

A review of experimental data and heat transfer correlations for parallel flow of alkali liquid metals and lead-bismuth eutectic in bundles



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HIGHLIGHTS

- Comprehensive review of convection heat transfer of alkali liquid metals and LBE in bundles of bare heated tubes in a triangular lattice.
- Compiled database, for wide ranges of P/D and Pe, is used to develop Nu correlation for alkali metals.
- The alkali metals' Nu correlation is in good agreement with the compiled data for LBE.

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ABSTRACT

A comprehensive review is performed of the reported experimental data on convection heat transfer for parallel flows of the alkali liquid metals of sodium, NaK-44, NaK-56, and NaK-78 alloys, and liquid lead-bismuth eutectic (LBE) in bundles of uniformly heated bare tubes in a triangular lattice at $Pe = 4\text{--}3074$. The performed experiments by various investigators have employed either a heat exchanger or hexagonal and cylindrical bundles of 7–37 heated tubes with $P/D = 1.06\text{--}1.95$. The compiled experimental database of 746 Nusselt number values for Na and various NaK alloys is used to develop the following continuous correlation:

$$Nu = [10.7(P/D) - 7.1] + 0.024[1 - e^{-10.4((P/D)-1)}]Pe^{0.85}$$

For the entire ranges of P/D and Pe values in the experiments, this correlation is in good agreement, within $\pm 15\%$, with the compiled Nu data. The compiled Nu database for LBE flows in bundles of bare heated tubes with grid spacers, has 205 values for $P/D = 1.33\text{--}1.80$ and $Pe = 211\text{--}3049$. The present Nu correlation for alkali liquid metals agrees with the LBE data to within $\pm 20\%$. This agreement suggests that the proposed Nu correlation for alkali liquid metals in bundles of bare tubes may also be used to calculate Nu for LBE.

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1. Introduction

Liquid metals are being used for cooling and heating in many engineering systems. Examples are solar thermal power, fast-spectrum small modular, large commercial, and space fission nuclear reactors, high temperature heat exchangers, and superheated steam generators (Chang et al., 2008; Dieckamp, 1967; El-Genk and Palomino, 2015; Faust, 1972; IAEA, 2006, 2013; Le Coz et al., 2011; Mason et al., 2008; Nikitin et al., 2000; Schriener

and El-Genk, 2013). Liquid metals of interest include sodium (Na), potassium (K), lithium (Li), sodium-potassium alloys (NaK), molten lead (Pb), and molten lead-bismuth eutectic (LBE). The primary advantages of liquid metals, compared to gases (e.g. helium or helium-xenon) and non-liquid metal fluids, such as water, are the high thermal conductivity, and the low dynamic viscosity and specific pumping power. In addition, the low vapor pressure of liquid metals makes it possible to operate at high temperatures at low or near atmospheric pressure. Nonetheless, the thermophysical properties of the different liquid metals vary widely. Fig. 1a–d compare the properties of alkali liquid metals of interest and mercury (Hg), only for a historical perspective (IAEA, 2008; OECD, 2015). Although Hg had routinely been used in the past in many convection heat transfer experiments with tubes and

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Nomenclature

A	cross sectional flow area (m ²)	Pr	Prandtl number ($\dot{m} C_p/k$)
ARD	absolute relative difference	Re	Reynolds number ($\dot{m} D_e/\mu A$)
C _p	specific heat capacity (J/kg.K)	T	temperature (K)
D	tube outer diameter (m)	T _b	bulk temperature (K), $(T_{ex} + T_{in})/2$
D _e	equivalent hydraulic diameter (m), $4A/WP$	TC	thermocouple
D _{e,b}	equivalent hydraulic diameter for an entire bundle (m), $4A_b/WP_b$	WP	wetted perimeter (m)
D _{e,s}	equivalent hydraulic diameter for a subchannel in a hexagonal bundle of bare tubes (m), $D \left[\frac{2\sqrt{3}}{\pi} (P/D)^2 - 1 \right]$	<i>Subscripts</i>	
D _{ff}	hexagonal bundle flat-to-flat (m)	b	bundle, bulk
ERH	electric resistance heater	Corr	correlation
FD	fully developed	ex	exit
HEX	heat exchanger	Exp	experiment
h	heat transfer coefficient (W/m ² .K)	ff	flat-to-flat
k	thermal conductivity (W/m.K)	h	heated
L	tube length (m)	i	index number
LBE	lead-bismuth eutectic alloy	in	inlet
<i>dotm</i>	mass flow rate (kg/s)	s	subchannel
n	number of rods or tubes in a bundle	<i>Greeks</i>	
N _{rings}	number of rings of heated tubes in a hexagonal bundle	α	flow area correction factor for the bundle (m ²), $(A_b - nA_s)$
N	number of experimental Nu values compiled	β	wetted perimeter correction factor for the bundle (m), $(WP_b - nWP_s)$
NaK	sodium-potassium alloy	δ	ratio of hydraulic diameters of the bundle and the subchannel, $(D_{e,b}/D_{e,s})$
NL	not listed	ε	distance between shroud and outer ring of tubes in hexagonal bundle (m)
Nu	Nusselt number for a subchannel, $(hD_{e,s}/k)$	μ	dynamic viscosity (kg/m.s)
Nu _b	Nusselt number for an entire bundle, $(hD_{e,b}/k)$	ρ	density (kg/m ³)
OEB	overall energy balance		
P	pitch (m)		
P/D	pitch-to-diameter ratio		
Pe	Peclet number for a subchannel, $(\dot{m} D_{e,s}/A.C_p.k)$		
Pe _b	Peclet number for an entire bundle, $(\dot{m} D_{e,b}/A.C_p.k)$		

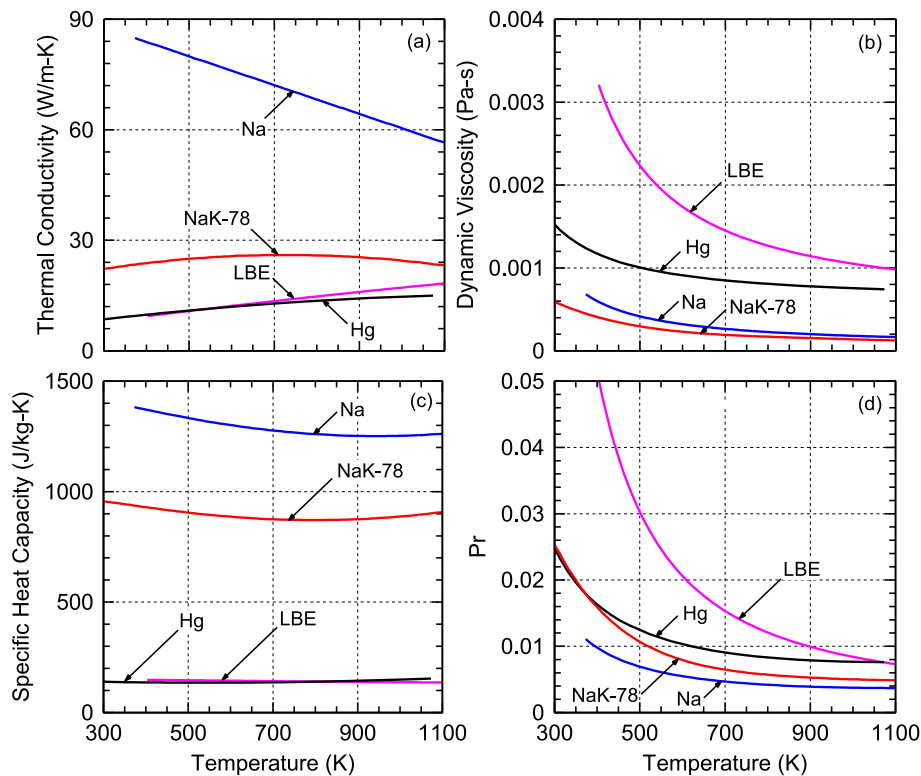


Fig. 1. Comparisons of thermophysical properties of liquid metals (IAEA, 2008; OECD, 2015).

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