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Linear and angular momentum conservation in hydraulic jump in diverging channels

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ABSTRACT

This paper addresses the integral conservation of linear and angular momentum in the steady hydraulic jump in a linearly diverging channel.

The flow is considered to be divided into a mainstream that conveys the total liquid discharge, and a roller where no average mass transport occurs. It is assumed that no macroscopic rheological relationship holds, so mass, momentum and angular momentum integral balances are independent relationships. Normal stresses are assumed to be hydrostatic on vertical, cylindrical surfaces. Viscous stresses are assumed to be negligible with respect to turbulent stresses. Assuming that the horizontal velocity distribution in the mainstream is uniform and that the horizontal momentum and angular momentum in the roller are negligible with respect to their mainstream counterparts, an analytical solution is obtained for the free surface profile of the flow. This solution is fundamental for finding the sequent depths and their positions. Consequently, it permits solving for the length of the jump, which is assumed to be equal to the length of the roller. Mainstream and roller thicknesses can also be derived from the present solution. This model may also be theoretically used to derive the average shear stresses exerted by the roller on the mainstream and the power losses per unit weight. This second relationship, which returns the well-known classical expression for total power loss in the jump, demonstrates that the strongly idealized mechanical model proposed here is internally consistent.

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1. Introduction

The importance of the hydraulic jump for environmental hydraulics and hydraulic engineering is well known. This phenomenon is highly relevant in both fluid mechanics and classical hydraulics. From the point of view of mathematical analysis of shallow water equations, a hydraulic jump represents a singularity that breaks the solution continuity and completely changes the role of the boundary conditions. If a jump occurs, both upstream and downstream boundary conditions influence water elevation [1].

This work addresses a classical problem in applied hydraulics. It is inspired by the work of the first author [2], who identified the problem of unbalanced angular momentum in the hydraulic jump for wide rectangular channels. In several applications, a diverging channel is used to force the jump in shorter lengths and to increase control over the position of the jump.

Many works in the available literature concern small-scale problems that are dominated by viscosity and surface tension

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(see, for example [3], and the reference therein). In contrast, this paper focuses on fully developed turbulent flow over a smooth bottom with negligible surface tension and viscosity effects. The studied case has important applications for large-scale hydraulic engineering because it pertains to the radial flow in stilling basins more than the small jump created in the laboratory.

Basic theoretical and experimental analyses of the hydraulic jump are based on the fundamental studies by Bakhmeteff and Matzke [4] and Rouse et al. [5]. Recent work has incorporated modern flow visualization and laser Doppler anemometry techniques [6–8]. A more extensive review can be found in [2].

From a large-scale point of view, it is worth noting that a huge amount of scientific literature has been recently published concerning one- or two-dimensional numerical schemes for simulating steady jump and moving bore propagation (i.e., [9–11]). Nevertheless, it is important to recall that all of these schemes necessarily treated a bore as a step with vanishing length. In fact, the less a numerical method introduces diffusion effects, the more it can be considered a good, high-resolution method.

The present approach provides unique physical insights on the phenomenon and its spatial development despite the fact that an exhaustive treatment of turbulence is completely omitted. This work follows the typical approach of the hydraulic engineering community, in which turbulence effects are averaged over both a

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Nomenclature unit vector. r direction \mathcal{F}_{s} non-dimensional static force in a generic position [0] \mathbf{e}_r unit vector, z direction horizontal force acting on the mainstream from the roll e_{7} F_{RSx} velocity vector [m/s] v non-dimensional constant in Eq. (49) [0] vertical force acting on the mainstream from the roller F_{RSz} a_{χ} typical distance from the origin of the action line of vertical forces [m] non-dimensional force exerted by the lateral walls [0] \mathcal{F}_{I} gravity acceleration [m²/s] non-dimensional total force through a section [0] g \mathcal{F}_t pressure [Pa] Н total(=piezometric + kinetic) head of the flow [m] р non dimensional total force due to the lateral walls [0] pressure exerted on the mainstream by the roller [Pa] \mathcal{I} p_{RS} generic distributed quantity, see Fig. 1 M_R roller momentum flux [N] q radial coordinate [m] mainstream momentum flux [N] M_S vertical momentum crossing the roller [N] critical radius [m] r_c M_{Rz} streamline dividing the mainstream from the roller [m] M_{Sz} vertical momentum crossing the mainstream [N] S dummy variable in Eq. (85) [0] vertical momentum crossing the whole stream [N] t M_{7} radial velocity [m/s] 0 pole for angular momenta v_r vertical velocity [m/s] IJ cross section averaged velocity [m/s] v_z tangential velocity [m/s] Q liquid discharge [m3/s] v_{θ} axial coordinate [m] generic integral quantity, see Fig. 1 χ 0 ν non-dimensional depth [0] R (vertical) reaction force on the mainstream from the upstream non-dimensional depth [0] y_1 bottom [N] downstream non-dimensional depth [0] Т (vertical) total tangential forces on vertical sections [N] y_2 guess value of upstream non-dimensional depth [0] T_R (vertical) total tangential forces on vertical sections of y_{10} guess value of downstream non-dimensional depth [0] the roller [N] y_{20} (vertical) total tangential forces on vertical sections of vertical coordinate [m] T_S the mainstream [N] moment of longitudinal momentum crossing the whole A_{M} W depth [N m] (vertical) mass force on the whole depth [N] moment of longitudinal momentum crossing the roller (vertical) mass force on the roller [N] A_{M_R} W_R [Nm] W_{S} (vertical) mass force on the mainstream [N] moment of longitudinal momentum crossing the main-Y current depth [m] A_{M_S} upstream depth of the jump [m] stream [N m] Y_1 A_{M_z} moment of vertical momentum crossing the whole downstream depth of the jump [m] Y_2 stream [N m] Y_c critical depth [m] V $A_{M_{R_7}}$ moment of vertical momentum crossing the roller [N m] volume of the whole stream inside the jump [m³] V_R volume of the roller inside the jump [m³] moment of vertical momentum crossing the main- $A_{M_{Sz}}$ volume of the mainstream inside the jump [m³] stream [N m] V_S moment of the horizontal forces acting on the mainν non-dimensional volume of the whole stream inside the $A_{F_{RSx}}$ stream by the roller [N m] jump [0] moment of the vertical forces acting on the mainstream non-dimensional volume of the roller inside the jump $A_{F_{RS_7}}$ V_R by the roller [N m] moment of vertical tangential stress on the whole non-dimensional volume of the mainstream inside the A_T \mathcal{V}_{ς} stream [N m] jump [0] half angular amplitude of the channel [0] moment of vertical tangential stress on the roller [N m] A_{T_p} α moment of vertical tangential stress on the mainstream parameter in Eqs. (A.7) and (A.8) [0] $A_{T_{\varsigma}}$ α_1 parameter in Eqs. (A.7) and (A.8) [0] [Nm] α_2 $tan(\beta)$ jump local steepness [0]

moment on the whole stream due to the pressure force A_{II} [Nm]moment on the whole stream due to the pressure force A_{Π_i} by the lateral walls [N m] moment on the roller due to the pressure force by the $A_{\Pi_{LR}}$ lateral walls [N m]

moment on the mainstream due to the pressure force by $A_{\Pi_{LS}}$ the lateral walls [N m]

moment on the roller due to the pressure force [N m] A_{Π_R} moment on the mainstream due to the pressure force A_{Π_S} [Nm]

C constant in Eq. (73)

 C_1 non-dimensional constant in Eq. (83) [0] Е specific energy of the flow [m] E_1 upstream specific energy [m]

downstream specific energy [m] E_2 Fr Froude number of the flow [0] Fr_1 upstream Froude number [0]

 Fr_{20} guess value of downstream Froude number [0] non-dimensional total force of the flow at the upstream \mathcal{F}_1 jump position [0]

 $tan(\beta_1)$ jump local steepness at the upstream section of the jump [0]

momentum coefficient for the mainstream flow [0] β_s specific weight of the fluid [N/m³]

γ χ δ non-dimensional constant in Eq. (19) [0] roller thickness [m]

mainstream thickness [m] η density of the fluid [kg/m³] ρ σ non dimensional roller thickness [0]

vertically averaged tangential stress on vertical sections $\bar{\tau}$

z-component of the local turbulent stress on a cylindri- τ_{rz} cal surface normal to \mathbf{e}_r [Pa]

total tangential stress exerted on the mainstream by the τ_{RS} roller [Pa]

vertically averaged tangential stress on the roller [Pa] $\bar{\tau}_R$ vertically averaged tangential stress on the mainstream $\bar{ au}_{\mathcal{S}}$

[Pa] angular coordinate [0] θ non-dimensional radius [0]

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