## **ARTICLE IN PRESS**

#### Applied Energy xxx (2016) xxx-xxx



## **Applied Energy**

journal homepage: www.elsevier.com/locate/apenergy

# On the trade-off between aviation $NO_x$ and energy efficiency

### Konstantinos G. Kyprianidis\*, Erik Dahlquist

Future Energy Center, School of Business, Society and Engineering, Mälardalen University, Västerås 721 23, Sweden

#### HIGHLIGHTS

• A NO<sub>x</sub> emissions correlation for RQL combustors is derived; an approach for modelling LDI designs is also presented.

• Improving engine propulsive efficiency has a beneficial effect on NO<sub>x</sub> emissions at sea level.

• Improving engine thermal efficiency has a detrimental effect on NO<sub>x</sub> emissions for RQL combustors, but not for LDI designs.

• Future emissions certification legislation needs to become more stringent and comprehensive.

#### ARTICLE INFO

Article history: Received 15 August 2015 Received in revised form 8 November 2015 Accepted 3 December 2015 Available online xxxx

Keywords: NO<sub>x</sub> Performance Rich-burn Quick-quench Lean-burn combustor Gas turbine Lean direct injection Aircraft engine

#### ABSTRACT

This study aims to assess the trade-off between the ever-increasing energy efficiency of modern aeroengines and their NO<sub>x</sub> performance. The work builds on performance models previously developed to optimise the specific fuel consumption of future aero-engine designs. As part of the present work a simple and adaptable NO<sub>x</sub> emissions correlation for Rich-burn Quick-quench Lean-burn combustor designs is derived. The proposed model is computationally inexpensive and sufficiently accurate for use in aeroengine multi-disciplinary conceptual design tools. Furthermore, it is possible to adapt the correlation to model the NO<sub>x</sub> emissions of combustors designed for very aggressive future cycles. An approach to lean-burn combustor NO<sub>x</sub> emissions modelling is also presented. The simulation results show that improving engine propulsive efficiency is likely to have a benign effect on NO<sub>x</sub> emissions at high altitude; at sea-level conditions NO<sub>x</sub> emissions are particularly likely to reduce. Improving engine thermal efficiency however has a detrimental effect on NO<sub>x</sub> emissions from RQL combustors, both at high altitude and particularly at sea-level conditions. LDI combustor technology does not demonstrate such behaviour. Current legislation permits trading NO<sub>x</sub> emissions engine efficiency and hence reduce CO<sub>2</sub> emissions. If we are to reduce the contribution of aviation to global warming, however, future certification legislation may need to become more stringent and comprehensive.

© 2015 Elsevier Ltd. All rights reserved.

AppliedEnergy

#### 1. Introduction

Public awareness and political concern over aviation-induced pollution has increased substantially in recent decades, driving policy and technological developments. The Intergovernmental Panel on Climate Change (IPCC) [1] provides a good introduction to the impact of aviation induced emissions on the global atmosphere; the interested reader may refer to the latest synthesis report [2]. A good review on aero engine pollutant emissions, and an introduction to some of the technologies for reducing them, is given by Wulff and Hourmouziadis [3]. Mongia [4], Matthes et al. [5], Lieuwen and Yang [6] and Masiol and Harrison [7] provide a fresh perspective on the topic and a comprehensive summary of the latest technological developments.

\* Corresponding author. *E-mail address:* k.kyprianidis@gmail.com (K.G. Kyprianidis).

http://dx.doi.org/10.1016/j.apenergy.2015.12.055 0306-2619/© 2015 Elsevier Ltd. All rights reserved.

Overall, significant reductions in airliner fuel burn and associated CO<sub>2</sub> emissions have been achieved [8] in the past few decades. This has been realised primarily by reducing turbofan engine Specific Fuel Consumption (SFC). SFC is inversely proportional to both thermal and propulsive efficiency. Propulsive efficiency has been improved by increasing fan diameter and fan flow to reduce specific thrust (i.e. net thrust divided by mass flow). For very low specific thrust levels open rotor designs may be considered [9,10]. Thermal efficiency has been improved mainly by increasing the Overall Pressure Ratio (OPR) and High Pressure Turbine (HPT) rotor entry temperature  $T_{41}$  to the extent possible with current materials and design technologies. An alternative approach is the use of advanced intercooled cycles as documented by several researchers [11–18]. Intercooled-recuperated core cycles have also received significant attention [19-26]. For an extensive literature review on both core concepts the interested reader is referred to [27].



## **ARTICLE IN PRESS**

#### K.G. Kyprianidis, E. Dahlquist/Applied Energy xxx (2016) xxx-xxx

#### Nomenclature

AFR BPR CAEP CO <sub>2</sub> CRFD Comb. DLR DNS EINO <sub>x</sub> EIS EOR Exp. FPR h HD HPC HPT ICAO Id. IPC IPC IPT ISA LDI LES LPT LT LTO	Air to Fuel Ratio ByPass Ratio Committee on Aviation Environmental Protection carbon dioxide Computational Reactive Fluid Dynamics Combustor Deutsches Zentrum für Luft- und Raumfahrt (German Aerospace Center) Direct Numerical Simulation NO <sub>x</sub> Emissions Index (g NO <sub>x</sub> /kg fuel) Entry Into Service End Of Runway Exponent Fan Pressure Ratio Ambient humidity (kg H <sub>2</sub> O/kg dry air) Hot-Day High Pressure Compressor High Pressure Turbine International Civil Aviation Organization Ideal Intermediate Pressure Compressor International Standard Atmosphere Lean Direct Injection Large Eddy Simulation Low Pressure Turbine Inden and Take-Off cycle	NO $_x$ OPR P Ref. RANS RQL SL SLS SFC SFN T $T_{flame}$ $T_m$ TO TBC TOC $V_{id}$ W $\Delta$ 2 24 25 26 3 31 4 41 47	mono-nitrogen oxides Engine Overall Pressure Ratio total pressure (Pa) Reference Reynolds-Averaged Navier-Stokes Rich-burn Quick-quench Lean-burn Sea-Level Sea-Level Static Engine Specific Fuel Consumption (g/(kN s)) Engine Specific Thrust (m/s) total temperature (K) combustor flame temperature (K) metal temperature (K) Take-Off Thermal Barrier Coating Top Of Climb jet velocity from full expansion in an ideal convergent- divergent nozzle mass flow difference fan entry IPC entry IPC delivery HPC delivery combustor entry combustor delivery HPT rotor entry LPT entry temperature
LPT	Low Pressure Turbine	4	combustor delivery
	Long Term	41	HP1 rotor entry
LIU	Landing and Take-Off cycle	47	LP1 entry temperature
MCR	Mid-Cruise	8	core nozzle throat
MT	Medium Term	18	bypass nozzle throat
NEWAC	NEW Aero engine Core concepts		
п	pressure ratio split exponent		

Although  $CO_2$  emissions per passenger-kilometer have been decreasing the same cannot be said for  $NO_x$  emissions. Aggressive turbofan designs that reduce  $CO_2$  emissions – such as increased OPR and  $T_{41}$  designs – can increase the production of  $NO_x$  emissions due to higher flame temperatures resulting in less mixing air being available for emissions control. An important research question therefore rises:

# What is the trade-off between low $CO_2$ and $NO_x$ considering the influence of current emissions legislation?

For conceptual designs of more environmental friendly aero engines with advanced technologies, the need arises for sufficiently accurate models for predicting engine performance and pollutant emissions. Advanced engine performance models developed by the authors have been previously utilised for optimising aero-engine energy efficiency [27–30]. Although the optimisation results have been very promising little attention was given in these studies on the accurate prediction of gaseous pollutants other than  $CO_2$ .

Prediction models of gaseous emissions for aero gas turbine combustors typically need to focus on the following pollutants:  $NO_x$ , CO, unburned hydrocarbons and smoke. Lefebvre [31] describes thoroughly the formation mechanisms for these pollutants, focusing on the influence of various parameters such as temperature and pressure. Combustion and emissions prediction models can be divided broadly into the following categories [32]:

• Phenomenological (e.g. stirred reactor networks).

- 3-D CRFD RANS (Computational Reactive Fluid Dynamics, Reynolds-Averaged Navier–Stokes equations).
- 3-D CRFD LES (Computational Reactive Fluid Dynamics, Large Eddy Simulation modelling).
- Direct Numerical Simulation (DNS).

It is evident that, although direct numerical simulation is the most powerful of the above mentioned methods, the associated computational time and cost is prohibitive. Large eddy simulations offer a convenient computational trade-off between DNS and RANS, and have been used successfully for many years for studying turbulent combustion processes. A common disadvantage between all three analytical methods is the requirement for a large amount of input data (i.e. boundary conditions) that are not always readily available. Semi-empirical models are well suited for conceptual design of future aero-engine concepts, since only a limited amount of data is usually available at the beginning of such projects.

The latter constraint makes the implementation of the computationally more expensive phenomenological models, within an overarching conceptual design tool for advanced system analysis such as the ones utilised in [33–39], a fairly challenging task. For such tools, it is imperative that the different disciplines are considered at a reduced level of modelling complexity, and therefore semi-empirical models are the preferred choice.

It should be noted that developing robust and generic prediction models for  $NO_x$  emissions is not a trivial task. In the authors' view, gas turbine combustor design has for a long time been, and largely still is, characterised as a "black art"; many design principles are still based primarily on experimental observations and empirical

Semi-empirical.

Download English Version:

# https://daneshyari.com/en/article/4917084

Download Persian Version:

https://daneshyari.com/article/4917084

Daneshyari.com