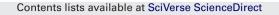
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# Improving the DME steam reforming catalyst by alkaline treatment of the HZSM-5 zeolite

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#### ABSTRACT

Dimethyl ether (DME) steam reforming for hydrogen production has been studied on a bifunctional catalyst prepared by the (wet) physical mixing (at 50 wt%) of a metallic function of CuO–ZnO–Al<sub>2</sub>O<sub>3</sub> (Cu/Zn/Al atomic ratio = 4.5:4.5:1.0, prepared by co-precipitation) and an acidic function of HZSM-5 zeolite modified by alkaline treatments of different severity. The runs have been carried out in a fluidized bed reactor. The results obtained by using treated HZSM-5 zeolites and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> as acid functions have been compared. The alkaline treatment affects both the acid properties of the zeolite (attenuating total acidity and acid strength) and its porous structure (increasing the mesoproous surface and decreasing the microporous volume and BET surface area). The attenuation in acidity hinders the formation of undesired hydrocarbons for 300 min) is suitable for improving the kinetic performance of the bifunctional catalyst, as it provides high selectivity and a high yield of H<sub>2</sub> at 300 °C without hydrocarbon formation, as well as minimizing CO formation and avoiding deactivation by Cu sintering. The catalyst is stable, and its kinetic performance remains constant throughout long runs.

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#### 1. Introduction

Hydrogen is considered a suitable fuel to meet ever-increasing energy demand because it may be produced from renewable sources [1]. Hydrogen fuel cells are presented as an efficient and environmentally friendly power generator applicable to both mobile and stationary use [2]. Although hydrogen has a high fuel density, it is difficult to handle and, therefore, a hydrogen vector (e.g., methanol, ethanol, gasoline, diesel and methane) needs to be used for H<sub>2</sub> production for fuel cell processors by means of reforming processes.

Methanol can be easily and selectively converted into an H<sub>2</sub>-rich gas at low temperature (150–300 °C) by steam reforming [3] and, therefore, it is an excellent raw material for on-board H<sub>2</sub> production for PEM fuel cells. However, the infrastructure for processing methanol is not well developed and methanol toxicity is high. The reforming of dimethyl ether (DME) is an alternative of growing interest [4–11], given that DME is relatively inert, non-corrosive, non-carcinogenic and can be stored and handled as LPG, which means it is more readily used as a fuel and in fuel cells [12]. DME synthesis from syngas in a single step on bifunctional catalysts is thermodynamically more favoured than methanol synthesis and,

moreover,  $CO_2$  can be co-fed together with the syngas [13–15]. Accordingly, Olah et al. [16] consider DME synthesis in a single step as a key process for large-scale  $CO_2$  valorization. Furthermore, DME has also attracted increased attention as a clean fuel.

The main reactions in the process of DME steam catalytic reforming are:

DME steam reforming	$(CH_3)_2O + 3H_2O \leftrightarrow 6H_2 + 2CO_2$	(1)
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DME hydrolysis  $(CH_3)_2O + H_2O \leftrightarrow 2CH_3OH$  (2)

MeOH steam reforming  $CH_3OH + H_2O \leftrightarrow 3H_2 + CO_2$  (3)

r-WGS 
$$CO_2 + H_2 \leftrightarrow H_2O + CO$$
 (4)

DME decomposition  $(CH_3)_2 O \rightarrow CH_4 + H_2 + CO$  (5)

Steam reforming of DME (SRD) (Eq. (1)) consists of two steps in series: DME hydrolysis (Eq. (2)) on an acid function and methanol steam reforming (Eq. (3)) on a metallic function. Apart from SRD, a reverse water-gas shift reaction (r-WGS) (Eq. (4)) usually takes place on the metallic function, and methane is also formed via DME decomposition (Eq. (5)) when a strong acidic function or high temperatures are used [7]. Consequently, suitable metallic and acid functions are required for attaining high DME conversion and high H<sub>2</sub> selectivity by avoiding the formation of CO (poison for the anodic catalyst in PEM fuel cells) and CH<sub>4</sub> as byproducts.

Cu-based catalysts are well known for their high activity for methanol steam reforming and selectivity towards  $H_2$  [17].

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Nomenclature		
A0.2-10	, A0.2-300, A0.4-300 HZ30 zeolites treated with 0.2 M NaOH for 10 min, 0.2 M NaOH for 300 min and 0.4 M NaOH for 300 min, respectively	
ALU	$\gamma$ -Al <sub>2</sub> O <sub>3</sub> acid function	
Br	Brönsted acid sites	
CZA	$CuO-ZnO-Al_2O_3$ metallic function	
CZA/ALU	U, CZA/HZ30, CZA/A0.2-10, CZA/A0.2-300,	
·	CZA/A0.4-300 bifunctional catalysts made up of CuO–ZnO–Al <sub>2</sub> O <sub>3</sub> and different acid functions: ALU, HZ30 zeolite or zeolites treated with alkali	
	(A0.2-10, A0.2-300, A0.4-300), respectively	
$\bar{d}_{Cu}$	average particle size of Cu (Å)	
DME	dimethyl ether	
$d_{\rm pore}$	pore diameter (Å)	
DSC	digital scanning calorimetry	
<i>F</i> <sub><i>i</i></sub> , <i>F</i> <sub><i>i</i>,0</sub>	molar flow rate of <i>i</i> component at the reactor outlet	
,0	and in the feed, respectively	
GHSV	gas hourly space velocity	
HC	hydrocarbons	
HZ30	parent (untreated) HZSM-5 zeolite	
Lw	Lewis acid sites	
MeOH	methanol	
MTG, M	TH, MTO methanol to gasoline, methanol to hydro-	
	carbons and methanol to olefins, respectively	
PEM	polymer electrolyte membrane	
$P_i$	partial pressure of <i>i</i> component (bar)	
r-WGS	reverse water-gas shift reaction	
S <sub>BET</sub>	BET surface area of the solid $(m^2/g)$	
S <sub>external</sub>	external surface area of the solid $(m^2/g)$	
S <sub>metallic</sub>	specific metal surface area $(m^2 Cu/g Cu)$	
Smicropor	micropore surface area $(m^2/g)$	
SRD	steam reforming of dimethyl ether	
TPD	temperature programmed desorption	
TPR	temperature programmed reduction	
V <sub>mesopor</sub>	$(cm^3/g)$	
$X_{\rm DME}$	DME conversion	
$x_i$	<i>i</i> component molar fraction	
X <sub>MeOH</sub>	methanol effective conversion in the second step of	
VDD	the SRD process	
XRD	X-ray diffraction analysis	
XRF	X-ray fluorescence spectroscopy	
$Y_i$	yield of <i>i</i> component	
$v_i$	stoichiometric coefficient of <i>i</i> component	

Accordingly, commercial or laboratory synthesized CuO–ZnO– $Al_2O_3$  metallic functions have been widely used in the bifunctional catalysts for SRD [6,18–22]. Other Cu-based metallic functions studied for SRD include Cu–CeO<sub>2</sub> [23–25] and Cu–Ni [26]. Noble metal based catalysts, such as Pt/Al<sub>2</sub>O<sub>3</sub> or Ru/Al<sub>2</sub>O<sub>3</sub>, give way to a relatively high DME conversion, although a rather high production of CH<sub>4</sub> is obtained [11]. The formation of CH<sub>4</sub> (up to 25%) can be significantly reduced (to 7%) by mixing Pt/Al<sub>2</sub>O<sub>3</sub> catalysts with Pd/Al<sub>2</sub>O<sub>3</sub>, with no loss in hydrogen production activity [27].

The choice of acid function is essential for the development of catalysts for SRD, given that hydrolysis is the process limiting step.  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> is the more commonly used catalyst [4,8–10,18,26,28], but due to its very low acidity, high temperatures (usually in the 300–400 °C range) are required for high DME conversion, with considerable sintering of the Cu metallic function at these temperatures. Spinels have been proposed for improving the stability of Cu metallic functions above 300 °C, and a spinel of CuM<sub>2</sub>O<sub>4</sub>

(M=Fe, Mn, Cr, Ga, Al and others) has greater stability than a commercial CuO–ZnO–Al<sub>2</sub>O<sub>3</sub> metallic function [8–10,28]. It has also been proven that Ni addition attenuates Cu sintering, given that it improves surface dispersion and strengthens the interaction between Cu and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [26].

However, the use of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> as an acid function for SRD has the additional inconvenience of promoting DME decomposition and the r-WGS reaction due to the high temperatures required for DME hydrolysis and, therefore, the formation of significant amounts of CH<sub>4</sub> and CO, which is a handicap for PEM fuel cells, given that CO concentrations lower than 50 ppm are required for avoiding anodic catalyst poisoning [29]. As an alternative to  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, acid functions of higher acidity have been proposed, such as 12-tungstosilicoheteropolyacids (H<sub>4</sub>SiW<sub>12</sub>O<sub>40</sub>) deposited on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [30], WO<sub>3</sub>/ZrO<sub>2</sub> [21,24,25], H-mordenite or HZSM-5 zeolites [5-7,20,22,23,31-33]. HZSM-5 zeolites are much more active for DME hydrolysis and allow obtaining high yields of H<sub>2</sub> at considerably lower temperatures (around 100 °C lower) than those required with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [5,6]. Nevertheless, due to their excessive acidity, they give way to hydrocarbons at temperatures close to 300 °C, which significantly reduces H<sub>2</sub> yield [7,31,32], and significant coking (deactivated catalyst) also occurs on the catalyst surface due to the condensation of the hydrocarbons formed [20]:

 $Oxygenates \rightarrow hydrocarbons \rightarrow coke$ (6)

This paper studies the attenuation of HZSM-5 zeolite acidity by alkaline treatment (with NaOH) and the effect of treatment conditions on the physical-chemical properties of the zeolite. Likewise, the effect of this alkaline treatment is determined on the kinetic performance of: (i) the zeolite in DME hydrolysis (Eq. (2)) and (ii) the bifunctional catalyst (with CuO-ZnO-Al<sub>2</sub>O<sub>3</sub> metallic function) prepared using different treated zeolites in the reforming of DME (Eq. (1)) and methanol (Eq. (3)), and in the formation of undesired byproducts, i.e., CO (Eq. (4)), CH<sub>4</sub> (Eq. (5)) and hydrocarbons (Eq. (6)). The study of coke deposition (second step in the scheme in Eq. (6)) is beyond the scope of this paper.

An alkaline treatment of the HZSM-5 zeolite is efficient for improving the kinetic behaviour and stability of the zeolite by attenuating acidity and mesopore generation. Accordingly, the condensation and coke formation reactions are attenuated in several processes, such as the transformation of methanol into olefins [34], the direct hydroxylation of benzene to phenol [35] and the selective transformation of aqueous ethanol into olefins [36,37].

#### 2. Experimental

#### 2.1. Catalyst synthesis

The bifunctional catalysts have been prepared by the wet physical mixing of CuO–ZnO–Al<sub>2</sub>O<sub>3</sub> metallic function (called CZA, Cu/Zn/Al atomic ratio = 4.5:4.5:1.0), prepared by coprecipitating the corresponding nitrates with Na<sub>2</sub>CO<sub>3</sub> at pH = 7.0 and 70 °C under conditions established in previous papers [38,39] and calcined at 325 °C for 3 h, and different acid functions, namely,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, commercial HZSM-5 zeolite and HZSM-5 zeolites modified by different alkaline treatments. The homogeneous mixtures obtained are centrifuged to separate the solid, which is dried, firstly at ambient temperature for 24 h and then in an oven at 110 °C for another 24 h. The powder obtained is calcined at 325 °C for 3 h and subsequently pressed, ground and sieved to a particle size between 0.15 and 0.25 mm, which is suitable for a fluidized bed reactor. The content of the acid function is 85 wt% for the bifunctional catalyst with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and 50 wt% for the bifunctional catalysts with zeolite.

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