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## Regenerable ceria-based SO<sub>x</sub> traps for sulfur removal in lean exhausts

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#### ABSTRACT

Bare and Pt-containing CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxide and Al<sub>2</sub>O<sub>3</sub> have been investigated as potential regenerable sulfur oxides (SO<sub>x</sub>) traps. The samples were evaluated by lean SO<sub>x</sub> adsorption and temperature programmed desorption using synthetic gas compositions. In addition, combined DRIFT spectroscopy and mass spectrometry were employed to obtain mechanistic information on the adsorption of SO<sub>x</sub>. The results suggest Pt/CeO<sub>2</sub> as promising SO<sub>x</sub> trap material owing to a high storage capacity at 250 °C in combination with efficient release above 600 °C. The presence of Pt is generally found to enhance the lean SO<sub>x</sub> storage capacity at 250 °C for CeO<sub>2</sub>-based samples. Lean SO<sub>2</sub> adsorption on CeO<sub>2</sub> is found to proceed via the formation of surface and bulk sulfates, where the latter is formed more rapidly for the Pt-containing CeO<sub>2</sub> sample. Ceria samples pre-exposed to high amounts of SO<sub>2</sub> at 250 and 400 °C show lower SO<sub>x</sub> storage capacity and higher SO<sub>x</sub> release as compared to fresh samples. This indicates that under the conditions used in this study, a part of the storage sites on CeO<sub>2</sub> are non-regenerable.

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#### 1. Introduction

One strategy to reduce CO<sub>2</sub> emissions within the transportation sector is to increase the fuel efficiency by the use of lean-burn or diesel engines [1]. The lean character of the exhausts from these engines requires other aftertreatment concepts than standard three-way technology. One such concept is NO<sub>x</sub> storage catalysis which has shown promising characteristics for NO<sub>x</sub> reduction under net-lean conditions [2]. This concept is based on temporary storage of NOx on basic storage sites, usually provided by metal oxides like barium oxide (BaO), during lean periods and release with subsequent reduction of NO<sub>x</sub> over noble metals during short periods of rich or stoichiometric conditions. However, one issue regarding this type of catalyst is the sensitivity of the storage material to sulfur, i.e., high affinity towards storage of sulfur oxides (SO<sub>x</sub>) under lean conditions and negligible release of sulfur compounds under the NO<sub>x</sub> regeneration phase. In course of time, a progressing sulfur poisoning will reduce the NO<sub>x</sub> storage capacity and the number of available NO<sub>x</sub> storage sites will eventually become critically low, which leads to insufficient NO<sub>x</sub> storage and reduction [2-5]. To regenerate the  $NO_x$  storage capacity at this stage, thermal decomposition under net reducing conditions by a drastic increase of temperature is essentially the only solution. However, the temperature required for this procedure is too high to guarantee the stability of the catalyst towards thermal deactivation.

Sulfur containing species in the exhausts originate from fuel and lubricants. Even though the content of sulfur in the fuel has been significantly reduced over the years, the presence of sulfur will always lead to reduced NO<sub>x</sub> storage capacity. Thus, within the present technology, strategies to handle sulfur in the exhaust are necessary. This can be achieved by increasing the sulfur tolerance of the aftertreatment system or preventing  $SO_x$  from reaching the  $NO_x$  storage catalyst by using upstream  $SO_x$  traps. The sulfur tolerance of the catalyst can be increased by enhancing the release of sulfur species during regeneration and/or by decreasing the sulfur affinity of the storage material. The sulfur release during regeneration can, for example, be facilitated by using thinner washcoat layers [6] or by adding TiO<sub>2</sub> to the Al<sub>2</sub>O<sub>3</sub>-support of the NO<sub>x</sub> storage catalyst [1]. Moreover, the amount of sulfur adsorbed can be decreased by replacing the NO<sub>x</sub> storing component with a material with lower affinity towards sulfur compounds [7,8]. A few different SO<sub>x</sub> trap strategies have been suggested and materials such as BaO supported on Al<sub>2</sub>O<sub>3</sub> [9], Ba/Cu-benzene tricarboxylate [10],  $K_xMn_8O_{16}$  [11] and MnO [12] have been proposed as  $SO_x$ adsorbents.

In the present work, a series of different materials is evaluated as regenerable  $SO_x$  traps. Such traps should, in different temperature intervals, store and release  $SO_x$  under lean conditions. During regeneration of the  $SO_x$  trap, the exhausts will be by-passed

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the NO<sub>x</sub> storage catalyst to minimize the sulfur exposure. This strategy should be chosen as sulfur species previously have been reported to adsorb on the catalyst under both lean and rich conditions blocking storage and noble metal sites [13]. To our knowledge, this regeneration technique has not previously been suggested in the literature. The desired properties of the  $SO_x$ adsorbent are to store  $SO_x$  under normal lean exhaust conditions in the temperature interval 200-500 °C and release the stored sulfur species under lean conditions at temperatures slightly above 500 °C. In this way, the fuel consumption required to produce the heat for regeneration is minimized. To avoid permanent sulfur poisoning, we intuitively choose to compare different metal oxides that are sufficiently basic to store SO<sub>x</sub>, e.g. CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxide and Al<sub>2</sub>O<sub>3</sub>, but less basic than BaO. Ceria is an interesting oxide for many aftertreatment applications. For example, ceria is used as an oxygen storage component in the three-way catalyst and as  $SO_x$  traps for stationary applications [14]. It is known that sulfates may form on ceria upon exposure to SO2 even in the absence of oxygen [15], a property that probably is caused by the high oxygen mobility within the material. Adsorbents based on Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxides from hydrotalcite precursors have also been suggested as  $SO_x$  traps for stationary applications [16]. By using hydrotalcite precursors for the mixed oxide, it is possible to control the basicity of the storage material by varying the Al<sub>2</sub>O<sub>3</sub>:MgO ratio. Alumina, which is an amphotheric oxide, is the least basic oxide in the present study and is included primarily as reference material. Boehmite is used as binder for the monolith samples which means that all samples contain some Al<sub>2</sub>O<sub>3</sub>. To investigate the suitability of these metal oxides as SO<sub>x</sub> traps, we have employed both kinetic studies in a flow-reactor and mechanistic studies by combined qualitative diffuse reflectance infrared fourier transformed spectroscopy (DRIFTS) and mass spectrometry. The influence of noble metal on the SO<sub>x</sub> storage and release properties of the SO<sub>x</sub> traps is investigated as well as the stability of the SO<sub>x</sub> adsorbent.

#### 2. Experimental considerations

#### 2.1. Sample preparation and characterisation

The metal oxides used as SO<sub>x</sub> adsorbents were; CeO<sub>2</sub> (99.5 H.S.A. 514, Rhône-Poulenc), Al<sub>2</sub>O<sub>3</sub>:MgO (30:70 wt.%) mixed oxide prepared from a hydrotalcite precursor (Condea) and Al<sub>2</sub>O<sub>3</sub> (Puralox SBa-200, Sasol). All samples were pre-treated in air at 750 °C for 2 h. The Pt-containing powder samples were prepared by wet impregnation of Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> using Pt(NO<sub>3</sub>)<sub>2</sub> (Hereaus) as precursor. Due to different point of zero charge for the oxides, the impregnation was performed at pH 2 and 3 for the Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> sample, respectively. After impregnation, the slurries were instantly frozen with liquid nitrogen and freeze-dried. The resulting powder samples were finally calcined in air at 600 °C for 1 h (heating rate of 4.8 °C/min from 25 to 600 °C). Surface area measurements of the powder samples were performed by N2physisorption at 77 K using a Micromeritrics Tristar instrument. For a few selected samples, the specific surface areas, calculated using the BET-method [17], are summarised in Table 1.

Monoliths samples ( $\emptyset$  = 20 mm and length = 20 mm) were cut from a commercial honeycomb cordierite structure with 400 cpsi. The monoliths were coated with the  $SO_x$  adsorbent material following the procedure described in Ref. [18]. As a binder for the adsorbent material, Boehmite (Disperal SOL P2, Condea) was used in all samples (20 wt.% of the dry material in the slurry). After coating, all monolith samples were calcined in air at 650 °C for 3 h. The Pt-containing samples were prepared by impregnation of the coated monoliths using Pt(NO<sub>3</sub>)<sub>2</sub> as platinum precursor for the

**Table 1**Specific surface area of Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>-based powder samples

Sample	Specific surface area (m²/g)	Comment
CeO <sub>2</sub> CeO <sub>2</sub> 5 wt.% Pt/CeO <sub>2</sub>	254 82 78	Fresh Air, 750 °C, 2 h CeO <sub>2</sub> treated in air, 750 °C, 2 h and impregnated with Pt
Al <sub>2</sub> O <sub>3</sub> Al <sub>2</sub> O <sub>3</sub> 5 wt.% Pt/Al <sub>2</sub> O <sub>3</sub>	203 187 174	Fresh Air, 750 °C, 2.5 h Al $_2$ O $_3$ treated in air, 750 °C, 2.5 h and impregnated with Pt

Al $_2$ O $_3$  and CeO $_2$  samples and Pt(NH $_3$ ) $_2$ (NO $_2$ ) $_2$  (Johnson Matthey) for the Al $_2$ O $_3$ :MgO sample. The impregnation was performed at pH 2, 3 and 8 for the Al $_2$ O $_3$ , CeO $_2$  and Al $_2$ O $_3$ :MgO sample, respectively. After impregnation, the monolith samples were dried in air at 80 °C for 12 h. The temperature was thereafter gently increased by 4.3 °C/min to 600 °C and the samples were finally calcined in air at this temperature for 1 h.

## 2.2. Isothermal SO<sub>2</sub> adsorption followed by temperature programmed desorption

The flow-reactor experiments with monolith samples were performed using a quartz tube reactor equipped with a gas mixer unit (Environmentics 2000) for control of the inlet gas composition, and a surrounding metal coil for resistive heating of the reactor tube. A thermocouple (type K, Pentronic) placed 10 mm upstream of the monolith was used together with a Eurotherm regulator to control the inlet gas temperature. A second thermocouple was positioned inside the monolith, about 2 mm from the end of the sample, to measure the sample temperature. To facilitate the analysis of the total  $SO_x$  outlet concentration, the experimental method previously reported by McLaughlin et al. [19] was used. Following this method, the outlet gas flow was first passed over an oxidation catalyst before introduced to the  $SO_2$  analyser (non-dispersive IR, Maihak UNOR 610). For further information about the experimental method see Appendix A.

For all experiments, the total flow was 3500 ml/min, which corresponds to GHSV = 33 400 h<sup>-1</sup>, and Ar was used as balance. Prior to each experiment, the samples were treated in 7%  $O_2$  for 10 min at 500 °C. The temperature was thereafter decreased and lean  $SO_x$  adsorption was performed (100 ppm  $SO_2$  and 7%  $O_2$  in Ar) at 250 or 400 °C for 1 h. The high  $SO_2$  concentration in these experiments was used to assure measurement accuracy rather than mimicking real lean exhaust conditions. After the  $SO_2$  exposure, temperature programmed desorption (lean  $SO_x$ -TPD) was performed by increasing the temperature by 10 °C/min to 700 °C in 7%  $O_2$ . The temperature was kept constant at 700 °C for 20 min before cooling in Ar.

#### 2.3. DRIFT spectroscopy measurements

FTIR measurements were performed with powder samples in diffuse reflectance mode using a Bio-Rad FTS6000 spectrometer equipped with a Harrick Praying Mantis DRIFTS cell and a MCT detector. The resolution was 1 cm $^{-1}$  and the number of scans per spectrum was set to 20. All experiments were performed with fresh samples using a total gas flow of 100 ml/min and Ar as balance. Prior to each experiment, the sample was treated in 20%  $O_2$  at 500 °C for 10 min followed by cooling in 7%  $O_2$  to the temperature to be studied, i.e., 250 or 400 °C. Because the windows in the reactor dome absorb IR radiation in the same wavenumber

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