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# Particle transport in a small square enclosure in laminar natural convection

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#### ABSTRACT

The transport of particles with diameters in the range of  $50\,\mathrm{nm}$  to  $1\,\mu\mathrm{m}$  in laminar free convection of air in square enclosures was numerically investigated by an Eulerian–Lagrangian method. Two-dimensional square enclosures with widths from  $2.5\,\mathrm{mm}$  to  $5\,\mathrm{cm}$ , with two adiabatic surfaces and  $100\,\mathrm{and}\,200\,^\circ\mathrm{C}$  temperature difference between the other two surfaces, were considered. The Rayleigh numbers varied from  $100\,\mathrm{to}\,8\times10^5$ . The air flow was simulated in Eulerian frame using a commercial CFD software, whose predictions were compared with published benchmark results. Lagrangian particle transport calculations were carried out by tracking  $1000\,\mathrm{particles}$  that were initially randomly distributed in the flow field, and assuming one-way coupling between the particles and the carrier gas. Particle motion mechanisms considered included gravity, drag, lift force, thermophoresis and Brownian dispersion.

The results showed that at Rayleigh numbers lower than about 10 000 the entire flow field was dominated by a single recirculation pattern. For these low Rayleigh number cases most of the particles disperse towards the walls, while a fraction of particles were trapped in a quasi-steady recirculation zone. Inside this recirculation zone the particles were at quasi-equilibrium with respect to the hydrodynamic and dispersive forces that acted on them, and left the zone due to Brownian dispersion only at a very low rate. This quasi-equilibrium zone was not observed at the higher Rayleigh numbers where a single recirculation pattern no longer governed the entire flow field. The results also confirmed the important role of thermophoresis and Brownian dispersion, in particular for submicron size particles.

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#### 1. Introduction

The transport of solid particles and liquid droplets in a fluid has long been a subject of great interest. Understanding, measuring, and quantifying the deposition of aerosol on walls is important in various sectors of science and technology. Some examples are the deposition of drugs and harmful substances in the nasal and respiratory tracts in medical science and engineering; deposition of particles and droplets in gas and steam turbines in power plant engineering; the atmospheric dispersal of pollutants and the determination of indoor air quality in environmental science; the transport and sedimentation of various substances in rivers in civil engineering; fouling of process and heat transfer equipments in process industries; and the transport of chemical aerosols in chemical process engineering.

Natural convection heat transfer is importance in many engineering applications, such as solar collectors, environmental engineering and electronic packaging. Considerable attention has been given to the study of natural convection in enclosures that are heated either externally or by internal energy sources. Natural convection induced by external heating is of importance in the

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Nomenclature
Α
           Constant used in Eq. (12)
В
           Constant used in Eq. (13)
C
           Cunningham's factor
C_T
           thermophoretic coefficient
           Stokes-Cunningham drag coefficient
F_{R}
           Brownian force (N)
F_{TP}
           thermophoresis force (N)
           gravity m/s<sup>2</sup>
g
G_i
           Gaussian random numbers
Κ
           Boltzmann constant (J/K)
K_f
           fluid thermal conductivity (W/m K)
Κ̈́p
           particle thermal conductivity (W/m K)
К'n
           Knudsen number
           shear induced lift force (N)
L
           characteristic length of enclosure (m)—width is used here
L_c
M_G
           molecular mass of gas (kg Kmol)
R
           universal gas constant ([Kmol K)
Ra
           Rayleigh number (=g\beta(T_h - T_c)W^3/(v\alpha))
St
           Stokes number (=(\rho_P C d_p^2 U_0)/(18\mu L_c))
Т
           fluid temperature (K)
           local gas velocity (m/s)
Ug
u_P
           velocity of particle (m/s)
\vec{U}_P
           particle velocity (m/s)
\vec{U}_G
           gas velocity at particle's location (m/s)
\vec{U}_0
           gas velocity far away from the wall (m/s)
           volume (m<sup>3</sup>)
           position of particle
х
Greek symbols
β
           thermal expansion coefficient (1/K)
           gradient
Δ
           dynamic viscosity (kg/ms)
μ
           kinematic viscosity (m<sup>2</sup>/s)
ν
           gas density (kg/m<sup>3</sup>)
\rho_G
           particle density (kg/m<sup>3</sup>)
\rho_P
Subscripts
В
           Brownian
С
           cold
G
           gas
h
           hot
           vector axis indicators
i
P
           particle
TP
           thermophoresis
           axis indicators
x, y
Superscripts
t + \Delta t
           time step
```

estimation of heat loss from solar collectors (Buchberg, Catton, & Edwards, 1976) and across double-paned windows (Korpela, Lee, & Drummond, 1982), in the design of energy efficient buildings, and in many other applications. Natural convection driven by volumetric energy sources is of importance for post-accidental heat removal in nuclear reactors (Baker, Faw, & Kulacki, 1976), and geophysical problems associated with the underground storage of nuclear water (Mckenzie, Roberts, & Weiss, 1974).

A comprehensive review of numerical methods for natural convection in rectangular cavities was presented by de Vahl Davis (1986). His results are used as the bench-mark solutions for natural convection in externally heated enclosures. Among more recent investigations, Wang, Mujumdar, and Yap (2006) numerically studied free convective heat transfer for three different nanofluids contained in horizontal and vertical cavities. Their results indicate that considerable heat transfer enhancement is possible with nanofluids. Nanofluids, due to enhanced heat transfer capacity as compared to traditional fluids, provide

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