



# Interwire wear and its influence on contact behavior of wire rope strand subjected to cyclic bending load

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## ABSTRACT

The present study establishes a solving model for analyzing the interwire wear evolution of a wire rope strand subjected to cyclic bending load, in which the frictional contact and sliding between the wires are considered simultaneously. A wear experiment between the wires is conducted to study the wear behavior of the wires. Meanwhile, the proposed model is verified experimentally. Then the interwire wear and its effect on the contact behavior of the strand are analyzed. The results show that the interwire wear only happens on the side further from the curvature center of the bended strand than its neutral layer, and no wear happens when the wires are apart from each other or the interwire slippage is zero. As the wear process goes on, the wear region extends only along the normal direction of the core-wire contact line, and the maximum wear depth occurs at the middle position between the neutral layer and the furthest location from the curvature center. The contact pressure is distributed uniformly along the normal direction of contact line, but a significant stress concentration and local deformation happen at the position furthest from the curvature center of the bended strand.

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## 1. Introduction

A wire rope is widely used in building, bridge, shipping, port and mining industries due to its high strength, good flexibility, impact resistance, stable operation and noiselessness. The wire rope is frequently loaded by tension, torsion and bending load in applications, which unavoidably results in contact and friction between the wires. Axial load and bending load in a simple straight wire rope strand bring about interwire pivoting and interwire sliding, respectively [1]. The interwire friction usually has little influence on the capability of the wire rope strand which is under the axial load, but its effect on the wire rope twisted around a sheave or drum cannot be ignored [2]. Particularly in periodic bending load conditions, long-time interwire friction and reciprocating slippage contribute to wire wear, which results in stress concentration and further the fracture of the wire rope. Therefore, it is of a great significance to conduct an in-depth study on the interwire wear mechanism to improve the design of wire ropes.

In the past years, some studies have been conducted on the friction and wear of wire ropes, most of which were conducted experimentally. For example, Rigde et al. [3] measured the strain of the wire rope caused by a periodic bending load. And their work

shows that the strain amplitude has an important influence on the fatigue of the rope. A series of experiments conducted by Harris et al. [4,5] on interwire frictional wear show that there exists a linear relation between the abrasion loss and contact load, that abrasion-caused damage is found at contact zone edge, and that wear and bending stress of the wire rope leads to crack occurrence and ultimately causes the fracture failure. To avoid this failure, the lubrication on the wire rope was also studied. The experiment on wear performance of a wire rope from McColl et al. [6] in different lubricating conditions shows that both oil lubrication and grease lubrication effectively reduce the friction coefficient of the wire rope, especially under the lubrication condition with additive graphite. Zhang et al. [7] reported experimentally that there exists an inverse ratio between the fatigue life, wearing depth, wearing-in period and load, and that an increased contact load induced three-body wear. Cruzado et al. [8,9] measured the wear volume of steel wires with a profilometer at different contact loads, wear distances and contact angles. And they concluded that the friction coefficient of the wire rises as the contact load and wear reciprocating distance increase, while the contact pressure and wear resistance decline as the wire intersection angle decreases under a certain contact load. Studies by Xu et al. [10] on the wear of the wire rope shows that acid medium can augment the interwire slip and the wear scar depth in this condition compared with dry friction environment. Further, Wang et al. [11–13] assessed the wear of steel wires in different lubrication conditions.

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**Nomenclature**

$A_c$	Contact region between central and outside wires	$p$	Contact pressure
$\bar{A}_2$	Cross-sectional area of deformed outside wire	$R_1, R_2$	Initial radii of central and outside wires
$E^*$	Reduced Young's modulus	$\bar{R}_1, \bar{R}_2$	Final radii of central and outside wires in deformed state
$E_1^*, E_2^*$	Composite Young's moduli of central and outside wires	$\bar{R}_{1y_c}, \bar{R}_{2y_c}$	Radii of surface curvature of central and outside wires along $y_c$ direction
$e_x, e_y, e_z$	Cartesian coordinates	$r_{h2}$	Helical radius of outside wire centerline
$G, G'$	Components of bending moment on outside wire's cross-section	$\bar{r}_{h2}$	Helical radius of deformed outside wire centerline
$G_u^p$	Green's functions of normal pressure for elastic deformation	$\bar{r}_{hc}$	Helical radius of deformed nominal contact line
$G_u^s$	Green's functions of shear stress for elastic deformation	$S$	Accumulated sliding distance
$H$	Twist moment on outside wire's cross-section about $z$ axis	$T$	Tensile force along $z$ direction
$h_c$	Core-wire contact clearance	$u$	Total deformation of core-wire contact
$h_i$	Initial clearance between central and outside wires	$u_1, u_2$	Deformations of central and outside wires along $y_c$ direction
$h_w$	Wear depth	$W_p$	Total planimetric wear of central and outside wires
$h_{w0}$	Total wear depth of central and outside wires at core-wire contact line	$X, Y, Z$	Components of external line load per unit length of outside wire centerline
$I_c$	Influence coefficient of contact pressure for elastic deformation	$X_c, Y_c, Z_c$	Line loads per unit length of core-wire contact line
$i_n$	Number of nominal wear cycles	$x, y, z$	Normal, binormal and tangential directions at a point on outside wire centerline
$K, K', \Theta$	Components of external moments per unit length of outside wire centerline	$y_c, z_c$	Tangential and normal directions of core-wire contact line
$k_l$	Length ratio of nominal contact line and outsider wire centerline at deformed state	$\alpha_2$	Helical angle of undeformed outside wire
$k_w$	Coefficient of wear	$\bar{\alpha}_2$	Helical angle of deformed outside wire
$L_s$	Relative sliding distance between central and outside wires	$\bar{\alpha}_c$	Helical angle of nominal core-wire contact line
$l$	Projection length of outside wire centerline	$\Delta N_w$	Number of wear cycles per nominal wear cycle
$l_p$	Initial lay length of wire rope strand	$\delta$	Total contact deformation due to core-wire contact
$\bar{l}_p$	Lay length of deformed strand	$\delta_1, \delta_2$	Contact deformations of central and outside wires
$l_s$	Length of outside wire centerline	$\kappa$	Bending curvature
$N, N'$	Components of shearing force on outside wire's cross-section	$\kappa_2, \kappa'_2, \tau_2$	Components of curvature and twist of outside wire centerline before deformation
$N_w$	Total wear cycle	$\bar{\kappa}_2, \bar{\kappa}'_2, \bar{\tau}_2$	Components of curvature and twist of outside wire centerline after deformation
		$\mu_e$	Equivalent shear modulus
		$\nu$	Poisson's ratio of wires
		$\xi_1, \xi_2$	Tensile strains of central and outside wires
		$\phi$	Angle position of outside wire centerline relative to strand axis

In addition, numerical approaches have been used in some studies to simulate the wear evolution of the wire rope. Warburton and Bradford [14] presented a method to compute the volumes of the intersections of worn cylinders, according to the geometrical parameter of the wear scars. Based on the experimentally obtained coefficients of friction and wear, McColl et al. [15] realized a numerical solution of wear by combining of the modified Archard's wear model with a finite element software. They conducted the solution through a progressive loading way and also put forward an optimization method in decreasing computing time. Cruzado et al. [16–18] analyzed the wear of wires at different intersection angles by using a finite element method and wear model, and verified the numerical results experimentally. Johansson [19] studied the evolution of contact pressure in frictional wear process, and found that the contact pressure changes as the volumetric wear increases. And the work by Argatov et al. [20] shows that the influence of the contact pressure on the wear coefficient should be considered. Argatov and Tato [21] made a comparison between sliding wear solution obtained by an asymptotic model and that obtained by finite element method. Wang et al. [22] estimated the fatigue life of a steel wire and found that the structural location and material property of the wire exert a significant influence on its stress distribution and fatigue life in the finite element analysis of fretting wear evolution of the wire. Wang et al. [23] studied the crack initiation in a wear

simulation of wire and found that the crack is liable to be found at the trailing edge.

Studies on the tribological performance of wire rope have been made so far, most of which were conducted experimentally. However, experimental studies are time-consuming and costly. And the local performances, such as the interwire contact pressure and deformation, are difficult to be obtained by experiments. As to the reported numerical works about wear of the wire rope, the interwire contact is usually studied through simplified point contact dealings. This is not completely in accordance with the real contact situation of wires in the wire rope, such as the helical line contact between the central and outside wires in a wire strand. Additionally, there are only few theoretical researches about the interior frictional wear of the cyclically bended wire rope, but the simultaneous consideration of the behaviors of bending, interwire contact and wear has not been conducted in these researches. To accurately evaluate the rope performances, the above bending, interwire contact and wear under the helical wire contact should be studied, which is helpful to improve the service performance of the wire rope.

With the consideration of factors including interwire friction, contact and wear, the present study establishes a solution model of frictional wear for a wire rope strand subjected to a cyclic bending load based upon the thin rods theory, elastic contact

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