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## An analytical method for magnetoelastostatic analysis of functionally graded hollow cylinders

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### ABSTRACT

This paper considers magnetoelastostatic behavior of a functionally graded material (FGM) hollow cylinder, placed in a uniform magnetic field, subjected to thermal and mechanical loads. Exact solutions for stresses and perturbations of the magnetic field vector in FGM hollow cylinders is determined by using the infinitesimal theory of magnetoelastostaticity. Numerical results indicate that the inhomogeneous constants presented in the present study are useful parameters from a design point of view in that it can be tailored for specific applications to control the stress and perturbation of magnetic field vector distributions. This research is helpful for the optimum design annular cylindrical FGM sensors/actuators.

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### 1. Introduction

FGMs have been developed for structural components or mechanical elements such as those used in nuclear, aircraft and space engineering. To aid in the design of FGMs, it will be useful to have an understanding of the manner in which the inhomogeneous constants affect the induced magnetoelastostatic stresses and perturbation of magnetic field vector. To our knowledge, investigations on the exact solutions for the FGM hollow cylinder, placed in a uniform magnetic field, subjected to thermal and mechanical loads have not been found in literatures.

To date there have only been a few studies on mechanical behaviors of the FGM hollow cylinder. Zimmerman and Lutz [1] investigated the thermal stresses and effective thermal expansion in a uniformly heated FGM cylinder. Using the infinitesimal theory of elasticity, Naki and Murat [2] obtained a closed-form solution for stresses and displacements in functionally graded cylindrical and spherical vessels subjected to internal pressure. Wu et al. [3] presented an analytical study for piezoelectric behavior of a functionally graded piezoelectric cylindrical shell subjected to axisymmetric thermal of mechanical loading. Using the state space formulations, Chen et al. [4] investigated the free vibration of an arbitrarily thick orthotropic piezoelectric hollow cylinder with a functionally graded property along the thickness direction and filled with a non-viscous compressible fluid medium. Jabbari et al. [5,6] studied the mechanical and thermal stresses in a functionally graded hollow cylinder due to axisymmetric mechanical and thermal loads. Jabbari et al. [7] gave a general theoretical analysis of three-dimensional mechanical and thermal stresses for a short FGM hollow cylinder. Recently, Jabbari et al. [8] presented an analytical solution of one-dimensional mechanical and thermal stresses for a hollow cylinder made of functionally graded material. Zhao et al. [9] analyzed theoretically the transient thermo-mechanical behavior of a FGM solid cylinder under convective boundary condition. Dai et al. [10–13] studied the magnetoelastostatic interactions in hollow and solid

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### Nomenclature

$\vec{U}, u$	displacement vector and radial displacement [m]
$r$	radial variable [m]
$E_0, c_{ij}$	elastic constants [N/m <sup>2</sup> ]
$\nu$	Poisson ratio
$\sigma_r, \sigma_\theta$	components of stress [N/m <sup>2</sup> ]
$T(r)$	temperature distribution [K]
$\alpha_i, \lambda_i$	thermal constants [1/K] and thermal modulus [N/m <sup>2</sup> K]
$k$	thermal conduction coefficient [W/mK]
$h$	ratio of the convective heat-transfer coefficient [W/K]
$\vec{J}$	electric current density vector
$\vec{h}$	perturbation of magnetic field vector
$\vec{e}$	perturbation of electric field vector
$\vec{H}$	magnetic intensity vector
$\mu_0$	magnetic permeability [H/m]
$f_z$	Lorentz's force [kg/m <sup>2</sup> s <sup>2</sup> ]
$a, b$	inner and outer radii of the FGM hollow cylinder [m]
$P_a, P_b$	internal and external pressure of the FGM hollow cylinder [kg/m <sup>2</sup> s <sup>2</sup> ]

### Non-dimensional quantities

$R$	$\frac{r-a}{b-a}$
$T^*$	$\frac{T(r)}{T_0}$
$u^*$	$\frac{u}{a}$
$\sigma_r^*$	$\frac{\sigma_r}{P_a}$
$\sigma_\theta^*$	$\frac{\sigma_\theta}{P_a}$
$h_z^*$	$\frac{h_z}{H_z}$
$\sigma_r^\#$	$\frac{\sigma_r}{P_b}$
$\sigma_\theta^\#$	$\frac{\sigma_\theta}{P_b}$

cylindrical and spherical structures of functionally graded material subjected to mechanical loads. By means of the Fredholm integral equation, Li et al. [14] investigated radially polarized functionally graded piezoelectric hollow cylinders as sensors and actuators. Hosseini and Shahabian [15] presented the reliability analysis and safety evaluation of dynamic stresses for Al-Al<sub>2</sub>O<sub>3</sub> FG thick hollow cylinder subjected to sudden unloading as a mechanical shock loading.

This paper investigates magnetoelastothermoelastic behaviors of a FGM hollow cylinder, placed in a uniform magnetic field, subjected to thermal and mechanical loads. A simple, tractable closed-form solution for the FGM hollow cylinder is presented. The emphasis of this research is laid on the effects of the inhomogeneous constants on magnetoelastothermoelastic stresses and the perturbation of magnetic field vector. By means of practical example, it is possible for engineers to design a FGM cylindrical structure that can meet some special requirements by selecting proper values of  $\beta_i (i = 1, 2, 3, 4)$  and suitable loads.

## 2. Basic formulations of the problem

### 2.1. Derivation of equations

A long, FGM hollow cylinder with internal radius  $a$  and external radius  $b$  placed in a uniform magnetic field  $\vec{H}(0, 0, H_z)$  is shown in Fig. 1, the magnetoelastothermoelastic stresses and perturbation of magnetic field vector distributions in the FGM hollow cylinders will be calculated. Letting the cylindrical coordinates of any representative point be  $(r, \theta, z)$ , the stiffness and thermal expansion coefficients are assumed to vary as  $c_{ij} = c_{ij}^0 r^{\beta_i}$  ( $i = 1, 2, j = 1, 2$ ) and  $\alpha_i(r) = \alpha_i^0 r^{\beta_i}$  ( $i = 1, 2$ ) through the wall thickness, respectively. Similar assumptions can be found in previous studies [2,16,17]. Here,  $c_{ij}^0$  is the stiffness at the external surface ( $r = b$ ),  $\alpha_i^0$  are the thermal expansion coefficients at the external surface ( $r = b$ ) and  $\beta_i (i = 1, 2)$  is the inhomogeneous constant determined empirically. However, these values for  $\beta_i (i = 1, 2)$  do not necessarily represent a certain material. The range  $\beta_i \in [-2, 2]$  to be used in the present study covers the main part of the values of coordinate exponents encountered in the references cited earlier [2,3], and it is enough to demonstrate the effect of inhomogeneity on the

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