#### Separation and Purification Technology 186 (2017) 117-124

Contents lists available at ScienceDirect

Separation and Purification Technology

journal homepage: www.elsevier.com/locate/seppur

## Techno-economic feasibility analysis on carbon membranes for hydrogen purification

### Xuezhong He

Department of Chemical Engineering, Norwegian University of Science and Technology, NO-7491, Trondheim, Norway

#### ARTICLE INFO

Article history: Received 20 February 2017 Received in revised form 19 May 2017 Accepted 19 May 2017 Available online 20 May 2017

Keywords: Biomass Hydrogen purification Carbon membranes Process simulation Cost estimation

#### 1. Introduction

Hydrogen production from biomass is the most promising scenario due to the waste minimization issue and the demands for the sustainable development. The hemoheterotrophic ("dark") fermentation deserves particular interests due to the advantages of high bacterial growth rate, hydrogen production rate, low energy demands, minimal pollution generation, no oxygen limitation problems and low capital costs for at least small-scale production facilities [1]. Dark fermentation H<sub>2</sub> production (instead of using fossil fuel-like steam methane reforming) provides a great opportunity for H<sub>2</sub> generation, but the process usually produces a humidified gas containing H<sub>2</sub> and CO<sub>2</sub> where hydrogen content normally ranges between 35 and 65 (vol.)%, and may also contain volatile organic compounds (VOC), H<sub>2</sub>S and NH<sub>3</sub> [1]. H<sub>2</sub> purification from this gas stream requires novel separation technologies. The existing technologies for H<sub>2</sub> purification are pressure swing adsorption (PSA), cryogenics, palladium (Pd) membranes [2-4]. Conventional PSA or cryogenics will not be suitable for small scale H<sub>2</sub> productions from fermentation processes due to the expected high costs. Even though the palladium membranes have already been commercialized for  $H_2$  purification such as  $H_2$  Pure<sup>M</sup> and HYSEP, the membrane production cost is still high and the lifetime is relatively short due to the H<sub>2</sub> embrittlement, which leads to a high capital expenditure (CAPEX). Moreover, the low processing temperature in a fermentation process will cause membrane

#### ABSTRACT

 $H_2$  production from a biomass fermentation process provides a great opportunity for green and sustainability economy compared to use fossil fuels (e.g., steam methane reforming process), but the process usually produces a humidified gas containing 35–65 (vol.%)  $H_2$  and 40–50 (vol.%) CO<sub>2</sub>. A novel, energy efficient two-stage carbon membrane system for  $H_2$  purification based on the combination of  $H_2$  selective carbon molecular sieve membranes in the first stage and CO<sub>2</sub> selective carbon membranes in the second stage was proposed. The concept is the first unique technology providing a low  $H_2$  purification cost <1 \$/kg H<sub>2</sub> produced at a feed pressure of 20 bara based on process simulation and cost estimation. The produced high purity CO<sub>2</sub> (>95 vol.%) and H<sub>2</sub> (>99.5 vol.%) can be integrated into a gasification reformer and Fischer-Tropsch reactors to improve the biodiesel productivity from biomass.

© 2017 Elsevier B.V. All rights reserved.

cracking due to the Pd-H two phases in this regime (typically <200 °C) that differ considerably in their lattice constant [5] when no pre-heating employed. Some literature has already reviewed the status of different polymeric membranes for hydrogen purification [6-9]. The issues and challenges with gas separation membranes to be applied for the concentration of fermentatively produced H<sub>2</sub> gas has been reviewed recently by Bakonyi et al. [6]. Li et al. compared the H<sub>2</sub>-selective and CO<sub>2</sub>-selective membrane materials and processes, and pointed out the future direction on the development of energy-efficient membranes [7]. With respect to the non-porous polymeric and mixed matrix membranes, it is guite challenging to achieve a high H<sub>2</sub> purity (>99%) requirement with low selectivity (<10) [6,10–13]. Moreover, the composition of the biohydrogen gas mixture, in particular its impurity (e.g., H<sub>2</sub>S) content was found to significantly influence the polymeric PDMS membrane performance reported by Bakonyi et al. [14]. They also pointed out that polymeric membranes were mostly tested under ideal laboratory conditions in the literature though in reality, the hydrogen generated by fermentation process is a part of a complex biogas stream, leading to the potential differences in the modules behavior. A hybrid polymeric membrane/ absorber system might be a solution to achieve the separation requirement for biohydrogen purification reported by Bakonyi et al. [15], but the process complexity and economic feasibility should be further investigated. The above described challenges direct to the development of an alternative membrane material with high H<sub>2</sub>/CO<sub>2</sub> selectivity and good chemical stability exposed to the impurities (e.g., H<sub>2</sub>S) which are usually existed in the raw





Separation EPurification Technology

E-mail address: xuezhong.he@ntnu.no

biohydrogen gas mixture, and can bring down the H<sub>2</sub> purification cost, and potentially expand the H<sub>2</sub> production from new fermentation processes.

Carbon membranes have great advantages on their mechanical and chemical stabilities when exposed to a high pressure and/or a high temperature process, and the performance can exceed the Robeson upper bound (2008) based on the molecular sieving transport mechanism, and reach the industrial attractive region [16]. Carbon membranes possess ultramicroporous structure, which are mainly prepared by the carbonization from polymeric precursors such as cellulose derivatives [17-20], polyimide [21-25], and polyacrylonitile (PAN) [26]. By carefully controlling the pyrolysis conditions, the pore size of the produced carbon materials can be well tailored at nanoscale, and to separate the gas molecules which are much alike in the size (molecular sieving). Moreover, the surface properties of carbon membranes can also be modified to present a selective surface flow (SSF) mechanism where more condensable gas like CO<sub>2</sub> has a high permeance compared to the less/no condensable gas of H<sub>2</sub>. Both molecular sieve and selective surface flow carbon membranes provided great potentials for selected gas separations (e.g., CO<sub>2</sub>/CH<sub>4</sub> [27,28], hydrocarbon separation [24,29]). In addition, carbon membranes are also expected to tolerate the impurities (e.g., H<sub>2</sub>S) when exposed to a fermentation gas stream. This statement is based on experience achieved with a carbon membrane pilot tested at a biogas plant in Southern Norway [30]. Thus, the feasibility of carbon membranes for purification of H<sub>2</sub> produced from new fermentation processes was studied in this work. An energy efficient two-stage carbon membrane system was designed to achieve the separation requirement for hydrogen purification from a fermentation process without combining with other separation technique.

#### 2. Carbon membranes for H<sub>2</sub>/CO<sub>2</sub> separation

#### 2.1. Carbon molecular sieve membranes

Lie et al. reported that  $H_2/CO_2$  separation used cellulosic-based carbon molecular sieving membranes [31]. The metal added carbon membrane, especially MgO-carbon membrane showed a high  $H_2/CO_2$  selectivity of 81 with a  $H_2$  permeance of 0.05 m<sup>3</sup>(STP)/ (m<sup>2</sup> h bar). It was worth noting that results were reported at 30 °C, and the membrane performance of both  $H_2$  permeance and  $H_2/CO_2$  selectivity are expected to increase at higher operating temperature (e.g., 100–150 °C). For the smaller gas molecules (e.g.,  $H_2$ ), the influence of temperature on permeation (diffusion, activated transport) is more significant compared to the CO<sub>2</sub> molecules due to a reduction of CO<sub>2</sub> solubility coefficient at higher temperature. Thus,  $H_2/CO_2$  selectivity are expected to increase with temperature. However, due to the challenges on module sealing at higher operation temperature, the carbon membrane system is usually recommended to be operated at <200 °C.

#### 2.2. SSF carbon membranes

The concept behinds the selective surface flow (SSF) carbon membranes is that when operated at a lower temperature (<20 °C), the larger and more condensable gas molecules (e.g., CO<sub>2</sub>) will adsorb on the pore walls, and "flow" through the membranes, which will result in a reduced pore size and eventually hinder the smaller and more inert molecules (e.g., H<sub>2</sub>) to transport through the membranes. The separation will thus depend on the critical temperature (T<sub>crit</sub>, high T<sub>crit</sub> means more condensable) of gas component [32], which is specially suitable for the 2nd stage membrane unit. This separation method was first patented by Air

Products & Chemicals Inc. in early 90'ies, while later Carbon Membranes Ltd. in Israel also documented the excellent separation performance of their self-supported hollow fibers for various gas mixtures. They used (chemical vapor deposition (CVD) for pore adjusting (tailoring with oxidation) after the pyrolysis. The company had to close down for reasons not discussed here. The importance of process conditions such as pressure and temperature for a SSF separating membrane was reported by K. Vennes [33] - their focus was separation of propane (T<sub>crit</sub> = 96.7 °C) from propene or H<sub>2</sub>. Thus, low temperature and higher pressure will favour the permeation. Moreover, Trinh et al. reported the CO<sub>2</sub> permeation through a carbon membrane by molecular modelling at various temperatures [34] – they documented that an adsorbed layer of CO<sub>2</sub> on the pore wall was formed. The experimental data of the SSF carbon membranes reported by Paranjape et al. [35] was used as simulation basis in this work.

#### 3. Process concept design

#### 3.1. Process description and simulation basis

The combination of biomass gasification with Fischer-Tropsch (FT) synthesis is designated as biomass-to-liquids (BTL). Nowadays, the main objective of the research and development projects on BTL is to produce the second generation bio-fuels by biomass gasification combined with FT synthesis [36]. In this work, the FT synthesis process integrated with carbon membrane unit for  $H_2/CO_2$  separation was designed to provide an alternative route for the production of transportation fuels (biodiesel) from biomass as illustrated in Fig. 1. The humidified gas stream produced from a biomass dark fermentation process mainly contains H<sub>2</sub> and CO<sub>2</sub> where hydrogen content usually ranges from 35 to 65 (vol.)%. The H<sub>2</sub> gas stream was then fed into a carbon membrane unit for H<sub>2</sub>/CO<sub>2</sub> separation. Moreover, biomass was also fed into a gasification reformer to produce syngas. Part of the captured high purity CO<sub>2</sub> (>95 vol.%) from the retentate stream in the membrane unit was sent to the gasification reformer to shift reaction to left side and improve the CO productivity. While the permeate high purity (>99.5 vol.%) H<sub>2</sub> stream from the carbon membrane system was added to the syngas, which can adjust the H<sub>2</sub>/CO ratio to the optimal value of 1.9 in the first FT reactor. The additional H<sub>2</sub> was used as H<sub>2</sub> makeup in the subsequent (i.e., 2nd and 3rd) FT reactors to maintain the  $H_2$ /CO ratio at 1.9 [37]. Developing an energy efficient  $H_2/CO_2$  separation carbon membrane system is crucial to achieve an economic process for biodiesel production from biomass.

In order to document the technology and economic feasibility of a carbon membrane system for  $H_2$  purification from a fermentation process, process simulation was conducted in a gas stream with the characteristics listed in Table 1. The membrane performance reported in the literature [31,35] was used as the simulation basis listed in Table 2. The following assumptions were made in the process simulation:

- No feed and permeate pressure drop employed.
- Compressor efficiency was set 75%.
- A counter-current configuration was used in the membrane transport model.

#### 3.2. Membrane process design

A novel, energy efficient two stage carbon membrane system for  $H_2$  purification was designed (see Fig. 2) based on the combination of  $H_2$  selective hollow fiber carbon membranes (Carbon molecular sieve membranes (CMSMs)) in the first stage and CO<sub>2</sub> selective carbon membranes (Selective surface flow (SSF) carbon Download English Version:

# https://daneshyari.com/en/article/4989882

Download Persian Version:

https://daneshyari.com/article/4989882

Daneshyari.com