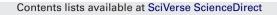
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**Applied Catalysis B: Environmental** 



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# Application of spaciMS to the study of ammonia formation in lean NO<sub>x</sub> trap catalysts

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### ARTICLE INFO

Article history: Received 21 December 2011 Received in revised form 26 April 2012 Accepted 1 May 2012 Available online 10 May 2012

Keywords: SpaciMS Lean NO<sub>x</sub> trap NO<sub>x</sub> adsorber catalyst Storage Reduction Ammonia Aging

## ABSTRACT

SpaciMS was employed to understand the factors influencing the selectivity of NO<sub>x</sub> reduction in two fully formulated LNT catalysts, both degreened and thermally aged. Both catalysts contained Pt, Rh, BaO and Al<sub>2</sub>O<sub>3</sub>, while one of them also contained La-stabilized CeO<sub>2</sub>. The amount of reductant required to fully regenerate each catalyst was first determined experimentally based on the OSC of the catalyst and the  $NO_x$  storage capacity (NSC). In this way a correction was made for the change in catalyst OSC and NSC after aging, thereby eliminating these as factors which could affect catalyst selectivity to NH<sub>3</sub>. For both catalysts, aging resulted in an elongation of the NO<sub>x</sub> storage-reduction (NSR) zone due to a decrease in the concentration of NO<sub>x</sub> storage sites per unit catalyst length. In addition to decreased lean phase  $NO_x$ storage efficiency, stretching of the NSR zone affected catalyst regeneration. Three main effects were identified, the first being an increase of the  $NO_x$  "puff" that appeared during the onset of the rich front as it traversed the catalyst. Spatially,  $NO_x$  release tracked the NSR zone, with the result that the  $NO_x$ concentration peaked closer to the rear of the aged catalysts. Hence the probability that NO<sub>x</sub> could readsorb downstream of the reduction front and subsequently undergo reduction by NH<sub>3</sub> (formed in the reduction front) was diminished, resulting in higher rich phase  $NO_x$  slip. Second, the stretching of the NSR zone resulted in increased selectivity to NH<sub>3</sub> due to the fact that less catalyst (corresponding to the OSC-only zone downstream of the NSR zone) was available to consume NH<sub>3</sub> by either the NH<sub>3</sub>-NO<sub>x</sub> SCR reaction or the NH<sub>3</sub>-O<sub>2</sub> reaction. Third, the loss of OSC and NO<sub>x</sub> storage sites, along with the decreased rate of NO<sub>x</sub> diffusion to Pt/Rh sites (as a result of Pt/Rh–Ba phase segregation), led to an increase in the rate of propagation of the reductant front after aging. This in turn resulted in increased  $H_2$ :NO<sub>x</sub> ratios at the Pt/Rh sites and consequently increased selectivity to NH<sub>3</sub>.

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# 1. Introduction

Recent years have witnessed concerted efforts to reduce  $NO_x$  emissions from mobile sources of lean exhaust gas using lean  $NO_x$  trap (LNT) or selective catalytic reduction (SCR) catalysts. Although both technologies have many positive features, each approach has drawbacks which have slowed their application to the automotive marketplace. For LNT catalysts, one of the main disadvantages is the cost associated with the use of platinum group metals (PGMs), while for SCR, the cost of the injection system and refilling of the NH<sub>3</sub> source adds to the consumer's costs. However, recent studies have shown that by combining LNT and SCR catalysts in series, these drawbacks can be lessened [1–5]. In this configuration the SCR catalyst functions in a passive or in situ mode, i.e., with the storage and utilization of NH<sub>3</sub> generated by the LNT during rich

purge events. Given that the presence of the SCR catalyst relaxes the  $NO_x$  conversion requirements of the LNT catalyst, the volume of the LNT in the LNT–SCR system can, in principle, be lower than for an LNT–only system, thereby reducing the precious metal costs. Furthermore, the need for a urea injection system is eliminated.

To realize a LNT–SCR system capable of achieving these aims, an understanding is required of the interplay between system operating parameters and the underlying chemistry of NO<sub>x</sub> reduction. Probably the most important aspects to be considered are the generation of NH<sub>3</sub> over the LNT, and its subsequent reaction with NO<sub>x</sub> over the SCR catalyst. A potential problem in studying these processes in a LNT–SCR system is the integral nature of the catalysts. Reactants and products can react, adsorb, and desorb multiple times before exiting the system. This makes the study of LNT–SCR systems difficult using traditional laboratory techniques based on analysis of the reactor effluent.

To overcome these problems, spatially resolved capillary inlet mass spectrometry (spaciMS), developed at Oak Ridge National Laboratory, has been applied to monitor the composition of

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simulated exhaust gas as it passes through LNT catalysts [6–14]. The key feature of a spaciMS system is the use of a capillary connected to the sample cell of a mass spectrometer. The capillary allows the internal gas stream to be analyzed at different points along the length of the LNT or SCR catalyst under study. Conse-

along the length of the LNT or SCR catalyst under study. Consequently, the gaseous components present can be monitored on both a spatial and temporal scale. Partridge et al. employed spaciMS to study NH<sub>3</sub> formation and utilization over a Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst during regeneration with H<sub>2</sub> [10]. It was found that NH<sub>3</sub> was formed at the same time as the N<sub>2</sub> product inside the catalyst during regeneration, and was consumed as aggressively as the H<sub>2</sub> reductant along the catalyst. From this it was concluded that the intermediate NH<sub>3</sub> regeneration pathway plays an important role in LNT catalyst regeneration. The same research group also utilized this technique to study the effect of sulfur on the spatiotemporal distribution of  $NO_x$  storage and reduction [11]. Prior to sulfation, NO<sub>x</sub> storage/reduction was found to be localized in the front portion of catalyst, whereas sulfation resulted in a shift of the NO<sub>x</sub> storage/reduction (NSR) zone downstream, thereby decreasing the length of the downstream zone in which only oxygen was stored. These workers also reported an increase in selectivity to NH<sub>3</sub> after sulfation, and ascribed it to decreased oxidation of NH<sub>3</sub> slipping from the NSR zone by the oxygen stored downstream [11,12]. A more recent study by this group further demonstrated that NH<sub>3</sub> slip at the catalyst exit increased with sulfur loading due to its formation closer to the catalyst outlet and decreased NH<sub>3</sub> conversion by stored oxygen downstream of the NSR zone [13]. Moreover, during catalyst regeneration the extent of NO<sub>x</sub> readsorption downstream of the NSR zone was found to diminish after sulfation, resulting in earlier and broader NO<sub>x</sub> peaks at the catalyst outlet. The spaciMS technique was also applied in another recent LNT study by Luo et al. [14] in which catalyst desulfation was examined. For a partially sulfated commercial catalyst, the plug-like sulfur profile was redistributed after desulfation at 600 °C as a result of re-adsorption. The extent of re-adsorption was found to be determined by the catalyst formulation and sulfation degree.

We have previously investigated the effect of regeneration conditions on NH<sub>3</sub> formation in LNT catalysts [15]. One of the findings from these studies was that NH<sub>3</sub> selectivity is dependent on the local H<sub>2</sub>:NO<sub>x</sub> ratio at the precious metal sites. Increasing the regeneration time or reductant concentration fed to the catalyst increases this ratio and thereby increases the amount of NH<sub>3</sub> formed, as opposed to  $N_2$ . Conversely, increasing the amount of  $NO_x$  stored decreases the selectivity to NH<sub>3</sub>. It was also observed that the addition of a ceria-based oxygen storage material to a Pt/Rh/BaO/Al<sub>2</sub>O<sub>3</sub> catalyst caused a decrease in NH<sub>3</sub> selectivity [15–18], which was explained on the basis that consumption of reductant by stored oxygen results in decreased H<sub>2</sub>:NO<sub>x</sub> ratios during regeneration, which favors the formation of N2 over NH3. In addition, oxygen stored in the rear of the catalyst can consume NH<sub>3</sub> formed upstream via oxidation to produce N<sub>2</sub>, NO, or N<sub>2</sub>O. After aging, increased selectivity to NH3 was observed, for both the ceriacontaining and ceria-free catalyst. In principle, this increase in selectivity to NH<sub>3</sub> can be accounted for by any one of a number of factors [15]:

(i) Aging-induced Pt sintering, resulting in Pt–Ba phase segregation. Consequently, the rate of  $NO_x$  transport to the Pt sites during regeneration is decreased. As Harold and co-workers have pointed out [19], if this rate is slower than the H<sub>2</sub> feed rate, then H<sub>2</sub> will break through with substantially more  $NO_x$ remaining on the catalyst. Consequently, the Pt surface will be predominantly covered by hydrogen, and as the stored  $NO_x$ diffuses to the Pt particles, NH<sub>3</sub> will be formed with high selectivity. Modeling studies confirm this idea, i.e., that NH<sub>3</sub> formation is favored when solid-phase diffusion of  $NO_x$  to the Composition of catalysts used in this study

| Component   | Catalyst code/nominal loading |         |
|---|-------------------------------|---------|
|   | B-225                         | BC-175  |
| Pt (g/L)  | 3.05                          | 2.38    |
| Rh (g/L)  | 0.61                          | 0.48    |
| BaO <sup>a</sup> (g/L)                                      | 26                            | 20      |
| $CeO_2^{b}(g/L)$  | 0                             | 67      |
| $\gamma$ -Al <sub>2</sub> O <sub>3</sub> <sup>c</sup> (g/L) | Balance                       | Balance |
| Total washcoat (g/L)  | 225                           | 175     |

<sup>a</sup> 21.5 wt% supported on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>.

<sup>b</sup> Stabilized with 5 wt% La<sub>2</sub>O<sub>3</sub>.

<sup>c</sup> Stabilized with 3 wt% La<sub>2</sub>O<sub>3</sub>.

Pt/Ba interface is the rate determining process, which becomes increasingly likely as the Pt dispersion decreases [20].

- (ii) For a fixed concentration of reductant, the decreased oxygen storage capacity (OSC) of the aged catalysts should result in higher effective  $H_2:NO_x$  ratios in the reduction front due to decreased reductant consumption by stored oxygen, thereby favoring  $NH_3$  formation. Furthermore, there is less oxygen available downstream of the reductant front to react with formed  $NH_3$ .
- (iii) After aging, there are fewer NO<sub>x</sub> storage sites available per unit of catalyst length. This should result in higher effective  $H_2:NO_x$  ratios in the reductant front, again favoring NH<sub>3</sub> formation [15].
- (iv) The length of the  $NO_x$  storage–reduction zone increases due to the decrease in  $NO_x$  storage capacity (NSC) as the catalyst ages [11,12,15]. More  $NH_3$  slips from the LNT without being oxidized because the increased length of the NSR zone decreases the length of the downstream OSC-only zone.
- (v) After aging, higher  $NH_3$  emissions may result from decreases in the rates of  $NH_3$  consumption via reaction with  $NO_x$  or  $O_2$ stored downstream of the reaction front.

From the foregoing, it is evident that  $NH_3$  selectivity after aging is likely to be dependent – at least in part – on the residual OSC of the catalyst, as well as the amount of  $NO_x$  stored. In an effort to distinguish between the factors that can account for increased LNT selectivity to  $NH_3$  after aging, in this study we adjusted the amount of reductant used to regenerate each catalyst (degreened and thermally aged) based on the OSC of the catalyst and the  $NO_x$ storage capacity (NSC). In this way we attempted to correct for the change in catalyst OSC and NSC after aging, thereby eliminating these as factors. SpaciMS was used to monitor the  $NO_x$  storage and reduction processes for degreened and aged catalysts in order to investigate the contribution of other factors to  $NO_x$  reduction selectivity.

#### 2. Experimental

#### 2.1. Catalyst preparation

Two fully formulated Ba-based LNT catalysts were used in this study, the compositions of which are shown in Table 1. For simplicity, the BaO-only formulation is denoted as B-225 (where 225 refers to the washcoat loading in g/L), while the catalyst containing both BaO and CeO<sub>2</sub> is denoted as BC-175 (containing a washcoat loading of 175 g/L). Details of the catalyst preparation have been described elsewhere [16,17]. In both cases, the washcoat was applied to a 4 in. × 6 in. cordierite monolith substrate, possessing a cell density of 400 cpsi and a wall thickness of 6.5 mil. The BaO component (21.5 wt %) was supported on  $\gamma$ -alumina, while bare alumina was also used as a balance to bring the total washcoat loadings to the values indicated in Table 1.

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