $V_S$  profiles extending to depths of at least 10 m. Furthermore, the shape curve method developed in this study may be useful in the western United States as well as in Korea.

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#### 1. Introduction

The dynamic characteristics of a site can be represented by shear wave velocity  $(V_S)$ . Current earthquake-resistant design codes [1–5] suggest that the mean  $V_S$  of the upper 30 m  $(V_S30)$  be used to characterize site conditions [6–8]. Site coefficients (or site amplification factors), which quantify local site effects, can be determined based on the site classification system according to  $V_S30$  [9–12]. Design ground motion is estimated by combining the reference rock motion and the site coefficients for short-period  $(F_a)$  and mid-period  $(F_\nu)$  associated with seismic amplification effects [9,11,13]. The most important factor in these determinations is the  $V_S$  profile with depth at the site.

Site conditions can be characterized into five categories (denoted by A through E) according to the  $V_S30$  described in current seismic design codes, as listed in Table 1 [1,2,5]. Although a depth of 30 m (100 ft) is very shallow in seismological terms, it is the depth of conventional borehole drilling and of detailed geotechnical studies in the western United States (US), where the depth to bedrock (H) is

comparatively large [14]. The geological conditions and dynamic properties of material near the ground surface contribute significantly to seismic site responses [15,16], so  $V_S30$  is very useful for earthquake engineering [17–19].  $V_S30$  is calculated from the time taken by a shear wave to travel from a depth of 30 m to the ground surface. For a profile consisting of n soil and/or rock layers,  $V_S30$  can be calculated as

$$V_S 30 = 30 / \sum_{i=1}^{n} \frac{d_i}{V_{Si}}$$
 (1)

where  $d_i$  and  $V_{Si}$  are the thickness and the  $V_S$  of each soil or rock layer to a depth of 30 m (30 m= $\Sigma d_i$ ), respectively. To use  $V_S$ 30 in seismic site categorization, the  $V_S$  distribution to a depth of more than 30 m should be acquired from seismic tests in the field. Despite the requirement for the  $V_S$  profile to have a considerable depth,  $V_S$ 30 has been applied widely as the sole criterion for classifying site conditions in most current earthquake-resistant design codes because of its simplicity and lack of ambiguity [20,21].

Several in situ seismic testing techniques have been developed to determine  $V_S$  profiles worldwide [22–24]. In Korea, existing techniques are being improved by incorporating the ability to include local field conditions [25,26]. To determine  $V_S$  for earthquake-resistant applications in a particular area using seismic testing, a  $V_S$  profile that

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covers a depth of at least 30 m from the ground surface must be acquired. However, testing that extends beyond 30 m may result in unreliable variables because of incomplete knowledge of the subsurface environment. Furthermore, a particular in situ testing method or instrument may be useful for only a limited range of ground conditions and depths [11]. Recently, geotechnical and geophysical testing techniques, including in situ seismic survey methods, and hybrid in situ testing techniques such as the seismic piezocone penetration test (SCPTu) and the seismic dilatometer test (SDMT), have been successfully combined to evaluate various geotechnical characteristics [27,28]. Penetration tests, however, remain limited in the depth to which they can provide meaningful  $V_{\rm S}$  data.

**Table 1** Site classification system with  $V_s$ 30 of the current earthquake-resistant design guidelines [1–3,5].

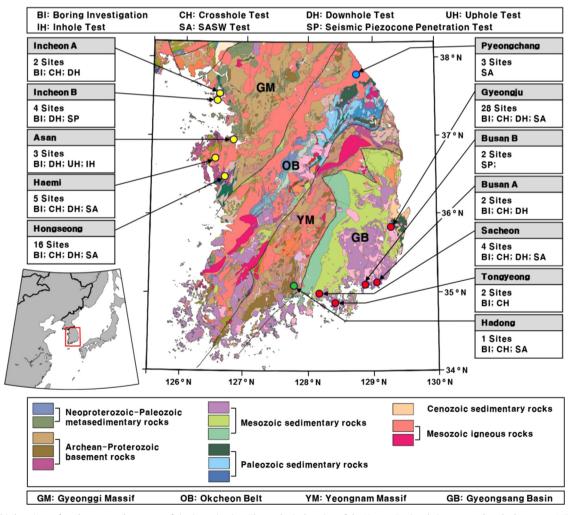
Site class (soil profile type)	Generic description	Mean $V_S$ of top 30 m, $V_S$ 30 (m/s)
A (S <sub>A</sub> ) B (S <sub>B</sub> ) C (S <sub>C</sub> )	Hard rock Rock Very dense soil and soft rock	$1500 < V_S 30$ $760 < V_S 30 \le 1500$ $360 < V_S 30 \le 760$
D (S <sub>D</sub> ) E (S <sub>E</sub> ) F (S <sub>F</sub> )	Stiff soil Soft soil Requires site-spe	$180 < V_s 30 \le 360$ $V_s 30 \le 180$ ecific evaluation

The  $V_S$  profiles acquired from different in situ seismic tests are used to determine near-surface earthquake ground motion. The two most commonly used methods for determining the ground motion are site classification based on  $V_S30$  and site-specific seismic response analysis using the  $V_S$  profile of soil strata and the unique  $V_S$  of infinite-assumed bedrock. Recently several researchers [13,24,29,30] have proposed another method of site classification that uses the predominant (or fundamental) site period ( $T_G$ ) determined using Eq. (2), but this method has not yet been officially sanctioned in earthquake-resistant design guidelines. The site period is based on the thickness of the soil layers overlying the bedrock at each site and their  $V_S$ 

$$T_G = 4 \sum_{i=1}^{n} \frac{D_i}{V_{Si}}$$
 (2)

where  $D_i$  and  $V_{Si}$  are the thickness ( $H = \sum D_i$ ) and  $V_S$ , respectively, of the ith layer above bedrock. Regardless, all of these methods require  $V_S$  profile data.

As a result of the complex factors discussed above,  $V_S$  profiles to a depth of 30 m might not be obtainable for a given site [11,17]. To determine earthquake ground motion in the context of current seismic design guidelines [31], it is necessary to calculate  $V_S$ 30 (the criterion for site classification), which means that sites with  $V_S$  data that do not extend to a depth of 30 m cannot be evaluated properly [11,32]. Several studies [17,33,34] have used  $V_S$  profiles of



**Fig. 1.** Geographic locations of study areas and contents of site investigation. The geological setting of the Korean Peninsula is presented as the base map. Within the box for each study area, the first line is the name of the study area and the second and third lines are the number of site locations and the in situ investigation methods adopted in the study area, respectively. In total, the target area of this study contains 12 study areas and the associated 72 test sites.

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