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## Reactive rimming flow of non-Newtonian fluids

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#### ABSTRACT

The steady and non-steady flows of a liquid polymer treated as a non-Newtonian fluid on the inner surface of a horizontal rotating cylinder are investigated. Since the Reynolds number is small and the liquid film is thin, a simple lubrication approximation is applied. Governing equations for non-steady Power-Law and Ellis fluids are solved numerically and the time of transition from non-steady to steady-state mode for various model parameters and flow conditions are defined. The stabilization effect of a chemical reaction within the polymeric fluid (reactive flow) is examined.

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#### 1. Introduction

The problem of rotational flow on the inner and/or outer wall of a hollow horizontal cylinder has been of interest for many years due to its wide range of applications in industry [1,2]. Moffatt [3] was the first to derive the condition for the maximal supportable load for a Newtonian liquid. Preziosi and Joseph [4] later presented the same result in another form and named it a run-off condition for coating and rimming flows.

The possible instability of the liquid film on a cylindrical surface is one the most challenging aspects of this problem. The highly unstable nature of rimming Newtonian flow was discussed in a number of publications [5–11]. Although the aforementioned investigations highlight the main characteristics of rimming flow, not enough has been done to show the effect of non-Newtonian properties on such flow, given its importance. Only a few attempts have been made. The power-law [12], Carreau–Yasuda [13], Ellis [14,15], Bingham [16], and viscoelastic models [17,18] have been used to study rimming flow. Fomin et al. [13,14] and Fomin [15] recently extended the estimates, originally made by Moffatt [3] for Newtonian fluids, for a generalized Newtonian fluid. Most polymeric solutes used in rotational coating are non-Newtonian liquids, which exhibit shear-thinning behavior for moderate to high shear rates. Liquid polymers behave as Newtonian liquids near the free surface (at very low shear rates) and exhibit non-Newtonian characteristics above a certain transitional shear rate,  $\dot{\gamma}_t$ . The importance of non-Newtonian effects for generalized Newtonian fluids is characterized by the shear-thinning number  $Wi = \lambda \Omega/\delta$ , where  $\Omega$  is the characteristic angular velocity of the rotating cylinder,  $\delta$  is the ratio of the characteristic thickness of the film and the radius of the cylinder, and  $\lambda \approx (\dot{\gamma}_t)^{-1}$  is a typical time scale for liquid polymers, which is well documented [19] and normally stays in the interval of  $(10^{-2}, 10^{-1})$  seconds. In some situations, e.g. a higher speed of rotation, a thinner liquid layer, or a smaller transition shear rate, the value of Wi can be quite large. This illustrates the dominating role of non-Newtonian effects. Results of numerical computations available in [13] show that a Carreau and power-law models practically

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Nomenclature
           concentration of reacting solute, c = c/c_0
С
           initial concentration of reacting solute
c_0
           inverse of the Bond number
C_B
           Deborah number
De
           inverse function to \eta(x)x
G
           gravitational acceleration
g
           thickness of the liquid layer, h = h/h_0
h
           critical thickness of the liquid layer at \theta = 0
h_c
           characteristic thickness of the liquid layer
h_0
k
           consistency parameter in a power-law constitutive equation
n
           flow index
           non-dimensional pressure, p = p^*/(g\rho r_0)
р
           non-dimensional mass flux
q
           non-dimensional radial coordinate, r = r^*/r_0
r
r_{o}
           radius of the cylinder
           non-dimensional radial coordinate, R = (1 - r)/\delta
Re
           Reynolds number
t
           non-dimensional time, t = t^*\Omega.
           non-dimensional radial and azimuthal components of the fluid velocity, v_{\theta} = v_{\theta}^*/(\Omega r_0), v_R = v_r^*/(\Omega_0 r_0 \delta)
VR. VA
Wi
           shear-thinning number, Wi = \lambda \Omega / \delta
Greek symbols
           ratio of the characteristic liquid layer thickness to the radius of the cylinder, \delta = h_0/r_0
įγ
           shear rate
           relaxation time
λ
к
           parameter in a kinetic equation that defines the rate of polymeric reaction
           function of deformation rate
μ
           time-dependent viscosity
η
           characteristic viscosity (\eta_0 = k(\Omega/\delta)^{n-1} for the power-law fluid)
\eta_0
           azimuthal coordinate
θ
           liquid density
ρ
           surface tension
\sigma
      	au_{RR}, 	au_{	heta 	heta} non-dimensional components of the stress tensor deviator, 	au_{R	heta} = 	au_{r	heta}^*/(\eta_0 \Omega/\delta), 	au_{RR} = 	au_{rr}^*/(\eta_0 \Omega),
\tau_{\theta R},
           \tau_{\theta\theta} = \tau_{\theta\theta}^*/(\eta_0\Omega).
           angular velocity of the cylinder
u(t)
           characteristic (maximal) angular velocity of the cylinder
Ω
Superscripts
           dimensional quantities
Subscripts
0
           characteristic quantity
           azimuthal component
\theta
           radial component
R
```

coincide. A similar conclusion was made in [14] for Ellis fluids. Hence, flows that can be characterized by high values of the shear-thinning number can be modeled by the power-law constitutive equation.

Our main concern is the rotational molding of highly viscous polymers [1,2] that exhibit non-Newtonian shear thinning or shear thickening behavior. We are particularly interested in eliminating possible instabilities and providing the criteria for steady-state flow to obtain a continuous and smoothly coated film on the wall of the horizontal cylinder. Our research focuses on the analysis of the rimming flow of highly viscous non-Newtonian polymeric fluids and the transition of this time-dependent flow to a steady-state mode. Analysis of non-steady non-Newtonian rimming flow is based on the numerical solution of the governing equation of the liquid film thickness for power-law and Ellis fluids. The factors that affect the length of the transition period from non-steady to steady state mode are defined, and the behavior of the liquid film during this period is illustrated. For reactive rimming flow, the stabilizing effect of the viscosity-increasing chemical reaction is demonstrated.

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