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Construction and Building Materials

journal homepage: www.elsevier.com/locate/conbuildmat



Shear and flexural strength prediction of corroded R.C. beams



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HIGHLIGHTS

- Experimental versus analytical prediction of effects of general and pitting corrosion on steel bars.
- Experimental versus analytical prediction of effects of general and pitting corrosion on R.C. cross-section if flexure.
- Experimental versus analytical prediction of effects of general and pitting corrosion on R.C. beams in shear.
- Case of study for strength and ductility degradation in flexure and shear of R.C. beams under natural corrosion scenarios.

ARTICLE INFO

Article history: Received 16 January 2016 Received in revised form 21 April 2017 Accepted 12 May 2017

Keywords: Shear-moment interaction Corrosion Bond Pitting Flexural response

ABSTRACT

The purpose of the work was the study of the structural safety of R.C. beams subjected to corrosion processes though the derivation of moment-curvature diagrams and moment-to-shear interaction diagrams. Normal-strength reinforced concrete beams with longitudinal bars in the presence of transverse stirrups and subjected to corrosion processed are considered.

Experimental results available in the literature related to corrosion processes, for steel bars, crack openings and bond degradation due to rust formation are reviewed. Then analytical laws relating to crack opening, bond degradation with attack penetration depth, through a rearranged form of Faraday's law, are presented. An analytical model for cross-section analysis and shear strength prediction including the main effect due to rust formation is developed and verified against experimental data. Finally, a case study is added giving moment-curvature diagrams and moment-to-shear interaction diagrams to show the effects of different scenarios of natural corrosion increasing with time on beam elements.

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1. Introduction

Corrosion of reinforcing steel is one of the main causes of deterioration of reinforced concrete structures and affects both ultimate and serviceability conditions [1,2]. Its effects include cracking and spalling of the concrete cover, reduction and loss of bond between concrete and corroding reinforcement, and reduction of the cross-sectional area of the reinforcing steel (longitudinal bars and stirrups).

Reinforcing steel is normally passive in concrete due to high alkalinity of the concrete pore solution. However, penetration into the concrete of chlorides or carbonation destroys this inhibitive property of the concrete and leads to corrosion. Two types of corrosion of reinforcement can affect an R.C. structure: general and pitting. General corrosion affects a substantial area of longitudinal and transverse reinforcements with more or less uniform metal loss over the perimeter of the reinforcing bars. It also causes crack-

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ing and possibly spalling and delamination of the concrete cover and produces rust staining on the concrete surface. Pitting is a localized corrosion type, which concentrates on small areas of reinforcement, causing spalling of the concrete cover.

Nondestructive tests allows one to establish the presence of carbonation in concrete (carbonation test) and/or the presence of chlorides (chloride content) and to know whether the corrosion processes are ongoing. Also, nnondestructive testing allows one to estimate for general corrosion the reduction of the area of steel reinforcements through the gravimetric method and allows one to estimate the pit in the bar for chloride attack.

Numerous experimental studies have investigated the effects of corrosion of materials such as on steel bars [3–4], steel-concrete bond [5–8], etc. There have also been studies at a structural level, relative for example to the flexural behavior of beams [9–13] and columns [10].

To reproduce the corrosion process in a laboratory, high intensities of current are used (ranging between $100 \,\mu\text{A/cm}^2$, used by [11] and $3000 \,\mu\text{A/cm}^2$, used by [5]); the duration of the tests is reduced to a few months or even a few days. In in situ structures,

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Nomenclature A_s cross-sectional area of longitudinal bars V_c contribution of shear force due to crushing of the conarea of pit A_p reduced area of steel bars due to pitting dimensionless contribution of shear force due to loss of $A_{s.pit}$ v_a $A_{s,red}$ reduced area of steel bars due to general and pitting corbond in anchorage zone dimensionless contribution of shear force due to beam v_b $A_{st,red}$ reduced area of stirrups dimensionless contribution of shear force due to crush- A_{st} section of tie transverse steel v_c ing of concrete a shear span b beam section width in the virgin state dimensionless contribution of shear force due to stir v_{st} b_f beam width increased by corrosion cracking ď distance from the extreme compressive fiber to the cendimensionless shear stress v_u troid of the tension reinforcement corrosion attack depth Χ D bar diameter loss of mass of steel bar X_p D_{eq} equivalent diameter of longitudinal bars position of neutral axis X_{c} D_{st} diameter of stirrups total crack width for one corrosion level W_{cr} E_c modulus of elasticity of concrete stress block coefficient α E_s modulus of elasticity of steel percent reduction of bar cross-section due to pitting a pit f_c mean value of concrete compressive strength value of percent reduction of bar cross section causing f_c* f_y f_{ys} H reduced concrete strength complete loss of ductility for pitted bars yield stress of longitudinal bar (or tie) stress block coefficient β yield stress of stirrups dimensionless post-peak bond strength γ height of beam δ concrete cover thickness current intensity bar cross-section area reduction due to pitting ΔA_{pit} i_{corr} coefficient related to internal arm strain at peak compressive stress for concrete ϵ_0 coefficient related to internal arm in the loaded section transversal strain of corroded beam 10 ε_1 k coefficient related to bar roughness and diameter ultimate strain of concrete ε_{cu} Κ coefficient related to concrete ultimate strain for steel ε_{su} L length of beam ultimate strain for steel of pitted bars É.,, anchorage length yield strain for steel l_{anc} ε_{sv} ultimate moment due to compression failure angle related to limit state governed by crushing of con- M_{uc} M_{uy} ultimate moment due to yielding of reinforcement crete ultimate moment associated with shear failure ductility of member M_{us} μ ductility of corroded members N_c ultimate axial force μ_{corr} number of bars in one layer softening coefficient $n_{\rm bars}$ depth of pit volume expansion ratio between rust and steel p(t) v_{rs} post-peak bond strength geometrical ratio of steel bars ρ q_{res} pitting coefficient R ρ_s geometrical ratio of stirrups ratio between mean value of concrete compressive S depth of carbonation tie spacing strength and reduced concrete compressive strength S opening of corrosion crack curvature at yielding $u_{i,corr}$ ϕ_s curvature at failure of steel bars V shear force ϕ_{su} V_a contribution of shear force due to loss of bond in curvature at compression failure ϕ_{cu} anchorage zone mechanical ratio of steel bars ω V_b contribution of shear force due to the beam effect

natural processes are characterized by lower current intensity and longer process times.

Natural processes are characterized by an intensity i of about $1~\mu\text{A/cm}^2$ and duration of the phenomenon comparable with the useful service life of the construction. For natural corrosion conditions, Table 1 gives the qualitative correlation between corrosion current ($\mu\text{A/cm}^2$) and corrosion of the rebar obtained with the linear polarization method (LPR), as suggested in [14].

To describe the structural behavior of corroded beams, most studies are based on numerical analyses carried out with the finite

Table 1Corrosion current vs. condition of the rebar.

Corrosion current (μA/cm ²)	Condition of rebar
≤ 0.1	Passive
$0.1 \div 0.5$	Low to moderate
$0.5 \div 1.0$	Moderate to high
≥ 1.0	High corrosion rate

element method [3,12]. These are complex and require detailed information on the constitutive laws of the damaged materials. Numerical analyses to calculate the effects of corrosion on mechanical parameters are carried out in [13]. In this paper, a simple approach based on sectional analysis in flexure and on a truss model in shear is utilized. Since it allows manual calculation, it can be considered a useful instrument for preliminary verification of the safety state in a deteriorated structure or prevision of its residual life [15]. It has to be stressed that the aim of this paper was also to show through moment-curvature diagrams and moment-to-shear interaction diagrams the effects of different corrosion scenarios increasing with time on beam elements.

2. Effect of corrosion on concrete and steel reinforcements

The main effects due to corrosion of longitudinal and transverse steel in R.C. beams, widely observed experimentally [11], are the following: – reduction of the steel area in the longitudinal bars

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