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Activity Coefficients of Uranyl Nitrate and Nitric Acid in Aqueous Mixtures

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Abstract

The activity coefficients of nitric acid and uranyl nitrate in aqueous mixtures are necessary to model the system H₂O-HNO₃-UO₂(NO₃)₂-TBP-diluent. Three methods have been compared in this work to determine activity coefficients based on experimental data, Pitzer's equation or Zdanovskiy's rule. Acid activities have been calculated from the data of two first methods. These results were compared with the data of third method. Errors were about 3.3 %. Activity coefficients of uranyl nitrate γ_U as a function of concentration of uranyl nitrate and nitric acid were determined in 76 mixed solutions. The equation to calculate γ_U was proposed.

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1. Introduction

The nuclear fuel reprocessing is based on PUREX process. The organic solvent is usually composed of 30% tributyl phosphate (TBP) in a hydrocarbon diluents. Then the composition of the organic phase can be expressed as H₂O-HNO₃-UO₂(NO₃)₂-Pu(NO₃)₄-TBP-diluent. But because the concentration of plutonium is low the system can be considered a five-component one ^{1,2}. Activities of uranyl nitrate and nitric acid in mixtures should be determined to model this extracting system. The methods of the derivation of this data will be considered here.

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2. Determination of activities from the experiments and Pitzer parameters

Table 1. Acid activities in mixed solutions of acid and uranyl nitrate

N	Concentrations ³ , mole/L		Density ³ , g/cm ³	Vapor pressure of HNO ₃ ³ , mm Hg	HNO ₃ activity			Average <i>a_{am}</i>
	UO ₂ (NO ₃) ₂ <i>c_U</i>	HNO ₃ <i>c_a</i>			<i>a_{a3}</i> ³	<i>a_{a4}</i> ⁴	<i>a_{a5}</i> ⁵	
1	0.466	0.976	1.1782	288·10 ⁻⁶	1.158	1.359	1.543	1.353 1.451*
2	0.466	0.976	1.1782	288·10 ⁻⁶	1.158	1.359	1.543	1.353 1.451*
3	0.902	0.951	1.3176	725·10 ⁻⁶	2.914	2.926	3.433	3.091
4	0.902	0.951	1.3176	868·10 ⁻⁶	3.489	2.926	3.433	3.283
5	1.314	0.92	1.4467	0.00159	6.391	5.615	6.592	6.199
6	1.314	0.92	1.4467	0.00174	6.994	5.615	6.592	6.400
7	1.314	0.92	1.4467	0.00175	7.034	5.615	6.592	6.414
8	0.451	2.195	1.2163	0.00232	9.325	8.613	8.963	8.967
9	0.854	2.108	1.3426	0.00332	13.344	14.723	15.796	14.621
10	0.854	2.108	1.3426	0.00392	15.756	14.723	15.796	15.425
11	1.237	2.026	1.461	0.00724	29.100	23.798	25.804	26.234
12	1.237	2.026	1.461	0.00739	29.703	23.798	25.804	26.435
13	0.086	4.29	1.1651	0.01038	41.721	42.203	40.595	41.506
14	0.213	4.248	1.2027	0.01214	48.795	48.674	47.026	48.165
15	0.213	4.248	1.2027	0.0122	49.036	48.674	47.026	48.245
16	0.418	4.182	1.2646	0.0156	62.702	60.772	59.486	60.987
17	0.418	4.182	1.2646	0.0155	62.300	60.772	59.486	60.853
18	0.418	4.182	1.2646	0.0158	63.505	60.772	59.486	61.254
19	0.418	4.182	1.2646	0.016	64.309	60.772	59.486	61.522
20	0.803	3.923	1.38	0.021	84.406	80.186	80.387	81.660
21	0.803	3.923	1.38	0.0214	86.014	80.186	80.387	82.196
22	0.808	4.039	1.3804	0.0213	85.612	80.186	90.435	85.411
23	0.808	4.039	1.3804	0.0204	81.994	80.186	90.435	84.205
24	1.16	3.799	1.485	0.0286	114.95	113.79	116.56	115.10
25	1.16	3.799	1.485	0.0269	108.12	113.79	116.56	112.82
26	1.166	3.885	1.4812	0.0348	139.87	126.57	129.42	131.95
27	1.376	3.716	1.545	0.0379	152.33	139.75	143.89	145.32
28	1.376	3.716	1.545	0.0339	136.25	139.75	143.89	139.96
29	1.428	3.818	1.5668	0.0384	154.34	157.56	162.38	158.09
30	1.428	3.818	1.5668	0.0385	154.74	157.56	162.38	158.23
31	0.5331	4.981	1.3235	0.0358	143.9	129.78	127.81	133.83
32	0.392	6.135	1.3136	0.0558	224.8	237.5	235.9	232.7
33	0.0984	7.462	1.2621	0.0924	371.4	382.8	395.5	383.2
34	0.2464	7.641	1.3148	0.1215	488.3	482.7	490.4	487.1
35	0.374	7.135	1.3366	0.0953	383.0	418.8	422	407.9
36	0.374	7.135	1.3366	0.0935	375.8	418.8	422	405.5
37	0.4871	7.674	1.4663	0.163	655.2	623.4	619	632.5
38	0.7437	7.776	1.4663	0.201	807.9	798.2	783.8	796.6
39	0.9843	7.654	1.535	0.24	964.6	898.3	924.4	929.1
40	0.2469	8.07	1.32	0.159	639.1	623.4	635.1	632.5
41	0.5232	8.227	1.3969	0.232	932.5	889.1	858.2	893.3
42	1.003	8.129	1.5492	0.287	1153.5	1133.0	1213.8	1166.8
	δ				6.0	4.8	4.8	
	δ*				5.1	4.9	3.8	

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