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## Effect of aspect ratio on triaxial compression of multi-sphere ellipsoid assemblies simulated using a discrete element method

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### ABSTRACT

Here, we present a numerical investigation of the mechanical behavior of ellipsoids under triaxial compression for a range of aspect ratios. Our simulations use a multi-sphere approach in a three-dimensional discrete element method. All assemblies were prepared at their densest condition, and triaxial compression tests were performed up to extremely large strains, until a critical state was reached. The stress–strain relationship and the void ratio–strain behavior were evaluated. We found that the stress–dilatancy relationship of ellipsoids with different aspect ratios could be expressed as a linear equation. In particular, the aspect ratio influenced the position of the critical state lines for these assemblies. Particle-scale characteristics at the critical state indicate that particles tend to be flat lying, and the obstruction of particle rotation that occurs with longer particles affects their contact mechanics. Lastly, anisotropic coefficients related to aspect ratio were investigated to probe the microscopic origins of the macroscopic behavior. A detailed analysis of geometrical and mechanical anisotropies revealed the microscopic mechanisms underlying the dependency of peak and residual strengths on aspect ratio.

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### Introduction

Ellipsoids provide a good model to investigate the effects of particle shape on the mechanical behavior of granular materials (Lin & Ng, 1997; Ng, 2004, 2009). Previous studies (Bagherzadeh-Khalkhali & Mirghasemi, 2009; Zhou, Ma, Chang, & Zhou, 2013) confirmed that ellipsoid-shaped particles offer a realistic representation of soil behaviors. Ellipsoid-shaped particles can be characterized in terms of their aspect ratio, which is defined as the ratio of their major axis to their minor axis. Furthermore, aspect ratio is an important shape factor used to quantitatively describe the particle shape of actual granular materials (Altuhafi, O'Sullivan, & Cavarretta, 2013; Stahl & Konietzky, 2011). Using discrete element methods (DEMs; Cundall & Strack, 1979), two different initial conditions have been used for investigating the shape effects of ellipsoid-shaped particles in previous studies. These studies used either the same void ratio ( $e$ ) (Ng, 2004; Ting, Meachum, & Rowell, 1995; Yan, 2009; Yang, Wang, & Cheng, 2016), or the same relative density (Azema & Radjai, 2010, 2012; Lin & Ng, 1997; Rothenburg & Bathurst, 1992). Assemblies of

ellipsoid-shaped particles with different aspect ratios can have the same  $e$ ; however, their relative densities will be different because of differences in their limiting densities. Thus, differences in these two initial conditions can lead to conflicting observations. For example, Ng (2009) simulated mono-disperse ellipsoids with different aspect ratios at the same  $e$ ; he reported that the peak friction angles of the ellipsoids decreased slightly with increasing aspect ratio. However, when all of the assemblies were prepared at their densest condition, Rothenburg and Bathurst (1992) determined that the peak friction angle exhibited a unimodal feature, with varying aspect ratio. Most of the previous DEM simulations investigated the effects of aspect ratio on the mechanical behavior of ellipsoid-shaped particles at the same  $e$ , even though a relative density condition is more relevant to laboratory experiments. Alternatively, previous simulations prepared at the same relative density, were conducted in a 2D particle system. In 2D systems, the magnitudes of shear strength and deformation do not agree with those of actual granular materials because of their planar nature. Moreover, most of the earlier studies focused on the effects of aspect ratio on critical state behavior (e.g., Azema & Radjai, 2010, 2012). However, large strain regimes are less relevant to geotechnical applications because of the magnitude of the deformation. In contrast, a relatively small shear strain regime is of great importance because dilatancy and peak shear strength

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**Nomenclature**

*Symbols*

$a_c$	Anisotropic coefficient of the contact normal
$a_{ij}^c$	Second-order fabric anisotropy tensor
$a_{dn}$	Anisotropic coefficient of the branch vector
$a_{ij}^{dn}$	Second-order anisotropy tensor of the branch vector
$a_n$	Anisotropic coefficient of the normal contact force
$a_{ij}^n$	Second-order anisotropy tensor of the normal contact force
$a_t$	Anisotropic coefficient of the tangential contact force
$a_{ij}^t$	Second-order anisotropy tensor of the tangential contact force
$a^*$	Anisotropic coefficients $a_c$ , $a_n$ , $a_t$ , or $a_{dn}$
$a_{ij}^*$	Anisotropy tensor $a_{ij}^c$ , $a_{ij}^n$ , $a_{ij}^t$ , or $a_{ij}^{dn}$
$D$	Diameter of a reference spherical particle having the same volume with ellipsoids
$\bar{d}_0$	Average branch vector calculated for the entire range of $\Omega$
$d^c$	Branch vector joining the centers of the two particles in contact
$\bar{d}_{ij}'$	Deviatoric part of average branch vector tensors
$e$	Void ratio
$e_c$	Critical void ratio
$E_c$	The contact effective modulus
$E(\Omega)$	A probability distribution function of $\Omega$
$\bar{f}_0$	Average normal contact force calculated for the entire range of $\Omega$
$f^c$	Contact force at a given contact
$f_n$	Normal contact force at a specific contact
$f_t$	Tangential contact force at a specific contact
$F_{ij}^n, F_{ij}^{n'}$	Average normal contact force tensors and its deviatoric part
$F_{ij}^t, F_{ij}^{t'}$	Average tangential contact force tensors and its deviatoric part
$h$	Height of the assembly at a given deformation state
$h_0$	Initial height of the assembly after isotropic compression
$k$	Line-fitting parameter
$k_n$	Normal contact stiffness of the particles
$k_s$	Shear contact stiffness of the particles
$l_0$	Initial length of the assembly after isotropic compression
$n, n_i, n_j$	Unit contact normal vector and its component in the $i, j$ direction
$N_c$	Number of contacts in particle system
$N_p$	Number of ellipsoids in particle system
$p'$	Effective mean stress
$q$	Deviatoric stress
$r$	The smaller value of $r_a$ and $r_b$
$r_a, r_b$	The radii of particles in contact
$S$	Scalar parameter
$S_c$	The sliding ratio
$S_r$	Normalized quantity of the double contraction of $a_{ij}^*$ and $\sigma'_{ij}$
$t_i, t_j$	Component in the $i, j$ direction for unit contact tangential vector
$v$	Volume of the assembly at a given deformation state
$v_0$	Initial volume of the assembly after isotropic compression

$w$	Average rotation of particles about their minor axis
$w_0$	Initial width of the assembly after isotropic compression
$w_i$	Rotation of the major axis of the $i$ th particle from the initial state to steady state with $\varepsilon_1 = 65\%$

*Greek symbols*

$\varepsilon_1$	Axial strain
$\varepsilon_v$	Volumetric strain
$\mu_b$	Inter-particle friction
$\phi$	Internal angle of friction
$\phi_{ij}, \phi'_{ij}$	Fabric tensor and its deviatoric part
$\phi_p$	Peak internal friction angle
$\phi_c$	Residual friction angle
$\Omega$	The orientation of the branch-vector in spherical coordinates
$\theta_i$	The angle between the major axis of the $i$ th particle and the vertical direction
$\rho_p$	Density of the assembly at peak state
$\rho_c$	Density of the assembly at critical state
$\sigma_1$	Axial stress
$\sigma_2, \sigma_3$	Lateral stresses
$\sigma_c$	Confining pressure
$\sigma_{ij}, \sigma'_{ij}$	Stress tensor and its deviatoric part
$\psi$	Dilatancy angle
$\psi_p$	Peak dilatancy angle

are relevant to many engineering designs. In this context, we use a 3D particle system, which provides more accurate and reliable results than a 2D particle system, to investigate the effects of aspect ratio on the mechanical behavior of ellipsoids.

Eight types of ellipsoid-shaped particles, generated using a multi-sphere approach, were evaluated in this study. All of the assemblies were prepared at their densest condition for a given generation procedure. Quantitative relationships between particle shape and strength indices (i.e., friction angle and dilation angle), as well as stress–dilatancy relationships were investigated. In addition, the relationships between aspect ratio and particle-scale characteristics, such as coordination number (CN), particle rotation, orientational order, percentage of sliding contacts, and contact forces, were studied. Moreover, the accuracy of the stress–force–fabric based on the branch vector frame was analyzed, and any fabric anisotropies affected by aspect ratio were evaluated at peak and residual states. This detailed analysis of fabric anisotropies allowed us to determine the microscopic mechanisms underlying the dependence of shear strength on aspect ratio.

**Modeling using the discrete element method**

*Simulation parameters and assembly generation*

The popular DEM program PFC<sup>3D</sup> (Itasca, 2014) was used for numerical simulations in this study. The ellipsoid-shaped particles were modeled using a multi-sphere (MS) approach. The particle-forming method described by Taghavi (2011) is a built-in function of PFC<sup>3D</sup> and used to determine the positions and radii of the constitutive spheres, forming each particle. Eight types of particles with different aspect ratios were considered in this study, having aspect ratios of 1.00, 1.05, 1.10, 1.25, 1.50, 1.75, 2.00, and 2.50 (Fig. 1). All ellipsoids had the same volume, equal to the volume of a sphere with a diameter  $D = 1.86$  mm (Parafiniuk, Molenda, & Horabik, 2014). Taghavi (2011) defined a distance that corre-

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