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An overview of boundary implementation in lattice Boltzmann method for computational heat and mass transfer^{*}

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6 A R T I C L E I N F O

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ABSTRACT

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The ability to deal with the complex geometries precisely and accurately has always been the most integral part 14 of any computational fluid dynamics approach. The lattice Boltzmann method has already achieved considerable 15 success in the simulation of unsteady flow with arbitrary boundary shapes. To include boundaries in the lattice 16 Boltzmann simulations, several methods have been presented in the past to satisfy the standard boundary imple-17 mentation of macroscopic flows. In spite of the considerably vast body of literatures that discuss in this field, the 18 study still is in progress. The current study is an overview of the adopted boundary conditions in lattice 19 Boltzmann method. 20

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34 1. Introduction

The lattice Boltzmann method (LBM) is an innovative technique of 35 computational fluid dynamics based on the Boltzmann transport equa-36tion, which is supported by the advanced kinetic theory [1-7]. In the last 37few decades, LBM has changed into a successful alternative method for 38 simulating complex physical, chemical, and fluid mechanics problems 39 [8,9]. The LBM utilizes the ensemble-averaged distribution functions 40to explain the system by this assumption that the collective behavior 41 of the fictitious particles which, comprised of the system, is consistent 42 with the principles of the macroscopic physics. An interesting aspect 43 of the LBM is its ability to process the complicated boundary geometries 44 45 easily with acceptable accuracy [10]; hence, investigating the suitable boundary conditions' treatment for LB simulations has become a highly 46researched area in many engineering and scientific applications 47 [11–16]. The computational efficiency of LBM in comparison with the 4849 traditional CFD methods establishes it as a potent applicant. The quantitative behavior of LBM was investigated in comparison with FVM in 50many research studies [17-20]. The results show that, concerning 5152complex geometries, the lattice Boltzmann method showed more efficiency than the well accepted finite volume approach. The CPU 53 times with increasing complexity of the obstacle structure was 5455increased for both method and for highly complex structures became 56almost independent from it for LBM. Furthermore, based on review by 57Chen and Doolen [21] the approximated computational cost for moving 58solid particle simulation, in suspension simulation, in LBM had been

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http://dx.doi.org/10.1016/j.icheatmasstransfer.2016.08.014 0735-1933/© 2016 Elsevier Ltd. All rights reserved. convenient and efficient. The work for simulation of N particles in 59 LBM moving boundary method scales linearly with N while in finite 60 element method this scale is N^2 [22]. A method with the capability of 61 accurate inter-phase calculation and simple boundary condition imple-62 mentation can be a very good option for replacing the current methods 63 of complex flow simulation. Adding to these advantages, parallel scal-64 ability has made it exceptional to many other numerical approaches. 65 In this paper, we are willing to review the different boundary condition 66 developing trend in the frame of LBM. In the next section lattice 67 Boltzmann method will be briefly touched and on followings the most 68 popular studies of LBM boundary conditions will be summarized and 69 discussed based on the CFD standard categories. 70

2. Review of lattice Boltzmann method

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The LBM has its ancestry from the lattice gas automata (LGA), a 72 kinetic model that was constructed in discrete space and time. The 73 discretized velocity distribution function can be obtained by solving 74 the Boltzmann equation with different collision models. The LGA is frus-75 trated by some unwanted issues. First, the density dependent factor in 76 nonlinear advection term and a velocity dependent pressure that does 77 not lead to the Galilean invariance system of lattice gases. Second, it is 78 overwhelmed by noise. To overcome these undesirable problems LBM 79 replaced the Boolean variable in LGA by a single particle distribution 80 function [23]. This process eliminated the statistical noise in LGA and 81 single particle distribution function f_i was defined as an ensemble 82 average of particle occupation variable ($f_i = n_i$). The practical approach, 83 interpreted in the LBM, consists of solving the Boltzmann equation for 84 the evolution of a single distribution function f(x, v, t) of particles as 85 they move and collide on a lattice. The solution of the equation includes 86

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two main steps; the stream step or advection term propagates informa-87 88 tion through the lattice cells, while the collision step normalizes the distribution functions to the equilibrium distribution function. The col-89 90 lision operator represents the rate of change of the distribution function due to the colliding process and depends only on the local equilibrium 91state. The discrete Boltzmann equation with the BGK [24] collision 9293 model for the particle velocity distribution function, $f_i(x,t)$ ignoring 94the external force term can be expressed as:

$$f_i(x + e_i\Delta t, t + \Delta t) = f_i(x, t) + \frac{1}{\tau} (f_i(x, t) - f_i^{eq}(x, t)), (i = 0, 1, 2, 3, \dots, N)$$
(1)

where τ is the relaxation time, Δt is the time step, $e_i(=\Delta x/\Delta t)$ is the 96 particle velocity in the *i*-direction. f_i is the particle velocity distribution 97 along the *i*th direction, which represents the fraction of the particles 98 with velocities in the range of e_i and $e_i + d e_i$. The number of discrete velocity directions standing for the lattice is chosen based on certain sym-99 100 metry requirements to recover the isotropy of the viscous stress tensor of the fluid flow [25]. The zero index symbolizes the rest particle with 101 the zero velocity. The relaxation time is related to the kinematic viscos-102ity of the fluid via the relation: 103

$$\tau = 3\nu + \frac{1}{2}.\tag{2}$$

The equilibrium distribution function which appears in the collision operator is an expansion of the Maxwellian distribution function in an equilibrium state for the low Mach number.

$$f^{eq}(x,t) = \frac{\rho}{(2\pi RT)^{\frac{d}{2}}} \exp\left(-\frac{(e-u)\cdot(e-u)}{2RT}\right)$$
(3)

where *R*, *T*, ρ and *u* are gas constant, temperature, macroscopic density and macroscopic velocity respectively. *d* stands for space dimension.
 The general structure of the equilibrium function can be written up

111 to $O(u^2)$ [26]:

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$$f_{i}^{eq}(\rho, u) = \rho \left[a + b \left(e_{i}.u \right) + c \left(e_{i}.u \right)^{2} - d \left(u.u \right) \right]$$
(4)

113 where *a*, *b*, *c*, and *d* are the lattice constants. $\rho(=\Sigma f_i)$ is the fluid density, $u (\rho u = \Sigma f_i e_i)$ is the fluid velocity. The coefficients of the above equation 114 can be obtained analytically [27] and results in:

$$f_i^{eq}(\rho, u) = \rho w_i \left[1 + \frac{1}{c_s^2} (e_i . u) + \frac{1}{2c_s^4} (e_i . u)^2 - \frac{1}{2c_s^2} (u . u) \right]$$
(5)

116 where c_s is the speed of sound and w is the weighting factor in the lattice fluid density. This equation is used for lattice nodes within the fluid domain and the boundary nodes need extra treatments due to insufficient 117 number of known distribution functions. In the simulations of LBM, the 118 distribution functions f_i on the fluid nodes are known after each time 119120step of streaming, but some distribution functions on the boundary 121 nodes are unknown. Only if distribution functions on the boundary nodes are determined, the next computation step can proceed. So, the 122distribution functions on the boundary nodes need to be determined 123based on the known macroscopic boundary conditions. When boundary 124appears physical characteristics, including periodicity, symmetry, and 125fully developed flow conditions, unknown distribution functions can 126be simply determined by the motion pattern of particles. 127

128 **3. Boundary condition in LBM**

One of the most important and critical issues in the LBM is imposing the proper boundary condition for flow simulation. Applying the boundary condition in NS method is somehow straightforward, while in LBM, because of the mesoscopic nature, it is not so clear and it needs translation from macroscopic to mesoscopic scale. Hence, 133 remarkable efforts have been devoted to develop effective and precise 134 boundary schemes for different situations. Depending on the flow 135 structure and problem geometries, various types of boundary condition, 136 including free slip, no-slip, periodic, sliding walls, moving walls, in-flux, 137 and out-flux boundaries might be applied to the evolution of the distribution functions. In the frame of LBM, different approaches have been 139 presented for simulating BCs [28–32]. 140

3.1. Periodic boundary condition 141

Through the aforementioned BCs the easiest one is the periodic 142 boundary at the sides of the computational domain. In this case, the system is assumed to be isolated in a closed domain so the number of particles remains constant due to conservation law. The periodic conditions 145 are applied as a natural part of the streaming operation, so that outgoing 146 particles at one end of the lattice become incoming particles at the other 147 end. These make sure that mass is neither gained nor lost through the 148 periodic boundaries. The concerns about positivity of the population 149 are somewhat the key of numerical stability and the major drawback 150 of the proposed methods is laid in that the distribution function is lost 151 during the BC applying [33]. However, there is an agreement on the 152 methods of treatment for this type of BC, but a more specified study in 153 this field can be found in the literatures. 154

In a reported study of Zhang and Kwok [34] the general periodic BC 155 of the lattice Boltzmann method has been altered to include the pressure variance for fully developed periodic flows (Fig. 1). They stated Q2 that the proposed treatment does not generate nonphysical inlet or outlet disturbance and it is applicable for systems with periodic electric and 159 temperature fields. Later on, Kim et al. [35] proposed a new boundary 160 closure for fully developed pressure driven flow, which is of higher accuracy than of Zhang et al. [34] and it is applicable for both compressible and incompressible flows. Subsequently, Gräser and Grimm [36] have 163 combined the Kim and Pitsch method with a controller loop that 164 adapted a perpendicular pressure gradient to restrain any net momentum, perpendicular to the outer walls and developed an algorithm for an adaptive BC for fully developed pressure driven flow simulation.

3.2. Pressure and velocity boundary condition

Successful fluid flow numerical simulations desire the proper 169 velocity and pressure boundary conditions implementation. The gener- 170 al velocity and pressure boundaries are still under further development 171 for the lattice-Boltzmann method. In LBM, most previous researches 172 concerned with pressure and the velocity boundary condition concen- 173 trate somehow on the wall Dirichlet boundary condition based on the 174

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Fig. 1. The periodic boundary for left and right sides of a domain (D2Q9).

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