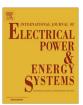
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Utility integration of PV-wind-fuel cell hybrid distributed generation systems under variable load demands



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ABSTRACT

This paper presents modeling, control and performance of a DC micro-grid connected to the utility under variable load demand and different environmental conditions. This micro-grid consists of 60 kW wind turbine (WT) energy conversion system, 40 kW photovoltaic (PV) panel and 40 kW fuel cell (FC) module, in addition to, DC and AC loads. The WT energy conversion system is controlled by the indirect field orientation control (FOC) method to extract maximum power from the wind. The PV module is controlled to generate the available maximum power using P&O MPPT control considering environmental conditions. The fuel cell, with a current controlled DC/DC boost converter, supplies power only when the load demand exceeds the total power of the WT and PV systems. A bidirectional 6-pulse PWM converter connects the micro-grid to utility using the natural frame control (NFC) technique. It controls the DC bus voltage, power and reactive power transfer to/from the utility according to the available power from the DG units and the total load demand. The various control algorithms are presented to harness the maximum power from the renewable energy sources at different operating modes. In addition, voltage stability and smooth power transfer between the micro-grid and utility are maintained.

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1. Introduction

Electrical power systems are being more stressed due to the increase in the power demand, limitation on power delivery capability of the grid, complications in building new transmission – distribution infrastructures and finally all these may lead to blackouts. Distributed Generation (DG) technology have been gaining interest due to its benefits such as high reliability, high power quality, efficiency, reduced emissions, security, and load management [1,2]. Development of power electronic converters along with its high-performance controllers makes it possible to integrate different types of DGs to the utility.

The majority of DG units are interfaced to the utility via DC/AC inverter systems. However, the uncontrolled use of individual DG can cause various problems thereby compromising their benefits [3,4]. These problems include difficulties in connecting these units directly to the AC system due to their variable and intermittent power generation, voltage oscillation and protection issues. Connecting the renewable energy resources to a common DC bus provides several advantages as higher efficiency and reliability, absence of frequency and phase control requirements, when

* Tel.: +20 97 466 1406. E-mail address: ahmadeid@ieee.org compared to the AC micro-grid [5]. Moreover, it has low losses, low cost, the possibility to operate across long distances, and it does not use transformers, in turn leading to volume and cost reduction [2].

Grid-connected three-phase inverters are well documented in literature [6–9] to connect the DGs to the utility grid. The current-controlled voltage source inverter is normally used to control the active and reactive power flow of the micro-grid. The controllers are implemented in synchronously rotating reference frame using proportional-integral (PI) controller or stationary reference frame using proportional-resonant (PR) controller or in Natural Frame Control (NFC) or sometimes called a–b–c frame using hysteresis or deadbeat controllers. A predictive controller-based current control scheme implemented in synchronously rotating reference frame is proposed in [10]. Predictive controller is also proposed in [11] for balanced grid-connected active filter application.

These advantages of simplicity, low cost, ruggedness, high efficiency make the SCIG very attractive for wind power applications both for fixed and variable speed operation [12,13]. Different control methods such as direct/indirect Field-Oriented Control (FOC) and direct torque are used for controlling the converter of the induction machine. The FOC method [14–16] has the ability to control the frequency, amplitude and phase of the motor drive

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Α	swept area of turbine rotor (m²)	P_{wt}	turbine output power (W)
A_{i}	ideality factor	q	electron charge (C)
$C_{\rm p}$	power coefficient	$Q_{\rm i}$	inverter reactive power (Var)
$E_{ m g}$	band energy gap (eV)	$Q_{ m L}$	AC load reactive power (Var)
$E_{\rm nst}$	Nernst voltage (V)	$Q_{\rm t}$	AC side reactive power of micro-grid (Var)
F	Faraday constant (9.648e4C/mol)	$Q_{\rm u}$	utility reactive power (Var)
Gr	gear ratio	R	ideal gas constant (8.314 J/K mol)
$i_{\rm ai},i_{\rm bi},i_{\rm ci}$	inverter output currents (A)	$R_{ m r}$	rotor resistance (Ω)
I_{au}	utility phase current (A)	$r_{ m s}$	PV internal series resistance (Ω)
i_{c}	FC current density (A/m ²)	$R_{\rm s}$	stator resistance (Ω)
i_c	inverter <i>d</i> -axis line current (A)	$r_{ m sh}$	PV internal shunt resistance (Ω)
$i_{ m dr}$	rotor <i>d</i> -axis current (A)	R_{t}	rotor radius of wind turbine (m)
ds	stator <i>d</i> -axis current (A)	S	reference solar irradiance (W/m²)
m	FC maximum current density (A/m ²)	T	cell absolute temperature (K)
i _n	FC internal current density (A/m ²)	$T_{ m em}$	electromagnetic torque (N m)
i _o	FC exchange current density (A/m ²)	$T_{\rm r}$	reference temperature (K)
$I_{ m ph}$	photon-current of PV (A)	v_{act}	FC activation loss voltage (V)
I_{pv}	rated output current of PV (V)	$v_{\rm ai}, v_{\rm bi},$	
$i_{ m qi}$	inverter <i>q</i> -axis line current (A)	· ali · Dli	inverter AC output voltages (V)
$i_{ m qr}$	rotor q -axis current (A)	V_{au}	utility phase voltage (V)
$i_{ m qs}$	stator q -axis current (A)	$V_{\rm c}$	FC terminal voltage (V)
$I_{ m rr}$	rated saturation current (A)	$v_{ m con}$	FC concentration loss voltage (V)
I _{sat}	reverse saturation current (A)	$V_{\rm dc}$	DC bus voltage (V)
I _{sat}	PV rated short circuit current (A)	$v_{ m di}$	inverter d-axis voltage (V)
J _m	moment of inertia (kg m ²)		rotor d-axis voltage (V)
lm k	Boltzmann constant (1.38e–23 m ² kg/s ² K)	$v_{ m dr}$	stator d-axis voltage (V)
$k_{\rm i}$	temperature coefficient of I_{SC}	$v_{ m ds} \ V_{ m oc}$	PV rated open-circuit voltage (V)
$k_{\rm t}$	torque constant		FC ohmic loss voltage (V)
	rotor leakage inductance (H)	$v_{ m ohm}$	rated output voltage of PV (V)
L _{lr}	stator leakage inductance (H)	$V_{ m pv}$	inverter q-axis voltage (V)
L_{ls}		$v_{ m qi}$	
L _m	magnetizing inductance (H)	$v_{ m qr}$	rotor q-axis voltage (V)
m n	fitting constant (8e - 3 cm ² /m ⁴)	$v_{ m qs}$	stator q-axis voltage (V)
n n	fitting constant (8e–3 cm²/mA)	$V_{\rm w}$	wind speed (m/s)
$n_{ m p}$	parallel PV modules	$w_{\rm g}$	generator synchronous speed (rpm)
n _s	series connected cells in PV module	α	charge transfer coefficient
N _t	rated turbine speed (rpm)	ho	air density (kg/m³)
P ~	pole pairs	λ	tip-speed ratio
p D	differential operator	β	pitch angle (°)
P_{AC}	AC load power (W)	ω	rotor speed (rad/s)
$P_{\rm DC}$	DC load power (W)	$\lambda_{\mathbf{dr}}$	rotor d-axis flux linkage (Wb)
fc	FC output power (W)	$\lambda_{\mathbf{ds}}$	stator d-axis flux linkage (Wb)
P _{H2}	hydrogen pressure (bar)	$ heta_{\mathbf{f}}$	rotor flux angle (rad)
Н2О	water pressure (bar)	λ_{opt}	optimum tip speed ratio
P _i	inverter output power (W)	$\lambda_{\mathbf{qr}}$	rotor q-axis flux linkage (Wb)
$P_{\rm m}$	wind turbine mechanical power (W)	$\lambda_{\mathbf{q}\mathbf{s}}$	stator q-axis flux linkage (Wb)
02	oxygen pressure (bar)	ω_{r}	rotor mechanical reference speed (rad/s)
P_{PV}	PV output power (W)	$ au_{ m r}$	rotor time constant (H/Ω)
$P_{\rm u}$	utility output power (W)	$\omega_{ m sl}$	slip frequency speed (rpm)
P_{w}	WECS output power (W)		

voltage. The key to field oriented control is to control the rotor flux vector and the rotor current. In this case, the stator currents of the SCIG are separated into flux and torque producing components by utilizing transformation to the d-q coordinate system. The maximum power point tracking (MPPT) technique is usually an essential part of photovoltaic or wind power generation systems to capture the available maximum power from the sun or wind, respectively.

In most of the published papers, the main problematic issue in micro-grids is the coordination control between the different distributed generations and the utility where one or two of DG units are typically studied. The contributions of this work can be summarized in the following points: (1) The coordination control

between three different sources; wind turbine, photovoltaic and fuel cell. Both the renewable energy resources are operated at MPPT, while, the fuel cell is used to supply the shortage of power amount exceeding the total output power from renewable sources needed by AC and DC loads. (2) The control of grid-side converter is bidirectional to facilitate the flow of power from the micro-grid to utility and vice versa instead of one way operation as indicated in [5]. The ability and fast response of grid-side converter to control both the active and reactive power and hence, operations of lead/lag/unity PF are possible. (3) Simplicity of abc control coupled with hysteresis band implementation provides a harmonic-free three-phase output voltages from the grid-side converter to feed the AC load.

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