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European Journal of Operational Research 000 (2016) 1-10



Contents lists available at ScienceDirect

European Journal of Operational Research



journal homepage: www.elsevier.com/locate/ejor

Production, Manufacturing and Logistics

Two new stochastic models of the failure process of a series system

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ARTICLE INFO

Article history: Received 6 September 2015 Accepted 19 July 2016 Available online xxx

Keywords:

Non-homogeneous Poisson process (NHPP) Geometric process (GP) Generalised renewal process (GRP) Superimposed renewal process Virtual component

ABSTRACT

Consider a series system consisting of sockets into each of which a component is inserted: if a component fails, it is replaced with a new identical one immediately and system operation resumes. An interesting question is: how to model the failure process of the system as a whole when the lifetime distribution of each component is unknown? This paper attempts to answer this question by developing two new models, for the cases of a specified and an unspecified number of sockets, respectively. It introduces the concept of a virtual component, which corresponds to the part of the system that is replaced upon system failure. It then discusses the probabilistic properties of the models and methods for parameter estimation. Based on six datasets of artificially generated system failures and a real-world dataset, the paper compares the performance of the proposed models with four other commonly used models: the renewal process, the geometric process, Kijima's generalised renewal process, and the power law process. The results show that the proposed models outperform these comparators on the datasets, based on the Akaike information criterion.

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1. Introduction

1.1. Background

Modelling the failure processes of technical systems has attracted much attention from reliability researchers. There exist many papers that attempt to develop statistical models for characterising the failure process of a system (see, Baxter, Kijima, and Tortorella (1996); Cox and Lewis (1966); Dorado, Hollander, and Sethuraman (1997); Doyen and Gaudoin (2004, 2011); Duane (1964); Kijima and Sumita (1986); Lam (1988); Wu and Zuo (2010), for example). However, much of this existing research assumes that the systems are equivalent to one-component systems. Such an assumption is restrictive and unrealistic as real-world systems normally consist of very many components. In addition, in the real world, the lifetime distribution of each component may not be estimable for various reasons; for example, data on real systems often contain little or no information about the failure processes of individual components. Hence, there is a need to develop new, simple (few parameters) and elegant (richly applicable) failure process models for multi-component systems. This is the purpose of this paper.

* Corresponding author. E-mail addresses: s.m.wu@kent.ac.uk (S. Wu), p.a.scarf@salford.ac.uk (P. Scarf). Before we introduce our models, we define repair concepts, and two important models of imperfect repair.

1.2. Definitions

In reliability mathematics, the effect of maintenance upon failure of an item is typically categorised into:

- *Perfect repair*, in which maintenance restores the condition of a failed item to an "as good as new" status; for example, a failed item is replaced with a new identical one. The renewal process is a widely used model for the failure process of items under perfect repair (Ross, 1996).
- *Minimal repair* (see, Cox and Lewis (1966); Duane (1964), for example), in which maintenance restores a failed item to its state immediately prior to failure. The operating state of an item after minimal repair is often called "as bad as old" in the literature. The only model of minimal repair available in the literature is the non-homogeneous Poisson process (NHPP).
- Imperfect repair, in which maintenance restores a failed item to a status somewhere between "as good as new" and "as bad as old". Many models, including the geometric process (GP) and its variants (Lam, 1988; Wang & Pham, 1996; Wu & Clements-Croome, 2006), the generalised renewal process models (GRP) (Doyen & Gaudoin, 2004; Kijima, 1989; Kijima & Sumita, 1986), and the reduction of failure hazard models

http://dx.doi.org/10.1016/j.ejor.2016.07.052 0377-2217/© 2016 Elsevier B.V. All rights reserved.

Please cite this article as: S. Wu, P. Scarf, Two new stochastic models of the failure process of a series system, European Journal of Operational Research (2016), http://dx.doi.org/10.1016/j.ejor.2016.07.052

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(Doyen & Gaudoin, 2004), have been developed for modelling imperfect repair.

The particular models themselves are defined as follows.

- *The geometric process*: Following Lam (1988), given a sequence of non-negative random variables $\{X_k, k = 1, 2, ...\}$, if they are independent and the cumulative distribution function of X_k is given by $F(a^{k-1}x)$ for k = 1, 2, ..., where *a* is a positive constant, then $\{X_k, k = 1, 2, ...\}$ is called a geometric process (GP). The GP has attracted a lot of attention in the literature (see, Wu and Scarf (2015); Zhang, Gaudoin, and Xie (2015), for example).
- The generalised renewal process: Kijima and Sumita (1986) and Kijima (1989) introduce two types of repair models, type I and type II, using the concept of virtual age. These models distinguish between the age of the system, which is the time elapsed since the system was new (usually at time t = 0), and the virtual age of the system, which accounts for the current health of the system when compared to a new system. The two models assume $V_k = V_{k-1} + q_k X_k$, and $V_k = q_k (V_{k-1} + X_k)$, respectively, where V_k is the virtual age of the system immediately after the *k*th repair, X_k is the operating time of the system since the *k*th repair, and $0 \le q_k \le 1$. The models are often referred to collectively as the generalised renewal process (GRP). In the type I model, if $q_k = 0$, then the *k*th repair is a perfect repair; if $q_k = 1$, then the *k*th repair, a minimal repair.
- The renewal process, the superimposed renewal process, and the homogeneous Poisson process (HPP): Consider a series system consisting of *m* sockets into each of which there are inserted non-repairable independent components, and whenever a component fails, the system fails, and the failed component is replaced with a new identical one and system operation resumes. Then the number of failures occurring at each socket is a renewal process and the number of failures of the series system as a whole forms a superimposed renewal process (Høyland & Rausand, 2009). In general, the superimposed renewal process is not a renewal process, unless the individual renewal processes are homogeneous Poisson processes (Drenick, 1960). When both the number of components in the system is large and the operation time of the system is large then the superimposed renewal process behaves approximately as a homogeneous Poisson process (HPP) (Høyland & Rausand, 2009). The HPP is a counting process with constant intensity function (or rate of occurrence of failures).
- *The non-homogeneous Poisson process (NHPP)*: This process generalises the HPP and has a time-varying intensity function.

1.3. Motivation for our models

The failure process models such as the GRP (Gilardoni, Toledo, Freitas, & Colosimo, 2015), GP (Wu & Clements-Croome, 2006) and NHPP (Asfaw & Lindqvist, 2015) do not distinguish the effect of maintenance upon failure of different components in the system. Thus, such models effectively consider the system as a onecomponent system. The use of these models is typically justified by the fact that in practice failure data are scarce, and so, even if one could model each component in the system individually and plan maintenance accordingly, such an approach would not be applicable.

Furthermore, appealing to the asymptotic behaviour of the superimposed renewal process as justification for the use of an HPP in an application is questionable because in practice typical systems are relatively young and failures are rare. Using an NHPP with an increasing intensity function such as the power-law process (Høyland & Rausand, 2009) overcomes this system age issue. However, the NHPP (and HPP for that matter) supposes repair is minimal. At the other end of the spectrum, the renewal process

supposes the entire system is replaced on failure so that repair is perfect.

Capturing imperfect repair with the GP or the GRP presents further difficulties. The GP implicitly assumes that the times between failures are either stochastically increasing or stochastically decreasing, which is not always true for the failure process of a series system. For example, if all the components in the series system have increasing hazard functions, then a replacement of a failed component improves the reliability of the system; on the other hand, operating times between adjacent replacements of the system are stochastically decreasing. Hence the times between failures of the system may be neither stochastically increasing nor stochastically decreasing. Furthermore, in the limit (large number components at large t) the superimposed renewal process behaves as a homogeneous Poisson process, which cannot be captured by the GP.

The GRP overcomes the issue of stochastically increasing or decreasing times between failures by allowing the repair effect parameter to vary. However, if indeed q_k vary with k, then typically they must be estimated using a very limited number of failure observations. As a result, the models will be poorly estimated. If the q_k are assumed equal for all k, then the GRP will not capture the fact that the effects of replacement of failed components of different types are different.

1.4. Our proposed solution

In summary then, the existing models of the failure process of a multi-component system are restrictive. Furthermore, limited failure data make it impossible to estimate either the lifetime distribution of each component in a system or a model for a system as a whole with many parameters. We must therefore seek simple and elegant models for a system as a whole that can be fitted using a limited number of failure observations. Our contribution develops two new classes of such models for a series system with non-identical components.

In these models, the failure process of the system is regarded as equivalent to the failure process of a system consisting of a component, called the virtual component, in its socket and the remainder of the system, called the virtual sub-system (VSS). Upon a failure of the system, we suppose that the virtual component is replaced and the remainder of the system is either not maintained (equivalently minimally repaired) or subject to imperfect repair. In reality, one can contend that at a repair, the change in system reliability is at least as big as if the most reliable component had been replaced. Broadly speaking, replacement of the virtual component upon system failure captures this notion.

It should be noted then that in this paper, we distinguish three systems: i) the *real system*, that is, the reality, e.g. a manufacturing cell, a traction motor, a wind turbine, a compressor; ii) the *system*, that is, the mathematical model of the system, e.g. a series system with a number of non-repairable, non-identical components; and iii) the *virtual system* (VS), consisting of a virtual component (VC) and a virtual sub-system (VSS).

In our first model (Model I) the number of sockets in the series system is not specified. In our second (Model II) the number of sockets in the series system is *m*. The distinguishing features of the two models are discussed in detail later in the paper. The key concept, and a contribution of this paper, is the notion of the virtual component. Through this notion, our models capture not only that a repair effect is neither as good as new nor as bad as old but also that systems comprise distinct, typically non-identical components.

The paper considers the scenarios where the lifetime distribution of each component is neither known nor knowable for various reasons. For example, if the number of system failures is large but

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