

# Parameters that control the cleanup of fractured permeable aquifers

Hillel Rubin <sup>a,\*</sup>, Sharon Yaniv <sup>a</sup>, Martin Spiller <sup>b</sup>, Jürgen Köngeter <sup>b</sup>

<sup>a</sup> Faculty of Civil and Environmental Engineering, Technion, Israel Institute of Technology, Haifa 32000, Israel

<sup>b</sup> Institute of Hydraulic Engineering and Water Resources Management, Aachen University (RWTH Aachen), D-52056 Aachen, Germany

Received 14 September 2004; received in revised form 15 October 2007; accepted 19 October 2007

Available online 13 November 2007

## Abstract

This study develops a modeling approach for simulating and evaluating entrapped light nonaqueous-phase liquid (light NAPL–LNAPL) dissolution and transport of the solute in a fractured permeable aquifer (FPA). The term FPA refers to an aquifer made of porous blocks of high permeability that embed fractures. The fracture network is part of the domain characterized by high permeability and negligible storage. Previous studies show that sandstone aquifers often represent FPAs. The basic model developed in this study is a two-dimensional (2-D) model of permeable blocks that embed oblique equidistant fractures with constant aperture and orientation. According to this model, two major parameters govern NAPL dissolution and transport of the solute. These parameters are: 1) the dimensionless interphase mass transfer coefficient,  $K_{f0}$ , and 2) the mobility number,  $N_{M0}$ . These parameters represent measures of heterogeneity affecting flow, NAPL dissolution, and transport of the solute in the domain. The parameter  $K_{f0}$  refers to the rate at which organic mass is transferred from the NAPL into the water phase. The parameter  $N_{M0}$  represents the ratio of flow through the porous blocks to flow through the fracture network in regions free of entrapped NAPL. It also provides a measure of groundwater flow bypassing regions contaminated by entrapped NAPL. In regions contaminated by entrapped NAPL our simulations have often indicated very low permeability of the porous blocks, enabling a significant increase of the fracture flow at the expense of the permeable block flow. Two types of constitutive relationships also affect the rate of FPA cleanup: 1) the relationship between the saturation of the entrapped NAPL and the permeability of the porous blocks, and 2) the relationships representing effects of the entrapped NAPL saturation and the permeable block flow velocity on rates of interphase mass transfer. This study provides basic tools for evaluating the characteristics of pump-and-treat cleanup of FPAs by referring to sets of parameters and constitutive relationships typical of FPAs. The numerical simulations carried out in this study show that at high initial saturation of the entrapped NAPL, during initial stages of the FPA cleanup the contaminant concentration increases, but later it decreases. This phenomenon originates from significant groundwater bypassing the NAPL entrapped in the permeable blocks via the fracture network.

© 2007 Elsevier B.V. All rights reserved.

**Keywords:** Fractured porous formation; Fractured porous media; Fractured permeable formation (FPF); Fractured permeable aquifer (FPA); Aquifer cleanup; NAPL contamination; Pump-and-treat

## 1. Introduction

This study originates from field observations and laboratory measurements (Rubin and Braester, 2000) performed in a part of the Coastal Plain Aquifer (CPA) in Israel. Entrained kerosene, which is a light nonaqueous-

\* Corresponding author. Tel.: +972 4 829 2306; fax: +972 4 822 898.

E-mail address: [hkrubin@technion.ac.il](mailto:hkrubin@technion.ac.il) (H. Rubin).

## Nomenclature

$B$	distance between adjacent fracture intersections (L)
$C$	normalized solute concentration in the fracture flow
$C_{av}$	normalized flux average solute concentration in the cross-section
$C_b$	normalized solute concentration in the permeable block flow
$C_{nv}$	equilibrium volumetric concentration of solute
$C^*$	solute concentration in the fracture flow ( $ML^{-3}$ )
$C_{av}^*$	flux average solute concentration in the cross-section ( $ML^{-3}$ )
$C_b^*$	solute concentration in the permeable block flow ( $ML^{-3}$ )
$C_s^*$	equilibrium concentration of solute ( $ML^{-3}$ )
$d$	grain diameter (L)
$D$	free liquid diffusivity ( $L^2/T$ )
$i$	number of the vertical grid point
$i_{max}$	total number of vertical grid points
$ibl$	number of the permeable block
$ifr$	number of the fracture segment
$J$	hydraulic gradient
$J_0$	hydraulic gradient in regions free of entrapped NAPL
$j$	number of the longitudinal grid point
$j_a$	number of the grid point for the calculation of $C_{av}$
$j_c$	number of the downstream-end longitudinal grid point
$K_b$	hydraulic conductivity of permeable blocks ( $LT^{-1}$ )
$K_B$	value of $K_b$ at the fracture segment ( $LT^{-1}$ )
$K_{b0}$	value of $K_b$ in regions free of entrapped NAPL ( $LT^{-1}$ )
$K_f$	dimensionless interphase mass transfer coefficient
$K_{f0}$	initial value of $K_f$
$K_t$	average cross-sectional hydraulic conductivity ( $LT^{-1}$ )
$K_{t0}$	value of $K_t$ in regions free of entrapped NAPL ( $LT^{-1}$ )
$k_f$	lumped mass transfer coefficient ( $T^{-1}$ )
$k_{rm}$	relative NAPL permeability
$k_{rt}$	cross-sectional relative water permeability
$k_{rw}$	relative water permeability
$k_{rwB}$	value of $k_{rw}$ at the fracture segment
$k_\alpha$	number of the fracture segment nodal point for calculating $C_{av}$
$m$	number of the time step
$M_f$	mobility of the fracture segment ( $L^2T^{-1}$ )
$N_M$	mobility number
$N_{M0}$	value of $N_M$ in regions free of entrapped NAPL
$n$	power coefficient used for permeability calculations
$n_c$	number of contaminated sections
$n_p$	coefficient for calculating permeability
$Q_b$	rate of permeable block flow ( $L^2T^{-1}$ )
$Q_{b0}$	value of $Q_b$ in regions free of entrapped NAPL ( $L^2T^{-1}$ )
$Q_f$	rate of fracture segment flow ( $L^2T^{-1}$ )
$Q_{f0}$	value of $Q_f$ in regions free of entrapped NAPL ( $L^2T^{-1}$ )
$Q_R$	ratio of $Q_b$ to $Q_f$ in a vertical cross-section
$Q_t$	total flow rate flowing through the subdomain cross-section ( $L^2T^{-1}$ )
$q_b$	specific discharge of the permeable block flow ( $LT^{-1}$ )
$q_B$	value of $q_b$ entering the fracture segment ( $LT^{-1}$ )

Download English Version:

<https://daneshyari.com/en/article/4547542>

Download Persian Version:

<https://daneshyari.com/article/4547542>

[Daneshyari.com](https://daneshyari.com)