



Numerical investigation of mixed convection of Bingham fluids in cylindrical enclosures with heated rotating top wall



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ABSTRACT

The steady-state laminar mixed convection of yield stress fluids obeying the Bingham model in a cylindrical enclosure with a heated rotating top cover has been numerically analysed based on axisymmetric incompressible flow simulations. Yield stress effects on heat and momentum transport have been investigated for an aspect ratio (height/radius) of unity (*i.e.* $AR = 1$) for a range of different values of nominal Prandtl, Richardson and Reynolds numbers given by $10 \leq Pr \leq 500$, $0 \leq Ri \leq 1$ and $100 \leq Re \leq 3000$. The mean Nusselt number \overline{Nu} has been found to decrease sharply with increasing Bingham number Bn , but subsequently \overline{Nu} approaches asymptotically to a value of unity, which is indicative of conduction-driven transport. It has also been found that \overline{Nu} increases with increasing values of Prandtl and Reynolds numbers for both Newtonian (*i.e.* $Bn = 0$) and Bingham fluids. In contrast, \overline{Nu} decreases with increasing Ri for both Newtonian and Bingham fluids for small values of Bingham number, whereas \overline{Nu} remains insensitive to the variation of Ri for large values of Bingham number. The variation of torque coefficient C_T , which gives a quantitative measure of power consumption, has also been investigated. The torque coefficient C_T has been found to increase with increasing Bn whereas it decreases with increasing Re . It has also been found that C_T decreases slightly with increasing Ri for small values of Bn , whereas it becomes insensitive to the variation of Ri for large Bingham numbers. For the fully forced convection ($Ri = 0$) case, Pr does not have a significant influence on C_T . However, in the case of mixed convection C_T increases with increasing Pr . The simulation data has been used in conjunction with a detailed scaling analysis to propose a correlation for \overline{Nu} for the range of Re , Ri and Pr considered here.

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1. Introduction

Mixing and heat transfer play pivotal roles in several engineering applications relevant to chemical processing, bio-chemical synthesis, polymer processing, food preparation, modern agriculture and many other related industries. Augmentation of mixing and heat transfer in laminar flow conditions can be challenging but it is possible to enhance the rates of heat transfer and mixing by rotating one of the covers of a cylindrical container to produce a swirling flow. Although superficially it seems to be a simple process, the heat transfer rate in this configuration depends on many parameters, such as the container geometry and rotational speed of cover. Flow in cylindrical enclosures with a rotating cover has been extensively analysed owing to its wide-ranging roles in the aforementioned engineering applications. However, the majority of these analyses have been conducted only for Newtonian Fluids

(where the viscous stress is directly proportional to strain rate). Vogel [1,2], Ronnenberg [3], and Bertela and Gori [4] pioneered the analysis of this configuration for Newtonian fluids. The findings of these studies [1–4] were confirmed and extended by Escudier [5] based on an experimental analysis where the stability criterion for vortex breakdown was identified in terms of aspect ratio ($AR = \text{height/radius} = H/R$) and Reynolds number ($\Omega R^2/\nu$). In addition to these experimental studies, several numerical investigations [6–10] involving Newtonian fluids have been carried out. Lee and Hyun [8] analysed the effects of Prandtl number on heat transfer rate in this configuration and revealed that Prandtl number has an important influence on the heat transfer characteristics and advective transport has been found to strengthen with increasing Prandtl number. Iwatsu [9] investigated the effects of Reynolds and Richardson numbers in the range of $100 \leq Re \leq 3000$ and $0 \leq Ri \leq 1$ for $Pr = 1$ on the flow pattern and heat transfer rate for swirling flows in cylindrical enclosures with an aspect ratio of unity (*i.e.* $AR = H/R = 1$) and a heated rotating top wall. The analysis by Iwatsu [9] revealed that advective (diffusive) transport

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Nomenclature

a, a_0 [-]	bridging function	$\dot{\gamma}$ [1/s]	shear rate
a_1, a_2 [-]	correlation parameters	δ, δ_{th} [m]	hydrodynamic and thermal boundary layer thickness
AR [-]	aspect ratio ($AR = H/R$)	θ [-]	non-dimensional temperature ($\theta = (T - T_C)/(T_H - T_C)$)
b, b_0 [-]	bridging function	θ_1 [-]	parameter
b_1, b_2 [-]	correlation parameters	μ [Ns/m ²]	plastic viscosity
Bn [-]	Bingham number	μ_{yield} [Ns/m ²]	yield viscosity
c_p [J/kg K]	specific heat at constant pressure	ν [m ² /s]	kinematic viscosity
C_T [-]	torque coefficient	ρ [kg/m ³]	density
e_a [-]	relative error	τ [N/m ²]	shear stress
f_1, f_2, f_3 [-]	functions	τ_y [N/m ²]	yield stress
g [m/s ²]	gravitational acceleration	Ω [1/s]	angular velocity
Gr [-]	Grashof number	ψ [m ² /s]	stream function
h [W/m ² K]	heat transfer coefficient	Ψ [-]	non-dimensional stream function ($\Psi = \psi/\alpha$)
H [m]	height of cylindrical enclosure		
k [W/m K]	thermal conductivity		
k_0, k_1 [-]	correlation parameters		
m_0, m_1 [-]	correlation parameters	Subscripts	
Nu [-]	Nusselt number	$Bn = 0$	Newtonian fluid case
\bar{Nu} [-]	mean Nusselt number	C	cold wall
p [-]	theoretical order of accuracy	eff	effective value
Pr [-]	Prandtl number	H	hot wall
q [W/m ²]	heat flux	max	maximum value
R [m]	radius of cylindrical enclosure	r	radial direction
Ra [-]	Rayleigh number	ref	reference value
Re [-]	Reynolds number	$wall$	wall value
Ri [-]	Richardson number	wf	condition of the fluid in contact with the wall
T [K]	temperature	z	axial direction
u [m/s]	radial velocity component	ϕ	tangential direction
U (m/s)	characteristic velocity scales in radial direction		
v [m/s]	tangential velocity component	Special characters	
V (m/s)	characteristic velocity scales in tangential direction	ΔT [K]	difference between hot and cold wall temperature ($= (T_H - T_C)$)
V_ϕ [-]	non-dimensional swirl velocity ($V_\phi = vH/\alpha$)	$\Delta_{min, cell}$ [m]	minimum cell distance
w [m/s]	vertical (axial) velocity component	r [-]	grid expansion ratio
α [m ² /s]	thermal diffusivity		
β [1/K]	coefficient of thermal expansion		

strengthens (weakens) and, accordingly, the mean Nusselt number decreases with increasing Richardson number. Compared to Newtonian fluids, relatively limited efforts have been directed to the analysis of mixed convection of non-Newtonian fluids (where the viscous stress is not proportional to the strain rate). Although both water and air, being the most abundant fluids on the planet, are Newtonian fluids, and it is logical that most previous work concentrated on such Newtonian fluids, virtually all synthetic, food-based and biological fluids (e.g. detergents, toothpaste, cosmetics, ketchup, custard, blood) are non-Newtonian in character. Some electro-rheological/magneto-rheological fluids exhibit yield stress and behave only as fluids once a threshold stress is surpassed. It is possible to modulate the yield stress by using an electrical/magnetic field in electro-rheological/magneto-rheological fluids. Thus, from an engineering perspective, the knowledge of mixed convection of more rheologically complex fluids than water or air is essential.

One of the first investigations related to swirling flows for non-Newtonian fluids was performed for flows over a rotating disk, which is commonly referred to as the von-Karman flow [11–13]. Most analyses on the non-Newtonian fluid flow in cylindrical enclosures with a rotating cover were carried out for viscoelastic fluids [14,15]. Escudier and Cullen [14] experimentally analysed cylindrical enclosures with a rotating top cover for shear-thinning viscoelastic fluids, and reported that the vortex structure is different from the Newtonian fluid case and an intense toroidal vortex that drives a secondary low intensity vortex was produced

in the vicinity of the rotating cover. Stokes and Boger [15] proposed a regime diagram for flow stability based on Reynolds and Elasticity numbers for viscoelastic fluids in cylindrical enclosures with a rotating cover. A recent experimental analysis of heat transfer under elastic turbulence of viscoelastic fluids within cylindrical enclosures with a rotating top cover was reported by Traore et al. [16]. It was found that the heat transfer rate under elastic turbulence might locally increase by up to four times as compared to the purely conduction regime. It was indicated by Traore et al. [16] that the elastic turbulence can augment the heat transport rate in situations where the inertial turbulence is difficult to obtain, such as in the case of microscopic flows.

Analysis of power-law fluids in cylindrical enclosures with a rotating cover was carried out by Böhme et al. [17]. The influence of shear-thinning on vortex breakdown (observed before by Vogel [1,2] and Escudier [5] for Newtonian fluids) in cylindrical enclosures with a rotating cover was experimentally and numerically analysed by Böhme et al. [17]. They constructed an aspect ratio - Reynolds number ($AR - Re$) diagram, representing the domain of vortex breakdown for shear-thinning fluids. A few recent analyses [18–20] have concentrated on rotating disk configuration for yield stress fluids. The mass transfer of yield stress fluids in such applications has recently been investigated by Rashaida et al. [18] and semi-analytical approaches for analysing swirling flow of Bingham fluids over a rotating disk has been reported by Ahmadpour and Sadeghy [19] and Guha and Sengupta [20]. However, to date, there is no analysis in the existing literature that deals with flow

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