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Multi-field coupling dynamic modeling and simulation of turbine test rig gas system



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ABSTRACT

On the basis of early research on the 38-component system, this paper extends the established finite volume model to the multi-field coupling numerical system which can describe flow, heat transfer, combustion and rotation, and conducts, based on the experiment, dynamic modeling and simulation research on the turbine test rig gas system which includes turbine and load. The comparison among the simulation results, test data and early simulation results indicates the 42-component system established by this paper has made improvements against many weaknesses of the Previous simulation in an allround way. Accordingly, it can be concluded that the case setting and algorithm improvement are effective. It is also found that the modeling of module with chemical reaction, the spool throttling modeling of various regulator valves, the modeling of the turbine characteristics and the modeling of wall heat transfer are four key factors which affect simulation accuracy, and that the coupling modeling of flow and combustion is the key factor which affects simulation stability.

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1. Introduction

The idea of modularization [1] is gradually formed to meet the demand of versatile system modeling. Its basic idea is firstly viewing the system as an assembly of some typical components which are called modules, secondly establishing numerical model of every module and encapsulating it as an independent function module, finally establishing numerical model of the whole system by combination of relevant modules according to special rules. As all components of the same type are described by one module, the modeling and simulation problem of all kinds of systems with different structures can be solved conveniently by computer. In the liquid propulsion system (LPS) simulation field, this idea is deemed to be put forward by A.P. Tishi and L.P. Gurova [2]. Since late 1980s, relevant researches have been evolving toward maturity and put into application in the form of simulation software [3–25]. Ref. [26] summarizes the relevant researches and points out that future improving direction in the aspect of algorithm will focus on more detailed and accurate modular modeling of typical component, and integration of simulation and optimization function for optimization application.

At the level of component research, the high-fidelity full-scale three-dimensional (3D) or two-dimensional (2D) modeling and simulation can be conducted by employing the leading CFD (Computational Fluid Dynamics) software tools (e.g. CFX, FLUENT) for many components of LPS. However, at the level of system research, that has not become the mainstream practice mainly because: for a transient complex system consisting of tens of or even hundreds of components, the CFD softwares

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Nomenclature	
٨	areas sortional area (m^2)
A	(1055-50)
л _{bmin}	critical cound velocity (m/c)
$u_{\rm cr}$	flow coefficient
C	flow coefficient of turbing stationary blade pozzle
C _{sb}	now coefficient of turbine stationary bidge nozzie specific heat at constant pressure $(1/(\log K))$
L_p	specific field at constant pressure $(j/(kg K))$
D _{TM}	turbine cascade average diameter (iii), $(D_{hub} + D_{tip})/2$
E f	mixture fraction
Jmix h	mixture indefioin
n Ma	much number
M.	load torque (N m)
M _m	turbine drive torque (N m)
m Ω	mass flow rate (kg/s)
m, Qm mr	mean mass mixture ratio
n.	rotate speed of rotor (r/min)
$n_{\rm rot}$	rotate speed of furbine (r/min)
P	nower (W)
n n.	static pressure and total pressure (Pa)
O_{m} nn	turbine flow capacity parameter
$O_{\rm u}$	volume flow rate (m ³ /s)
à	heat flux density per unit area (W/m^2)
grho	heat flux density per unit area from in-tube fluid to pipe wall (W/m^2)
grho2	heat flux density per unit area from wall to out-tube fluid (ambient atmosphere) (W/m^2)
Ŕ	specific gas constant (J/(kg K))
Re	Reynolds numbers
r	pipe-wall radial coordinate or radius (m)
r_{Q_m}	the mass-flow-rate ratio of oxidant to fuel flowing into combustion zone
S	surface area (m ²)
T, T _t	static temperature and total temperature, respectively (K)
T_{f_2}	fluid static temperature outside the pipe (ambient temperature) (K)
t	time (s)
u	fluid velocity in x direction (m/s)
$u_{\rm TM}$	neural-location circular velocity of turbine blade (III/S)
V MZ	volume (m)
vv	axial direction of nine (one-dimensional flow direction)
A No	coefficient of convective heat transfer from nine wall to out-tube fluid $(W/(m^2 K))$
v2 v	ratio of specific heat capacities of gas
1 E1 E2	blackness of pipe wall and ambient environment respectively
81, 0 <u>2</u>	system blackness
n	efficiency
λ	thermal conductivity (W/(m K))
λ	median-location circular velocity coefficient of turbine blade
π	circular constant
π_{nt}	turbine total pressure ratio
ρ	density (kg/m ³)
σ_0	blackbody radiation constant ($W/(m^2 K^4)$)
τ	valve relative opening
$\Omega_{ m T}$	turbine reaction degree
ω	rotational angular velocity (radians/s)
Subscrip	ts
ad	adiabatic
С	combustion zone
ektexine	e external surface of pipe wall
f	fluid
f	fuel
1	serial number of a axial-direction grid

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