



Research Paper

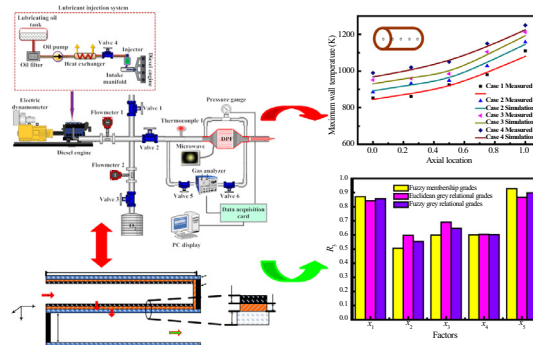
Influence of structural and operating factors on performance degradation of the diesel particulate filter based on composite regeneration

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HIGHLIGHTS

- An efficient method combining OED and FGRA for evaluating impacts is presented.
- Pressure drop and maximum wall temperature under various conditions are obtained.
- Fuzzy grey relational grades are employed for comprehensive evaluation.
- The primary influence factors of the DPF's performance degradation are obtained.

GRAPHICAL ABSTRACT



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ABSTRACT

In order to effectively investigate the effects of various factors on the DPF's performance deterioration, and obtain the primary influence factor, an efficient evaluation method is proposed in this work. Firstly, the maximum wall temperature and the pressure drop are taken as the evaluation indexes of DPF's performance deterioration (thermal aging and filter clogging) respectively, and the orthogonal experimental design is used for obtaining the simulation conditions of test cases. Then, the impacts of four structural factors (wall thickness, mean pore size, porosity and channel width) and five operating factors (exhaust flow rate, exhaust oxygen concentration, microwave power, catalytic additive mass concentration and deposited ash mass) on DPF's performance deterioration are evaluated by fuzzy membership grades and Euclidean grey relational grades, respectively. Finally, fuzzy grey relational analysis is employed to make a comprehensive evaluation. The results show that the wall thickness and the channel width have the most noticeable effect on filter clogging and thermal aging among all structural factors, respectively. Moreover, the deposited ash mass and the microwave power are the most important operating factors for filter clogging and thermal aging, respectively. This work offers us great reference value for optimizing DPF performances and improving its degradation resistance.

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1. Introduction

With the rapid increase of car ownership, the impact of automobile emission pollutants on the environment become more and more serious [1,2]. At present, various emission control methods

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Nomenclature

A_1	cross-sectional area of the inlet channel [m ²]	p_1	exhaust pressure in inlet channels [Pa]
A_2	cross-sectional area of the outlet channel [m ²]	p_2	exhaust pressure in outlet channels [Pa]
A_{soot}	area of the soot layer [m ²]	P_{mw}	microwave power [kW]
A_{ash}	area of the ash layer [m ²]	a	channel width of the filter [mm]
A_w	area of the substrate wall [m ²]	a_1	channel width for inlet channels considering soot and ash deposition
L	filter length [mm]	a_2	channel width for outlet channels
D	filter diameter [mm]	d	mean pore size [μm]
E	activation energy [J mol ⁻¹]	k_{wall}	permeability of the filter wall, $k_{\text{wall}} = 1.8 \times 10^{-13} \text{ m}^2$
F	friction coefficient of the filter wall, $F = 28.45$	k_{ash}	permeability of the ash layer, $k_{\text{ash}} = 3.08 \times 10^{-14} \text{ m}^2$
Q	exhaust flow rate [g s ⁻¹]	k_{soot}	permeability of the soot layer, $k_{\text{soot}} = 1.0 \times 10^{-14} \text{ m}^2$
R	universal gas constant, $R = 8.314 \text{ J (mol K)}^{-1}$	$k_{\text{O}_2,0}$	pre-exponential factor of oxidation reaction rate, $k_{\text{O}_2,0} = 5.96 \times 10^2 \text{ m s}^{-1}$
$R_{\text{cat O}_2}$	oxygen consumption rate by catalytic soot oxidation	w	wall thickness [mm]
$R_{\text{th O}_2}$	oxygen consumption rate by thermal soot oxidation	w_{ash}	thickness of the ash layer [mm]
V	filter volume [m ³]	w_{soot}	thickness of the soot layer [mm]
C_g	specific heat capacity of the exhaust gas [J (kg K) ⁻¹]	$w_{s,0}$	the initial thickness of soot layer at initial time [mm]
C_{soot}	specific heat capacity of soot [J (kg K) ⁻¹]	m_{soot}	the mass of PM deposition [g L ⁻¹]
C_{ash}	specific heat capacity of ash [J (kg K) ⁻¹]	m_{ash}	the mass of ash deposition [g L ⁻¹]
C_w	specific heat capacity of the substrate wall [J (kg K) ⁻¹]	Y_0	exhaust oxygen concentration [%]
M_C	molar mass of carbon particles [kg/mol]	c_a	catalytic additive mass concentration [mg L ⁻¹]
M_{OX}	molar mass of oxygen [kg/mol]	ε	porosity [%]
Y_1	oxygen concentration in the inlet channel (%)	β	complete coefficient of the soot oxidation reaction, $\beta = 0.8$
Y_0	oxygen concentration of the exhaust gas (%)	μ_1	dynamic viscosity of the exhaust gas in the inlet channels [Pa s]
H_{acc}	the amount of energy for solid phase [J]	μ_2	dynamic viscosity of the exhaust gas in the outlet channels [Pa s]
H_{con}	convection heat [J]	ζ_{cont}	contraction coefficient of the inlet channel, $\zeta_{\text{cont}} = 0.4$
H_{tran}	transfer heat [J]	ζ_{exp}	expansion coefficient of the outlet channel, $\zeta_{\text{exp}} = 0.4$
ΔH_{cat}	heat of reaction for catalytic oxidation [J]	ρ_1	exhaust gas density in inlet channels [kg m ⁻³]
ΔH_{th}	heat of reaction for thermal oxidation [J]	ρ_2	exhaust gas density in outlet channels [kg m ⁻³]
Q_{reaction}	reaction heat of soot oxidation [J]	ρ_w	exhaust gas density inside the substrate wall [kg m ⁻³]
S_p	specific surface area of carbon particle layer [m ⁻¹]	ρ_{soot}	packing density of the soot layer, $\rho_{\text{soot}} = 1500 \text{ kg m}^{-3}$
T_1	exhaust temperature in inlet channels [K]	ρ_{ash}	packing density of the ash layer, $\rho_{\text{ash}} = 450 \text{ kg m}^{-3}$
T_2	exhaust temperature in outlet channels [K]	ρ_{wall}	density of the filter wall [kg m ⁻³]
T_w	exhaust temperature inside the substrate wall [K]	ρ_{cell}	cell density of the filter [cells in ⁻²]
T_{w_max}	maximum wall temperature [K]	v_1	inlet velocity of the exhaust gas in the channels [m s ⁻¹]
T_0	initial exhaust temperature [K]	v_2	outlet velocity of the exhaust gas in the channels [m s ⁻¹]
Re_1	Reynolds number in the inlet channel	h_1	heat transfer coefficient between exhaust flow and filter wall in inlet channels [W (m ² K) ⁻¹]
Re_2	Reynolds number in the outlet channel	h_2	heat transfer coefficient between exhaust flow and filter wall in outlet channels [W (m ² K) ⁻¹]
Δp	total pressure drop of the DPF [Pa]	λ_{soot}	thermal conductivity of the soot layer [W (m K) ⁻¹]
Δp_{cont}	local pressure drop of the inlet with variable cross-section in filter channels [Pa]	λ_{ash}	thermal conductivity of the ash layer [W (m K) ⁻¹]
Δp_{exp}	local pressure drop of the outlet with variable cross-section in filter channels [Pa]	λ_w	thermal conductivity of the filter wall [W (m K) ⁻¹]
$\Delta p_{\text{inlet_channel}}$	pressure drop along the inlet channel [Pa]	α_1	thermal carbon monoxide selectivity
$\Delta p_{\text{outlet_channel}}$	pressure drop along the outlet channel [Pa]	α_2	catalytic carbon monoxide selectivity
Δp_{wall}	pressure drop of the filter wall [Pa]		
$\Delta p_{\text{ash_layer}}$	pressure drop of the ash layer [Pa]		
$\Delta p_{\text{soot_layer}}$	pressure drop of the soot layer [Pa]		
Δp_1	pressure drop of the DPF with PM [Pa]		
Δp_c	pressure drop of the clean DPF [Pa]		
Δp_r	pressure drop of the DPF after regeneration [Pa]		
p_0	atmospheric pressure [Pa]		

and electric vehicle technologies are used to solve environmental pollution and to comply with the increasingly stringent emission standards [3–5]. It is well known that diesel engines have been widely used as the vehicle power in the world due to their low fuel consumption, strong power performance and better reliability [6–9]. Unfortunately, diesel powered vehicles produce a considerable amount of particulate matter (PM) [10], which is thought to be the main source of air pollution. Currently, the wall-flow diesel particulate filter (DPF) is considered to be one of the most effective aftertreatment device for PM abatement in diesel powered vehicles [11,12], and the regeneration technology [13,14] is the key process for its actual application. However, widely application of the DPF in automobiles is restricted due to its deterioration after multiple

regenerations in the porous media filter [15,16], and DPF degradation can inevitably result in the increase of pressure drop as well as the decrease of filtration efficiency and regeneration efficiency, limiting the DPF's in use service life, so that the DPF requires removal for periodic cleaning or replacement. Therefore, it is quite necessary to investigate the performance degradation or durability of the DPF to improve its service life.

Over the years, the material of the filter, the regeneration strategy, the filter structural parameters, and the operating condition have been investigated to guarantee best performances, such as high filtration efficiency and regeneration efficiency as well as low pressure drop during standard operations, but also reliability and durability in the long run.

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