### ARTICLE IN PRESS

Control Engineering Practice **(111) 111**-**111** 



Contents lists available at ScienceDirect

## **Control Engineering Practice**



journal homepage: www.elsevier.com/locate/conengprac

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#### ARTICLE INFO

Article history: Received 15 May 2015 Received in revised form 1 July 2016 Accepted 2 July 2016

Keywords: Hybrid vehicles Dynamic programming Sequential quadratic programming Energy management Potential analysis Velocity optimization Predictive control Economic driving

#### ABSTRACT

The combination of electric motors and internal combustion engines in hybrid electric vehicles (HEV) can considerably improve the fuel efficiency compared to conventional vehicles. In order to use its full potential, a predictive intelligent control system using information about impending driving situations has to be developed, to determine the optimal gear shifting strategy and the torque split between the combustion engine and the electric motor. To further increase fuel efficiency, the vehicle velocity can be used as an additional degree of freedom and the development of a predictive algorithm calculating good choices for all degrees of freedom over time is necessary.

In this paper, an optimization-based algorithm for combined energy management and economic driving over a limited horizon is proposed. The results are compared with results from an offline calculation, which determine the overall fuel savings potential through the use of a discrete dynamic programming algorithm.

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#### 1. Introduction

Over the last few decades, reducing fuel consumption for vehicles has become a more and more important field of research. Reasons for this development are increasing environmental awareness accompanied by stricter regulations and rising fuel costs. One technology emerging from this research is the hybrid electric vehicle (HEV), combining electric batteries and motors with the internal combustion engine (ICE) in one powertrain. There exists a wide variety of HEVs with different structures, e.g. parallel hybrid vehicles or series hybrid vehicles, and different degrees of hybridization, e.g. micro-hybrids, which are characterized by small batteries and electric motors (EM) whose main purpose is to implement an automatic engine start/stop function. At the other end of the scale plug-in hybrid vehicles with large batteries and motors facilitate long all-electric range and the possibility to charge the battery from the power grid (Guzzella and Sciarretta, 2013).

To achieve the best fuel efficiency, an optimal energy management system (EMS) is necessary to coordinate both power

http://dx.doi.org/10.1016/j.conengprac.2016.07.003 0967-0661/© 2016 Elsevier Ltd. All rights reserved. sources. Since an optimal control strategy depends on the driving cycle, this poses two main challenges: firstly, the parameters of the driving cycle are not necessarily known and, secondly, finding a global, optimal solution for the resulting nonlinear optimal control problem is numerically challenging. Therefore, this is a demanding field of research. For previous work in this field, see Sciarretta and Guzzella (2007), Pisu and Rizzoni (2007), Johannesson and Egardt (2008), Bender, Kaszynski, and Sawodny (2013) and Panday and Bansal (2014).

Another approach is economic driving, i.e., using the velocity as an additional degree of freedom to reduce fuel consumption. In recent years, work for different types of vehicles, such as conventional cars and trucks (e.g. Hellström, Åslund, and Nielsen, 2010; Hooker, 1988; Kamal, Mukai, Murata, and Kawabe, 2013; Llamas, Eriksson, and Sundström, 2013; Terwen, Back, and Krebs, 2004), fuel-cell cars (Sciarretta, Guzzella, and van Baalen, 2004) and electric cars (Petit and Sciarretta, 2011) has been published.

The next step to increasing fuel efficiency is to combine both economic driving and predictive EMS. In van Keulen et al. (2009, 2010), the velocity profiles for a hybrid electric truck are optimized. Therefore, the driving cycle is partitioned into segments of constant power request and each of these segments is divided into four phases: max. power acceleration, constant velocity, coasting and max. power deceleration. The parameters of these phases are then optimized to maximize power recovery and minimize fuel consumption. In Kim, Manzie, and Sharma (2009), a model

Please cite this article as: Heppeler, G., et al. Predictive planning of optimal velocity and state of charge trajectories for hybrid electric vehicles. *Control Engineering Practice* (2016), http://dx.doi.org/10.1016/j.conengprac.2016.07.003

<sup>&</sup>lt;sup>\*</sup>This work is part of the "Promotionskolleg Hybrid", a cooperation between science and industry, funded by the Ministry of Science, Research and the Arts of the State of Baden-Württemberg, Germany and the Daimler AG.

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Nomenclature		
$\Delta d$ $\Delta J_{ m SHO}$	discretization of the short horizon optimization stage transition costs for the short horizon	
A	optimization	
$\Delta p$	phase length	
$\Delta p_{\rm max}$	maximum phase length minimum phase length	
$\Delta p_{\min} \Delta v_{ex}$	maximum allowed velocity exceedance	
$\Delta v_{\rm ex}$ $\Delta v_{\rm off}$	offset between reference and maximum velocity	
$\Delta v_{\text{off}}$ $\Delta v_{\text{safety}}$	security offset to the maximum possible curve velocity	
$\Delta x_{SoC,max}$	maximum SoC change for a use case in long horizon battery planning	
$\Delta x_{\rm SoC,min}$	minimum SoC change for a use case in long horizon battery planning	
ṁ <sub>f</sub>	fuel consumption per second of the internal combus- tion engine	
$\dot{m}_{f,save}$	fuel saved per second for a certain engine and motor operation point	
γ	road grade	
κ	road curvature	
λ	equivalence factor of the ECMS	
U	use case in the long horizon battery planning	
μ	friction coefficient between road and wheels	
$\mu_{R}$	rolling coefficient	
$\omega_{\rm EM}$	speed of the electric motor speed of the internal combustion engine	
$\omega_{\text{ICE}}$	speed of the propshaft	
$\omega_{ m prop} \ \omega_{ m whl}$	speed of the wheel	
$\varsigma_i$	weighting factors in the cost functions of the short	
	horizon optimization	
$\xi_i$	weighting factors in the cost functions of the long	
	horizon battery planning	
a	vehicle acceleration	
b <sub>clt</sub>	state of the clutch (open or closed)	
b <sub>ICE</sub>	engine on/off state air drag coefficient	
C <sub>Air</sub>	air drag resistance force	
F <sub>drag</sub> F <sub>grade</sub>	grade resistance force	
F <sub>roll</sub>	rolling resistance force	
<b>f</b> <sub>SHO</sub>	position derivative of the states $\boldsymbol{x}_{\text{SHO}}$	
$\mathbf{f}_{s}^{SHO}$	vector of time derivatives for the vehicle states $\mathbf{x}_{s}$	
$f_t$	vector of time derivatives for the vehicle states $\mathbf{x}_t$	
g	gravitational acceleration	
h	physical constraints of the short horizon optimization problem	
I <sub>bat,max</sub>	maximum battery current	
I <sub>bat,min</sub>	minimum battery current	
I <sub>bat</sub>	battery current	
ι <sub>G</sub>	gear transmission ratio rear axle transmission ratio	
l <sub>RA</sub>	effective vehicle inertia, inertias of all rotating parts	
J <sub>eff</sub>	inertia of the electric motor	
J <sub>EM</sub> J <sub>G</sub>	inertia of the gear box	
J <sub>G</sub> J <sub>ICE</sub>	inertia of the internal combustion engine	
$J_{\rm RA}$	inertia of the rear axle	
$J_{\rm whl}$	inertia of the wheels	
$J_{\rm LHBP, fuel}$	cost during use cases in LHBP except recuperation	
$J_{\rm LHBP,f}$	final costs for the long horizon battery planning	
J <sub>LHBP,recup</sub>	cost during recuperation use cases in LHBP	
$J_{\text{LHBP},k}$	cost functions for the long horizon battery planning	
J <sub>SHO,f</sub>	final costs for the short horizon optimization	
$k_{\mathrm{P},j}$	phase transition stage <i>j</i>	

т	vehicle mass
$m_{\rm eff}$	effective vehicle mass, including all inertias
$N_{\rm LHBP}$	number of use cases in the long horizon battery
	planning
N <sub>P</sub>	number of phases in the short horizon optimization
N <sub>S,j</sub>	number of stages in phase <i>j</i>
N <sub>S</sub>	number of stages in short horizon optimization
р	parameter vector
$P_{aux}$	electric power consumed by the auxiliaries
$P_{\rm bat}$	battery power
$P_{\rm brk}$	braking power
$P_{\rm el}$	power demand of power electric loads
$P_{\rm EM,el}$	electric power of the electric motor
P <sub>EM,max</sub>	maximum EM power
$P_{\rm EM,min}$	minimum EM power
P <sub>ICE, max</sub>	maximum ICE power
P <sub>ICE, min</sub>	minimum ICE power
$P_{lim}$	power limits for long horizon battery planning
Preq	predicted power demand for long horizon battery
	planning
Q <sub>bat</sub>	battery capacity
R <sub>EM</sub>	torque derivatives of the electric motor
R <sub>ICE</sub>	torque derivatives of the internal combustion engine
$R_{\rm i}$	battery resistance
$r_{\rm whl}$	wheel radius
S	position
s <sub>P,j</sub>	starting position of phase <i>j</i>
S <sub>SBS</sub>	battery power substitution benefit
t T	time
T <sub>brk</sub>	service brake torque
T <sub>des</sub>	desired torque from driver model
T <sub>drag</sub>	air drag resistance torque
$T_{\rm EM,high}$	highest possible EM torque for SoC change limit cal- culation in LHBP
т	lowest possible EM torque for SoC change limit cal-
$T_{\rm EM, low}$	culation in LHBP
T <sub>EM</sub>	electric motor torque
$T_{\rm G,in}$	torque transmitted from the motor side to the gearbox
$T_{G,out}$	torque transmitted from the gear box to the prop-
<sup>1</sup> G,out	shaft
Tgrade	grade resistance torque
$T_{\rm ICE}$	internal combustion engine torque
$T_{\rm loss, clt}$	torque loss in the clutch
T <sub>loss,G</sub>	torque loss in the gear box
$T_{\rm loss,RA}$	torque loss in the rear axle
T <sub>resist</sub>	driving resistance torque
T <sub>roll</sub>	rolling resistance torque
T <sub>whl</sub>	accumulated torque at the wheels
u	vector of model inputs
$U_0$	open circuit voltage of the battery
U <sub>bat</sub>	battery voltage
u <sub>clt</sub>	clutch open/close command
u <sub>G</sub>	desired gear
u <sub>ICE</sub>	engine on/off command
<b>u</b> <sub>SHO</sub>	input vector for short horizon optimization
ν	vehicle velocity
Vcorr	merged velocity limits
<i>v</i> <sub>curve,max</sub>	curve velocity limit
V <sub>des</sub>	desired velocity
$v_{\text{law}}$	speed limit
$v_{\rm lim,min}$	lowest curve velocity limit
$v_{\rm max}$	maximum velocity
$v_{\min}$	minimum velocity

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