Applied Energy 205 (2017) 260-279

Contents lists available at ScienceDirect

Applied Energy

journal homepage: www.elsevier.com/locate/apenergy

Transient dynamic modeling and validation of an organic Rankine cycle waste heat recovery system for heavy duty diesel engine applications



AppliedEnergy

Bin Xu*, Dhruvang Rathod, Shreyas Kulkarni, Adamu Yebi, Zoran Filipi, Simona Onori, Mark Hoffman

Clemson University, Department of Automotive Engineering, 4 Research Dr., Greenville, SC 29607, USA

HIGHLIGHTS

G R A P H I C A L A B S T R A C T

- A parallel evaporator organic Rankine cycle Simulink[®] model is presented.
 Component models are calibrated and
- validated with experimental data.
 Integration and quasi-transient
- validation of the component models are given.
- Co-simulation of organic Rankine cycle and heavy-duty diesel engine models.
- Integrated model capability is demonstrated over a transient driving cycle.



ARTICLE INFO

Article history: Received 21 April 2017 Received in revised form 19 June 2017 Accepted 15 July 2017

Keywords: Waste heat recovery Organic Rankine cycle Dynamic finite volume heat exchanger modeling Heavy duty diesel engine Transient operation

ABSTRACT

This paper presents a dynamic organic Rankine cycle waste heat recovery (ORC-WHR) Simulink[®] model and an engine model for heavy-duty diesel applications. The dynamic, physics-based ORC-WHR system model includes parallel evaporators, flow control valves, a turbine expander, a reservoir, and pumps. The evaporator model contains an enhanced pressure drop model, which calculates pressure drop for each working fluid phase via a linear relation to the axial location inside each phase. The ORC-WHR component models parameters are identified over large range of steady state and transient experimental data, which are collected from an ORC-WHR system on a 13 L heavy-duty diesel engine. The component models are integrated into an entire system model and the boundary conditions, inputs and outputs for the individual models are described. A GT-POWER[®] engine model and its transient validation is presented. The speed and torque profiles of a long-haul, constant speed variable-load heavy-duty cycle are processed through the engine model to produce the exhaust and recirculated exhaust gas transient conditions relevant for the ORC model. The ORC-WHR system then simulated over these highly transient engine conditions. Overall, this paper provides detailed guidelines for ORC-WHR system modeling, model calibration, and component models integration.

© 2017 Elsevier Ltd. All rights reserved.

* Corresponding author. *E-mail address:* xbin@clemson.edu (B. Xu).

http://dx.doi.org/10.1016/j.apenergy.2017.07.038 0306-2619/© 2017 Elsevier Ltd. All rights reserved. Applied Energy 20 Contents lists availa Applied

2	0	4
1	h	
-	~	1

а	ath boundary of the discretized evaporator	BC	boundary condition
А	area [m ²]	TP	tail pipe
B, n	Blasius factors	EGR	exhaust gas recirculation
C_{n}	heat capacity []/kg K]	HTC	heat transfer coefficient
Ċ	constant of two-phase multiplier correlation	turb	turbine
d	diameter [m]	FRM	fast running model
f	friction factor		5
F	force [N]	Subscrip	ts and superscripts
G	mass flux [kg/s m ²]	f	working fluid
h	enthalpy []/kg]	J 147	wall
Н	height [m]	0	exposed and
H	enthalpy flowrate []/s]	v	vanor
I	momentum [kg m/s]	1	liquid
k	kth time step	i	ith discretized cell
LL.	length [m]	l in	inlet/unstream
m	mass [kg]	uu out	outlet
m	mass flow rate [kg/s]	out n	Dutiet
N	revolution speed [rpm]	p fm	friction
0	valve opening [%]	ji a	niction gravitation
n	pressure [Pa]	g	gravitation
P t	time [s]	exc	excitatige
т Т	temperature [K]	vap	saturated vapor
1	velocity $[m/s]$ internal energy $[1/k\sigma]$	sai	saturated liquid
u II	heat transfer coefficient []/kg K]	tp	two phase
11	dynamic viscosity [m ² /s]	5	single phase
V	volume [m ³]		hydraulic haat tuunafan aaaffaiant
v	vapor quality	U	
x X	Martinelli parameter	15	isentropic
7	space coordinate [m]	a	discharge
2	void fraction	0,	reference
Po	Peypolds number	viv	valve
r	ratio	JIOW	Ilow
l Dr	Prandtl number	sım	simulation
F1 Nu	Nusselt number	exp	experimental
nu	specific heat ratio	CW	cooling water
Y	density [kg/m ³]	c va	compressible volume a
р а	nartial derivative operator	<i>c v b</i>	compressible volume b
0	intersection angle between horizontal surface and flow	mix	mixed working fluid after junction
52	direction [radius]	HPP	high pressure pump
z	friction factor	FP	feed pump
ç	dupamie viegositu [lug m/s]	1P	tail pipe
μ	two phase multiplier	EGR	exhaust gas recirculation
ϕ	two-phase multiplier	Cond	condenser
		cross	cross or sectional surface
Abbrevia	ations	ритр	pump
ORC	organic Rankine cycle	turb	turbine
WHR	waste heat recovery	TurbByp	turbine bypass valve
HDD	heavy duty diesel	<i>TurbIn</i> turbine inlet valve	
CSVL	constant speed variable load	TPE vapVlv TP evaporator distribution valve	
MBM	moving boundary method	<i>EGREvapVlv</i> EGR evaporator distribution valve	
FVM	finite volume method		

1. Introduction

Nomenclature

In the past decade, waste heat recovery (WHR) techniques have gained a large amount of attention in the automotive industry, especially in heavy-duty truck applications [1–3]. It is reported that up to 45% of fuel energy is wasted as heat in a heavy duty vehicle [2]. Given such a large percentage of waste heat, WHR technology represents an attractive option for improved fuel economy and reduced CO_2 emission.

Popular WHR technologies include the thermoelectric generators, the turbo-compounding, and the organic Rankine cycle (ORC). Thermoelectric generators utilize the temperature difference between the exhaust gas and the thermoelectric material coolant to produce electricity [4–6]. These devices are compact and can be simply structured, but their thermal efficiency is limited by the low figure of merit value of existing thermoelectric materials. Turbocompounding combines the turbocharger with an electric generator or a crankshaft coupling, respectively, representing the naming convention of electrical versus mechanical turbocompounding [7–9]. Turbocompounding recovers a portion of enthalpy energy from the exhaust gas. After expansion in the turbocharger, the remaining waste heat exists in the form of low availability thermal energy that cannot be efficiently recovered by additional turbocompounding. Additionally, turbocompounding Download English Version:

https://daneshyari.com/en/article/4915846

Download Persian Version:

https://daneshyari.com/article/4915846

Daneshyari.com