



# Microkinetic analysis of CH<sub>4</sub> CPO tests with CO<sub>2</sub>-diluted feed streams

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## ABSTRACT

Autothermal CH<sub>4</sub> catalytic partial oxidation (CPO) tests were performed in an adiabatic lab-scale reformer over 2 wt% Rh/α-Al<sub>2</sub>O<sub>3</sub> catalysts supported on 600 cpsi cordierite honeycombs. The effect of adding either CO<sub>2</sub> or N<sub>2</sub> to CH<sub>4</sub>/air mixtures was investigated at constant O<sub>2</sub>/CH<sub>4</sub> ratio (0.56) and total flow rate (10 Nl/min). At increasing dilution the conversion of CH<sub>4</sub> and the gas temperatures decreased. Also, at equal CH<sub>4</sub> concentration, the addition of CO<sub>2</sub> decreased the temperatures and the conversion of CH<sub>4</sub> more importantly than N<sub>2</sub>. Thus, in line with previous studies from this and other laboratories, no evidence of a direct dry reforming route was found; the observed thermal behavior appeared largely controlled by the heat capacity of the feed streams. However an important chemical effect of CO<sub>2</sub> addition, not previously appreciated in the literature, was shown by the evolution of the outlet H<sub>2</sub>/CO ratio; at increasing N<sub>2</sub> dilution, the H<sub>2</sub>/CO ratio slightly increased from about 2 to 2.5, but at increasing CO<sub>2</sub> dilution, the H<sub>2</sub>/CO ratio decreased from about 1.7 to 0.7. These trends are in line with the thermodynamics of the reverse water gas shift (RWGS) reaction; such a reaction was thus extremely fast in all the experiments with CO<sub>2</sub>, even at the highest values of dilution, while CH<sub>4</sub> conversion did not reach the equilibrium.

A C<sub>1</sub> microkinetic model was used to analyze the results. A close match between calculated and measured temperatures, conversions and syngas composition was obtained under all conditions. Notably, the present microkinetic scheme, which incorporates steps for CO<sub>2</sub> adsorption and reactivity, was able to account for the observed net consumption of CO<sub>2</sub> and for the lowering of the H<sub>2</sub>/CO ratio in the experiments with CO<sub>2</sub> co-feed. Surface coverages were analyzed for the various investigated conditions and the effects on the kinetics of methane steam reforming were evaluated in detail; the factors which control the onset of a more kinetically controlled regime at high degrees of dilution were highlighted.

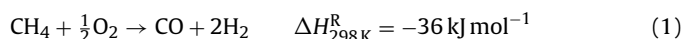
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## 1. Introduction

Global climate changes and the need to reduce greenhouse gas emissions and pollution have stimulated growing interest towards alternative and clean fuels, together with the development of highly efficient and environmentally friendly energy systems. In this respect, syngas offers several opportunities for enhancing the performances of both traditional combustion processes and novel energy systems, such as fuel cells. However, these new applications ask, at least for the short-term period, for small-scale devices and thermal efficient syngas production from natural gas. As a consequence, the traditional steam reforming on Ni-based catalysts, which is an energy-intensive endothermic process, cannot be readily scaled down and alternatives are required.

In light of this, the catalytic partial oxidation (CPO) of methane (1) over Rh or Pt supported catalysts is a promising solution for

novel, small-scale applications of syngas [1].



The CPO reaction is mildly exothermic and can be carried out under autothermal conditions at very short contact times (10<sup>−2</sup> to 10<sup>−4</sup> s) with almost complete selectivity to H<sub>2</sub> and CO [2] even with the use of air; these features allow for the development of compact and simple reformers for on-board applications [3]. Such a high selectivity to syngas can be maintained also at high pressures, thus allowing for an easier integration with downstream pressurized equipment [4–7]. In the field of power generation, interest has recently grown in the conduction of CH<sub>4</sub> CPO in catalytic burners under ultra-diluted, O<sub>2</sub>-lean conditions [8,9]: CH<sub>4</sub> and O<sub>2</sub> react in the presence of large amounts of H<sub>2</sub>O and CO<sub>2</sub> recycled from exhaust streams, consequently avoiding NO<sub>x</sub> production and moderating temperature gradients. Similar recycle may also take place in solid oxide fuel cells with direct internal reforming, where CPO can be exploited for the start-up and sustained in the presence of CO<sub>2</sub> and H<sub>2</sub>O during low-power operations [10]. In general, the possibility of feeding H<sub>2</sub>O and CO<sub>2</sub> to CPO reformers is

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extremely attractive, since it allows for modulating the balance between exothermic oxidation and endothermic steam and CO<sub>2</sub>-reforming, as well as tuning the H<sub>2</sub>/CO ratio of the syngas produced [11].

With respect to these applications, it is of interest to investigate the effect of CO<sub>2</sub> on CPO. In the literature, various research groups have addressed the role of CO<sub>2</sub> in the kinetic scheme of CH<sub>4</sub> partial oxidation on Rh in short contact time reactors. Most of the published works are experimental, and pieces of evidence were collected at various scales of investigation, ranging from isothermal microreactors to autothermal reactors. Numerical analyses have been reported to much less extent. Several authors agree that CO<sub>2</sub>-reforming does not partake in the reaction mechanism [7,12–15]: it is commonly assumed that the rate of CH<sub>4</sub> consumption by CO<sub>2</sub>-reforming is much slower than that of oxidative reforming and steam reforming, and therefore it does not occur in the presence of either H<sub>2</sub>O or O<sub>2</sub>. By means of spatially resolved temperature and composition profiles collected over Rh and Pt foam catalysts, Schmidt and co-workers [13] showed that CO<sub>2</sub> is produced in the presence of O<sub>2</sub>, while it keeps unaltered when O<sub>2</sub> is depleted and CH<sub>4</sub> is being consumed at the expenses of H<sub>2</sub>O. In a dedicated work on the effects of CO<sub>2</sub> and H<sub>2</sub>O, the same group [14] provided direct evidence on the absence of CO<sub>2</sub>-reforming in CH<sub>4</sub> CPO. It was concluded that H<sub>2</sub>O is the preferential co-reactant of CH<sub>4</sub> even in the presence of large amounts of CO<sub>2</sub>. Hence, CO<sub>2</sub> has no kinetic effect on the rate of CH<sub>4</sub> consumption, but only affects the distribution of the products by unbalancing the water gas shift equilibrium.

Mantzaras and co-workers [7,9,16–18] have also performed extensive work on the characterization of the steady state performance and the ignition/extinction dynamics of CH<sub>4</sub>–O<sub>2</sub> reformers with EGR (exhaust gas recycle). Together with a wide experimental investigation, this group has, to our knowledge, first addressed the numerical analysis of the adiabatic reactor operating with large amounts of H<sub>2</sub>O and CO<sub>2</sub>. A single-channel, 2D model of the reactor was developed; the model incorporated both the detailed description of the gas-phase chemistry from Warnatz et al. [19] and the detailed catalytic scheme of Deutschmann and co-workers [20]. The adequacy of such scheme in reproducing the measured methane conversion and syngas yields in CPO of CH<sub>4</sub>/air mixtures had been previously shown by the same authors [8]. In order to evaluate the impact of H<sub>2</sub>O and CO<sub>2</sub> on the production of synthesis gas, Mantzaras and co-workers developed a numerical methodology which consists of simulating the presence of a fictitious species H<sub>2</sub>O\* or CO<sub>2</sub>\* that had the same thermodynamic and transport properties as H<sub>2</sub>O and CO<sub>2</sub> but did not participate in any reaction. From this analysis, the authors concluded that while H<sub>2</sub>O had a direct impact on CH<sub>4</sub> conversion and syngas composition, CO<sub>2</sub> had neither one of the two chemical effects. This means that a specific contribution from the reverse water gas shift (RWGS) reaction was not taken into account.

However, experiments with single co-feed of CO<sub>2</sub> were not performed; all data were obtained only by diluting CH<sub>4</sub> and O<sub>2</sub> with H<sub>2</sub>O/CO<sub>2</sub> mixtures with a 2/1 ratio, thus largely favoring the water gas shift (WGS) thermodynamic driving force. On the other hand we do expect that CO<sub>2</sub> and RWGS may play a role in the CPO process when the exhaust gas recycle has a different composition, such as in the case of the exhaust mixture from an diesel engine where the H<sub>2</sub>O/CO<sub>2</sub> ratio is close to 1 [3]. Thus, in our opinion, neither the experimental work, nor the numerical analysis (which did not account for a significant readsorption of CO<sub>2</sub>) from previous works is conclusive about the role of CO<sub>2</sub> recycle in syngas catalysis.

The key role of the RWGS reaction has been shown in the literature. A number of kinetic studies performed over noble metal catalysts showed that a close similarity exists between CO<sub>2</sub>-reforming and steam reforming rates, so that CO<sub>2</sub>-reforming would rather proceed via a combination of RWGS and steam reforming

[21–25]. Experimental and theoretical works by different groups concur to suggest that CH<sub>4</sub> reforming is kinetically controlled by methane activation and is insensitive to the co-reactant (CO<sub>2</sub> or H<sub>2</sub>O), and that partial replacement of H<sub>2</sub>O by CO<sub>2</sub> has no relevant effect on the mechanism [24,26]. WGS or the RWGS steps have been often found as equilibrated reactions. Some authors [23,27,28] also observe a moderate inhibiting effect of CO adsorption on CH<sub>4</sub> reforming rate, which becomes relevant in the case of CO<sub>2</sub>-reforming, when CO is present in larger concentration on the metal surface.

In this work, we investigate the effect of CO<sub>2</sub> in CH<sub>4</sub> CPO under autothermal conditions. The experiments were simulated by means of a microkinetic scheme [29] incorporated in the detailed model of the adiabatic reactor [30]. Such scheme has been previously validated by comparison with isothermal kinetic data concerning the behavior of CH<sub>4</sub>/O<sub>2</sub>, CH<sub>4</sub>/H<sub>2</sub>O and CH<sub>4</sub>/CO<sub>2</sub> feed streams [26,31]. In particular, differently from previous kinetic schemes proposed in the literature, this model can describe conditions wherein CO<sub>2</sub> adsorption may have a role.

## 2. Modeling

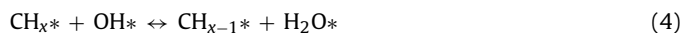
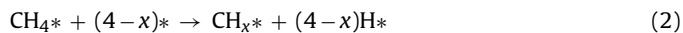
### 2.1. Reactor model

The experiments were analyzed by means of a 1D, heterogeneous, dynamic, fixed bed, single-channel model of the reactor [30,32]. The model consisted of mass, enthalpy and momentum balances for the gas phase and for the solid phase, which included axial convection, solid conduction and gas–solid transport terms. Following the results reported in Refs. [20,33,34], no contribution by homogeneous chemistry was accounted for under the operating conditions adopted. The heat and mass transport properties of the honeycomb monolith were accounted for with specific correlations [35]. Heat conduction in the solid was described with an effective axial thermal conductivity coefficient corrected by the addition of the radiative contribution according to the correlation of Lee and Aris [36]. Radiative dispersion effects at the back and front heat shield were also introduced in the boundary conditions.

### 2.2. Microkinetic heterogeneous scheme

A thermodynamically consistent C<sub>1</sub> microkinetic model for the conversion of CH<sub>4</sub> to syngas [29] was incorporated in the reactor model. The scheme consists of 82 elementary reactions and 13 surface species; it is able to predict mechanistic details of steam reforming, CO<sub>2</sub>-reforming and CH<sub>4</sub> CPO over Rh catalysts [27,37] in full agreement with independent experimental studies (e.g. [24]).

In the scheme, the activation of the CH<sub>4</sub> molecule is assumed to occur via pyrolysis (2), leading to the production of C\* species and CH<sub>x</sub>\* fragments [22,24,25,38]. Additionally, due to lower energy barriers compared to O-assisted processes [39,40], the OH\* species results the favorite co-reactant of C\* and CH<sub>x</sub>\* ((3) and (4)) instead of O\* adatoms. This applies also to the case of CH<sub>4</sub>/CO<sub>2</sub> feed streams that is for the CO<sub>2</sub>-reforming process.



The similarity between steam reforming and CO<sub>2</sub>-reforming is established by considering that both reactions occur via a mechanism wherein OH\* is the main oxidizing species: in steam reforming, OH\* comes from the quasi equilibrated dissociation of H<sub>2</sub>O, while in CO<sub>2</sub>-reforming OH\* is produced via activation of CO<sub>2</sub> [27]. Overall, experimental and modeling results [27,31] indicate

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