



## NO<sub>x</sub> storage and reduction with H<sub>2</sub> on Pt/BaO/Al<sub>2</sub>O<sub>3</sub> monolith: Spatio-temporal resolution of product distribution<sup>☆</sup>

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### ABSTRACT

The regeneration of a model Pt/BaO/Al<sub>2</sub>O<sub>3</sub> monolith catalyst was studied with hydrogen as the reductant to elucidate the reaction pathways to molecular nitrogen and ammonia. NO<sub>x</sub> storage and reduction experiments (NSR) were conducted with a 2 cm length monolith for a wide range of feed conditions. The NSR experiments were replicated for a series of monoliths of progressively decreasing length, enabling the construction of spatio-temporal profiles of reactant and product concentrations. The results show that there are two primary competing routes to the desired N<sub>2</sub> product; specifically a direct route from the reduction of stored NO<sub>x</sub> by H<sub>2</sub> (H<sub>2</sub> + NO<sub>x</sub> → N<sub>2</sub>) or by a sequential route through NH<sub>3</sub> (H<sub>2</sub> + NO<sub>x</sub> → NH<sub>3</sub>; NH<sub>3</sub> + NO<sub>x</sub> → N<sub>2</sub>). A comparison between H<sub>2</sub> and NH<sub>3</sub> as reductant feeds during NSR revealed H<sub>2</sub> is a more effective reductant in terms of NO<sub>x</sub> conversion for temperatures below approximately 230 °C. At higher temperatures (230–380 °C), the regeneration of stored NO<sub>x</sub> is feed-limited and the difference between the reductants H<sub>2</sub> and NH<sub>3</sub> is found to be small with H<sub>2</sub> being a slightly superior reductant. Experimental measurements of the traveling front velocity are compared with a simple feed-limited model that assumes complete consumption of H<sub>2</sub> as stored NO<sub>x</sub> is depleted. At lower temperatures the regeneration is limited by chemical processes at the Pt/Ba interface. The findings are pieced together to establish a phenomenological description of the spatio-temporal features of the lean NO<sub>x</sub> trap with hydrogen as the reductant.

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### 1. Introduction

Lean burn combustion encountered in lean burn gasoline and diesel vehicles provides for a higher fuel efficiency compared to stoichiometrically operated gasoline engines. However, the unconverted oxygen in the exhaust prevents the use of conventional three-way catalysts (TWC) in the reduction of NO<sub>x</sub> to N<sub>2</sub>. NO<sub>x</sub> storage and reduction (NSR) is a periodic catalytic process for converting NO and NO<sub>2</sub> (NO<sub>x</sub>) to N<sub>2</sub> that overcomes this obstacle.

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The inherent transient nature of NSR makes it highly complex, especially in terms of the spatio-temporal interactions of the storage and reduction catalytic processes. Advanced catalytic engineering is needed to elucidate the transient product distribution in particular since in most cases the objective is to convert NO<sub>x</sub> to molecular nitrogen.

During NSR, the NO<sub>x</sub> removal process involves two stages on a bifunctional supported catalyst. The first “storage” stage involves the reactive trapping of NO<sub>x</sub>, in the form of nitrites or nitrates, on an alkali earth component (such as Ba, Ca, or Sr) enhanced by the catalytic oxidation of NO to NO<sub>2</sub> on the precious metal (Pt, Rh). The typical duration of this stage is 30–90 s. The second “purge” or “regeneration” stage involves purging or regenerating with a rich pulse containing reductant(s), carried out before an unacceptable amount of NO<sub>x</sub> breaks through during the storage. The rich pulse duration is only a few seconds. It is created through intermittent rich operation of the engine, producing a mixture of H<sub>2</sub>, CO, and low molecular weight hydrocarbons, or through direct injection of fuel into the exhaust system.

Earlier studies of NSR focused on the storage process, which established that the primary steps are the catalytic oxidation of NO to NO<sub>2</sub> followed by NO<sub>2</sub> storage by the disproportionation

mechanism [1–5]. The mechanistic details at the Pt/Ba interface remain elusive. Recent research has shifted to the kinetics of the regeneration process. Particular attention has been placed on H<sub>2</sub> because it is not only present in the exhaust during rich engine operation, but also it is catalytically generated by both steam reforming of exhaust hydrocarbons and water gas shifting of CO. Hydrogen has been shown to be the most effective reductant due to its high reactivity with O, H, and N adspecies which are present during conventional NSR operation. Hydrogen is uniquely reactive at low temperatures (below 200 °C) [6–9]. The mechanism of NO<sub>x</sub> reduction under cycling conditions is still not fully understood. Muncrief et al. [10] suggested a thermally driven process under conditions in which a relatively large concentration of O<sub>2</sub> is present during the rich pulse, which is more typical of diesel applications. Liu and Anderson [7] proposed a spillover mechanism of reductant from the precious metal (Pt) to storage phase comprising barium nitrate, Ba(NO<sub>3</sub>)<sub>2</sub>. Their proposed mechanism involves the reductant reacting directly with Ba(NO<sub>3</sub>)<sub>2</sub> forming Ba(NO<sub>2</sub>)<sub>2</sub>, which then releases the stored NO<sub>x</sub> as NO. Nova et al. [11,12] studied the reduction process under nearly isothermal conditions and observed that the thermal decomposition of stored NO<sub>x</sub> was not necessary to reduce the stored NO<sub>x</sub> with H<sub>2</sub> since regeneration can occur at temperatures well below the temperature at which stored NO<sub>x</sub> decomposes. They proposed that the reduction of stored nitrates involves a Pt catalyzed surface reaction and argued that the pathway only occurs when both components (Pt and BaO) are well dispersed on the same support (as opposed to physical mixtures of separate populations of supported Pt and BaO particles). A follow up study by Cant et al. [13] observed results similar to those of Nova et al. [11] when comparing a sample with Pt and BaO dispersed on the same support with a physical mixture of BaO/Al<sub>2</sub>O<sub>3</sub> and Pt/SiO<sub>2</sub>; Pt/SiO<sub>2</sub> was used instead of Pt/Al<sub>2</sub>O<sub>3</sub> in order to rule out NO<sub>x</sub> storage on the same support as Pt. The reverse spillover of NO<sub>x</sub> from BaO to Pt has also been speculated to occur [13–17]. Cant et al. [13] studied the isotopic exchange rate of <sup>15</sup>NO and stored <sup>14</sup>NO<sub>x</sub> during storage on the two system described above at 360 °C. They concluded that the forward and reverse spillover of NO<sub>x</sub> is important since the exchange rate was more than five times faster for the Pt/BaO/Al<sub>2</sub>O<sub>3</sub> sample than for the physical mixture. James et al. [14] proposed the “reverse” spillover mechanism to explain the decomposition of nitrates stored far from Pt. Zhou et al. [17] have described the nitrate ions as being mobile in the barium phase with the reaction occurring at the Pt/Ba interface. However, neither H<sub>2</sub> spillover to BaO nor the reverse spillover of NO<sub>x</sub> to Pt has been proven to be the main mechanism. Medhekar et al. [18] studied pre-reduced, pre-oxidized, and pre-nitrated Pt/BaO catalysts, and proposed that there existed two distinct reduction sites on Pt crystallites on the supported catalyst. The first type of sites are located further from the Pt/Ba interface where H<sub>2</sub> scavenging of surface oxygen provides a clean surface for NO decomposition to N<sub>2</sub> and N hydrogenation to NH<sub>3</sub>. The second type of sites is located at the Pt/BaO interface. At these sites H<sub>2</sub> oxidation, nitrate decomposition, and NO decomposition and reduction occur, producing a complex mixture of N<sub>2</sub>, N<sub>2</sub>O, and NH<sub>3</sub> which depends on the temperature and effective NO<sub>x</sub>/H ratio.

The situation is further complicated by integral effects brought about by chemistry occurring downstream in the monolith channel, Choi et al. [19] applied spatially-resolved mass spectrometry, coined “Spaci-MS”, to obtain spatial profiles of reactant and product profiles through the use of capillary probes positioned in multiple monolith channels along the length of the monolith. In their study, Choi et al. [19] showed that H<sub>2</sub> produced from the water gas shift reaction had only a minor effect on the NO<sub>x</sub> release and reduction.

The effects of H<sub>2</sub>O and CO<sub>2</sub> on the reduction of stored NO<sub>x</sub> by H<sub>2</sub> have been investigated [20–22]. Lindolm et al. [20] observed that CO<sub>2</sub> had a promoting effect on NH<sub>3</sub> formation at low temperatures. Lietti et al. [21] observed that the reduction of stored NO<sub>x</sub> is slower when CO<sub>2</sub> and H<sub>2</sub>O are fed during the regeneration.

More recent studies have been carried out that have focused on the role of ammonia during NSR. Ammonia is an undesired product during conventional NO<sub>x</sub> trap operation, however, it is a desired product in coupled LNT/SCR systems [23–25]. Pihl et al. [26] and Cumarantunge et al. [27] proposed that NH<sub>3</sub> formed upstream by the reaction of feed H<sub>2</sub> and stored NO<sub>x</sub> may be consumed downstream by its own reduction of stored NO<sub>x</sub> [26,27]. Once formed, the generated N<sub>2</sub> flows down the reactor and out with the effluent. NH<sub>3</sub> has the complicating feature that it will readsorb and react downstream with stored NO<sub>x</sub>. Pihl et al. [26] described the monolith reaction system by three sections: mostly regenerated, reductant front, and un-regenerated. They proposed that the reductant H<sub>2</sub> front moves through the entrance section of the monolith where the main reduction chemistry occurs. Cumarantunge et al. [27] described the NH<sub>3</sub> as a hydrogen carrier, from which H adatoms react with stored NO<sub>x</sub> to produce N<sub>2</sub>. They showed that the effectiveness of NH<sub>3</sub> and H<sub>2</sub> under reductant limited conditions (350 °C) were similar. However, data were not presented by either of the two groups that conclusively prove the proposed picture. Xu et al. [28] showed that the steady-state selectivity of the reaction between H<sub>2</sub> and NO to N<sub>2</sub>O, N<sub>2</sub>, and NH<sub>3</sub> is largely dictated by the feed composition (H<sub>2</sub>/NO ratio) and temperature under steady-state conditions. Clayton et al. [29] have shown that the reduction of NO by a co-feed of H<sub>2</sub> and NH<sub>3</sub> identifies H<sub>2</sub> as the superior reductant. To this end, under the complex spatio-temporal conditions encountered during the hydrogen regeneration of the NO<sub>x</sub> trap, isolating the production of ammonia from its consumption is key to understanding the NO<sub>x</sub> trap performance.

The objective of this study is to establish a more complete picture supported by experimental measurement of lean NO<sub>x</sub> trap behavior during NSR using H<sub>2</sub> as a reductant. This is accomplished through bench-scale LNT measurements in which the concentrations of all reactants and products are measured. We utilize a novel approach to generate axial profiles of species concentrations over a range of conditions. An analysis of the product distribution reveals the different routes to the desired N<sub>2</sub> product, whether directly from the reduction of stored NO<sub>x</sub> by H<sub>2</sub> or indirectly through an NH<sub>3</sub> intermediate. The data also provide information about the velocity of the moving hydrogen and ammonia fronts. The findings are pieced together to establish a phenomenological description of the spatio-temporal features of the lean NO<sub>x</sub> trap with H<sub>2</sub> as the reductant.

## 2. Experimental

### 2.1. Catalyst samples

The catalyst samples used for these experiments were monolith catalysts provided by BASF Catalysts LLC (Iselin, New Jersey). Larger cylindrical cores ( $D = 3.8$  cm,  $L = 7.6$  cm) were cut using a dry diamond saw to smaller, nearly cylindrical shapes ( $D \sim 0.8$  cm,  $L = 0.33$ – $2$  cm). The samples contained BaO with varying amounts of Pt on a  $\gamma$ -alumina washcoat support adsorbed on a cordierite structure ( $\sim 62$  channels/cm<sup>2</sup>). The mass of washcoat material ( $m_{wc}$ ) on each monolith piece (of  $L = 2$  cm) was approximately 110 mg. The compositions and properties of the catalysts are given in Table 1. The methods used to characterize the catalysts were described previously [28]. The monoliths were then wrapped in Fiberfrax<sup>®</sup> ceramic paper that had been heat treated and then placed in a quartz tube flow reactor.

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