

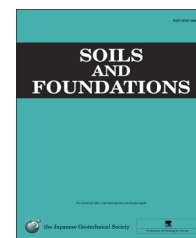


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Strength and deformation characteristics and small strain properties of undisturbed gravelly soils

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Abstract

A series of medium-scale and large-scale triaxial and unconfined compression tests was conducted in order to evaluate the strength and deformation characteristics and small strain properties of undisturbed well-graded gravelly soils retrieved from three tunnel excavation sites in Toyama prefecture, Japan. Undisturbed gravelly soils were taken by means of a new sampling method using thick water-soluble polymer solutions. The strength and deformation characteristics were evaluated mainly by performing sustained loading and large amplitude unloading and reloading cycles during otherwise monotonic loading at a constant strain rate in drained triaxial compression tests. During isotropic consolidation and shearing, at several stress states, eleven very small vertical cycles were applied to evaluate the quasi-elastic deformation property at small strain levels around 0.001% by static measurement. Dynamic measurements using a pair of accelerometers attached to the side surface of the specimen and wave sources attached to the top cap were also conducted at the same stress levels as static measurements in a single test. Several effects including grading characteristics and pressure level on the difference between the moduli measured statically and dynamically were discussed. The relationship between the small strain and strength properties of undisturbed gravelly soils was evaluated. The small strain properties of air-dried dense Toyoura sand in large-scale triaxial compression tests were also investigated in this study to compare the results of undisturbed gravelly soils.

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Keywords: Strength and deformation characteristics; Small strain stiffness; Static and dynamic measurements; Undisturbed gravelly soil; Triaxial compression; IGC: D6; D7

1. Introduction

The strength and deformation characteristics of gravelly soils (denoted as GSs) have been studied for about half a century in order to investigate their use in the large-scale structures such as rockfill dams and embankments (e.g., Holtz and Gibbs, 1956; Jiang et al., 1997; Okuyama et al., 2003). These experimental studies were mainly conducted under reconstituted conditions; however, the number of studies on undisturbed gravelly soils (UGSs) is limited due to technical problems in sampling methods for in-situ samples with cobbles and boulders. If the conventional sampling methods for

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| Nomenclature | | | |
|--------------------------|---|---------------------|---|
| a | parameter on inherent anisotropy | m' | parameter presenting stress-state dependency of shear modulus |
| c | cohesion | m_d' | m' by dynamic measurement |
| d | specimen diameter | m_s' | m' based on static measurement |
| D | partical diameter | p' | effective mean stress $= (\sigma'_v + 2\sigma'_h)/3$ |
| D_{50} | mean particle diameter | q | deviator stress |
| D_{max} | maximum particle diameter | q_{max} | maximum deviator stress |
| D_{r0} | initial relative density | R | effective principal stress ratio $= \sigma'_v/\sigma'_h$ |
| E_{max} | maximum secant Young's modulus | U_c | coefficient of uniformity |
| E_{sec} | secant Young's modulus | $V_{s(dynamic)}$ | shear wave velocity by dynamic measurement |
| E_{tan} | tangential Young's modulus | $V_{s(static)}$ | equivalent shear wave velocity converted from G_{vhs} |
| E_{v0} | reference vertical Young's modulus at a reference stress state | Δt_{peak} | peak-to-peak travel time |
| E_{vs} | quasi-elastic vertical Young's modulus by static measurement | Δt_{rise} | rise-to-rise travel time |
| FC | finest content | $\Delta \epsilon_v$ | vertical strain increment |
| G_{vh0} | reference shear modulus at a reference stress state | σ'_3 | effective minor principal stress |
| G_{vhd} | shear modulus by dynamic measurement | σ'_h | effective horizontal principal stress |
| G_{vhs} | shear modulus converted from E_{vs} | σ'_v | effective vertical principal stress |
| $(G_{vhd}/G_{vhs})_{50}$ | G_{vhd}/G_{vhs} at isotropic stress state of $\sigma'_v = \sigma'_h = 50$ kPa | $\dot{\sigma}'_v$ | effective vertical principal stress rate |
| h | specimen height | ϵ_h | horizontal strain |
| L | distance between the sampling location and the borehole where in-situ PS logging test was conducted | ϵ_v | vertical strain |
| m | parameter presenting stress-state dependency of E_{vs} | ϵ_{vol} | volumetric strain |
| | | $\dot{\epsilon}_v$ | vertical strain rate |
| | | ϕ | internal friction angle |
| | | λ | wave length in dynamic measurement |
| | | ν_0 | Poisson's ratio at isotropic stress state |
| | | ρ_d | initial dry density of specimen |
| | | ρ_t | wet density of specimen |

relatively finer geomaterials are used for GSs, positions of large particles may be moved largely during the coring process. Some studies using UGSs retrieved by the in-situ freezing method developed to provide temporary particle bonding were conducted (e.g., Nishio and Tamaoki, 1988; Goto et al., 1992; Yasuda et al., 1994; Tanaka et al., 2000). However, this sampling method is in general costly, in particular with large diameter samples, and also may not be applicable if fine particles are included. In view of the above, by taking advantage of a newly developed sampling method using thick water-soluble polymer solutions (Tani et al., 2007), UGSs were retrieved from three tunnel excavation sites in Toyama prefecture, Japan.

Soil characteristics at a small strain level are important in order to predict the overall deformation behaviour and have been studied by many researchers (e.g., Jardine and Potts, 1988; Tatsuoka and Shibuya, 1992; Kohata et al., 1997; Fioravante, 2000; AnhDan et al., 2002). The methods to evaluate small strain properties experimentally are divided into static and dynamic ones. The soil behaviour observed by applying many small unload/reload cycles of axial stress statically in the laboratory tests is essentially linear and nearly recoverable within a very small strain range lesser than 0.001% (Tatsuoka and Shibuya, 1992). For this static measurement, the experimental devices have to be very precise and accurate. On the other hand, the main method to evaluate small strain stiffness dynamically in the laboratory is the use of bender element (e.g., Brignoli et al., 1996; Fioravante, 2000; Leong et al.,

2005). However, in this method, the disturbance induced by inserting the plates into soil specimens as well as the effects of bedding error have a negative influence on the accurate evaluation of small strain properties (Wicaksono et al., 2008). In addition, this method may not be applicable to GSs with large particles due to its limited capacity of excitation and insufficient contact between the plates and coarse soil particles. In view of the above, the precise equipment for measurements of axial loading and deformation (e.g., Tatsuoka and Shibuya, 1992; AnhDan et al., 2002) and a new technique originally developed by AnhDan et al. (2002) were used for static and dynamic measurements, respectively.

In order to evaluate the strength and deformation characteristics and small strain properties of UGSs mentioned above, a series of medium-scale and large-scale triaxial and unconfined compression (TC and UC, respectively) tests with static and dynamic measurements was conducted. Small strain properties of air-dried dense Toyoura sand in large-scale TC tests were also investigated to compare with those of UGSs.

2. Tested materials and their sampling

The tested UGSs were retrieved from construction sites of Makurano, First Uozu and Second Uozu Tunnels (MT, FUT and SUT, respectively) for Hokuriku bullet train, in Toyama prefecture, Japan.

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