



## Research Paper

## Multi-objective optimization of the operational modes for redundant refrigeration circuits

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## HIGHLIGHTS

- Optimal control for redundant refrigeration circuits and multiple compressors.
- A method is presented to optimize the provision of the required cooling capacity.
- Different goals, such as reducing the wear or energy demand can be achieved.
- Implementation with little computing power by using off-line optimization.

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## ABSTRACT

This paper presents a method to optimize the provision of the required cooling capacity in redundant refrigeration circuits with respect to several conflicting goals. The proposed method is presented for a refrigeration system with redundant refrigeration circuits and multiple compressors. The cooling capacity required by an arbitrary controller can be delivered by such a system using several different operation modes. Each mode is characterized by the respective active components and the values of the individual continuous control variables. The resulting degrees of freedom can be utilized to optimize additional goals such as energy consumption and wear. The optimal process operation can thus be formulated as an optimization problem for a hybrid system. An important highlight of the proposed method is the computational efficiency, which allows the implementation in an inexpensive micro-controller. This is achieved by solving the computationally most expensive part of the problem off-line and storing the result in look-up tables. Simulation examples demonstrate the effectiveness and performance of the proposed method.

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## 1. Introduction

Refrigeration systems (RSs) consume a substantial amount of energy and are a large source of peak electrical demand. There is also a rising trend towards higher consumption of several food products with consequent increase in environmental impacts. Such a significant impact are greenhouse gas emissions, [1]. In UK the commercial food sector, including agriculture, food manufacture, transport and retail is responsible for 22% of the total greenhouse gas emissions. Technologies and approaches in food transport refrigeration and their environmental affects are reviewed in [2]. The impacts are expressed in terms of greenhouse gas emissions arising from the fuel consumption of the vehicle and refrigeration

system engines and refrigerant leakage to the environment. Norway is yet another example. In Norway, seafood is one of the largest exports, mostly in fresh, frozen or dried form, [3]. One study reported by [4] shows that there are at least one million refrigerated road vehicles in use in the world. Therefore, one of the objectives of technical development of RSs is to increase their energy efficiency. In the case of using an internal combustion engine as primary energy source also the reduction of emissions is crucial.

Typically, an RS is designed for one specific operating point, but it operates most of the life time in conditions significantly different from design cases. Therefore, it is worth to analyze how to make these systems operate more efficiently by optimizing all operational modes.

One method of achieving higher efficiency is through cooling capacity control. Cooling capacity control methods commonly employed are optimal on-off control, hot gas bypass, suction pressure control, multiple compressor control and variable speed

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## Nomenclature

<b>c</b>	all counts of compressor switching for $\sigma_{act}$	$S_{i,j}$	compressor state of the compressor $j$ of RC $i$
$c_l$	count of compressor switching for $\sigma_{act,l}$	$T$	simulation time in sec
$E_{el}$	energy consumption in J	$t$	index of the simulation time
$f_i$	function of the static RC $i$ model	$T_{amb}$	ambient temperature in °C
$f_h$	function of the compressor status	$T_{box}$	ICB temperature in °C
$g_{eq}$	equality constraint	$T_{box,set}$	ICB set temperature in °C
$g_{ineq}$	inequality constraints	$t_{cst}$	control settling time in sec
<b>h</b>	hours of all compressors of the RS in h	$T_{D_i}$	discharge temperature of RC $i$ in K
$h_{i,j}$	operating hours of compressor $j$ of RC $i$ in h	$T_{evap,i}$	evaporator temperature of RC $i$ in K
<b>H</b>	sum of the operating hours of all combinations $\sigma_{act}$ in h	$\Delta T_{SH_i}$	superheat of RC $i$ in K
$H_l$	sum of the operation hours of the $l$ th combination of $\sigma_{act}$ in h	$v_i$	valve position of RC $i$ in %
$i$	index for the RC	<b>W(S K)</b>	switching probability of all permutation indices in K
$j$	index for the compressors	$W_k(S K)$	switching probability of the permutation with index $k$
$J_C$	cost function of the continuous decision values	<b>z<sub>env</sub></b>	measurable environmental conditions
$J_D$	cost function of the discrete decision values		
$J_{D1}$	cost function of compressor switching	<i>Greek</i>	
$J_{D2}$	cost function of operating hours	$\alpha$	weighting factor
$J_E$	cost function of power consumption	$\kappa_A$	heat transfer coefficient of the ICB in $\frac{W}{K}$
$J_o$	cost function of other criteria (such as control settling time)	$\lambda$	Lagrange multiplier for equality constraints
$J_W$	cost function of wear	$\mu$	Lagrange multiplier for inequality constraints
$k$	index of the permutations	<b><math>\sigma</math></b>	vector of all discrete decision variables of the RS
$K$	indices of the permutations which can provide $\dot{Q}_{req}$	<b><math>\sigma_{act}</math></b>	subset of $\sigma$ with the actual compressor combinations
$l$	index of the subset of the compressor combinations $\sigma_{act}$	<b><math>\sigma_{act,l}</math></b>	the $l$ th compressor combination of $\sigma_{act}$
$\mathcal{L}$	Lagrange function	$\zeta_{ar}$	set of constraints
$mc_p$	thermal mass capacity of the ICB in $\frac{kg \cdot m^2}{s^2 \cdot K}$	<b><math>\Psi</math></b>	vector of all continuous decision variables of the RS
$n_c$	sum of all compressors in the RS	<b><math>\Psi_j</math></b>	vector of all continuous decision variables of the RC $i$
$n_i$	sum of all compressors in the RC $i$	<b><math>\bar{\Psi}_{max,i}</math></b>	vector of time-varying maximal system constraints of the RC $i$
$n_k$	number of permutations	<b><math>\bar{\Psi}_{min,i}</math></b>	vector of time-varying minimal system constraints of the RC $i$
$n_l$	number of all compressor combinations in the subset $\sigma_{act}$	$\omega$	speed of all compressors of the RS in $rad \cdot s^{-1}$
$n_{n_{RC}}$	sum of all compressors in the RC $n_{RC}$	$\omega_i$	speed of all compressors of RC $i$ in $rad \cdot s^{-1}$
$n_{RC}$	number of RCs	$\omega_{i,j}$	speed of the compressor $j$ of RC $i$ in $rad \cdot s^{-1}$
$p(\bar{Q})$	probability density function	$\omega_{FC,i}$	speed for the condenser fan of the RC $i$ in $rad \cdot s^{-1}$
$p_{D_i}$	discharge pressure of RC $i$ in bar	$\omega_{FE,i}$	speed for the evaporator fan of the RC $i$ in $rad \cdot s^{-1}$
$P_{el}$	total electrical power of the active RCs in kW	$\omega_m$	speed of the ICE in $rad \cdot s^{-1}$
$P_{el,i}$	electrical power of the RC $i$ in kW		
$P_{el}^k$	total electrical power of the permutation with index $k$ in kW	<i>Sub-/superscript</i>	
$p_{S_i}$	suction pressure of RC $i$ in bar	• <sub>B</sub>	subscript for method B
$\bar{Q}$	total cooling capacities of the active RCs in kW	• <sub>b</sub>	subscript for method b
$\bar{Q}_{\Sigma}$	possible cooling capacity range of all permutations in kW	• <sub>max</sub>	subscript for the maximal value of •
$\dot{Q}_H$	total heating capacity of the active RCs in kW	• <sub>min</sub>	subscript for the minimal value of •
$\dot{Q}_{H,i}$	heating capacity of the RC $i$ in kW	• <sup>*</sup>	optimal value of •
$\dot{Q}_i$	cooling capacity of the RC $i$ in kW	• <sup>̄</sup>	value of • considering constraints
$\bar{Q}_k$	range of possible cooling capacity from permutation $k$	<i>Abbreviations</i>	
$\bar{Q}_{min,k}$	smallest possible cooling capacity from permutation $k$	COP	coefficient of performance
$\bar{Q}_{max,k}$	maximum possible cooling capacity from permutation $k$	EXV	electronic expansion valve
$\dot{Q}_M$	average cooling capacity of the active RCs in kW	ICB	insulated cool box
$\dot{Q}_{req}$	desired cooling capacity in kW	ICE	internal combustion engine
<b>S</b>	switching event	PID	proportional-integral-derivative controller
<b>s</b>	compressor states of all compressors of the RS	PI	proportional-integral controller
<b>s<sub>i</sub></b>	compressor states of all compressors of RC $i$	RC	refrigeration circuit
		RMSE	root-mean-squared error
		RS	refrigeration system

control. The most energy efficient method is the variable speed control and the multiple compressor strategy, [5].

Several studies have demonstrated the potential savings associated with the use of variable speed control. In [6] the potential electricity savings by using a variable speed compressor and a con-

troller for air conditioning systems is shown. In [7] a feed-forward control for a variable speed refrigeration system is introduced. A PI controller manages the thermal capacity and superheat independently for saving energy and to improve the coefficient of performance (COP).

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